COUNTY OF MENDOCINO
DEPARTMENT OF PLANNING AND BUILDING SERVICES
860 NORTH BUSH STREET · UKIAH · CALIFORNIA · 95482
752 SOUTH FRANKLIN STREET · FT. BRAGG · CALIFORNIA · 95437

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www.mendocinocounty.org/pbs

December 16, 2025

Air Quality Management District
Assessor's Office
Building Division Fort Bragg
Department of Transportation (DOT)
Environmental Health (EH)
Mendocino City Comm Services District
Mendocino Fire Protection District
CALFIRE
- Land Use
California Coastal Commission
California Dept. of Fish & Wildlife
US Department of Fish & Wildlife
Cloverdale Rancheria
Redwood Valley Rancheria
Sherwood Valley Band of Pomo Indians

CASE#: UM_2025-0004
DATE FILED: 12/8/2025
OWNER: MENDOCINO UNION HIGH SCHOOL DI
REQUEST: Coastal Development Use Permit Modification for the conversion of an existing test well into a supply well, with installation of underground water and power lines and associated trenching.
LOCATION: In the Coastal Zone, 1.0± miles east-southeast of Mendocino Town center, on the north side of Little Lake Rd (CR 408), east of its intersection with Gurley Ln (CR 407Z), located at 44100 Little Lake Rd, Mendocino. (APNs: 119-100-23, 119-100-03, 119-100-04)
SUPERVISORIAL DISTRICT:
STAFF PLANNER: Rob Fitzsimmons
RESPONSE DUE DATE: December 30, 2025

PROJECT INFORMATION CAN BE FOUND AT:
www.mendocinocounty.org
Select "Government" from the drop-down; then locate Planning and Building Services/Public Agency Referrals.

Mendocino County Planning & Building Services is soliciting your input, which will be used in staff analysis and forwarded to the appropriate public hearing. You are invited to comment on any aspect of the proposed project(s). Please convey any requirements or conditions your agency requires for project compliance to the project coordinator at the above address, or submit your comments by email to pbs@mendocinocounty.org. Please note the case number and name of the project coordinator with all correspondence to this department.

We have reviewed the above application and recommend the following (please check one):

☐ No comment at this time.

☐ Recommend conditional approval (attached).

☐ Applicant to submit additional information (attach items needed, or contact the applicant directly, copying Planning and Building Services in any correspondence you may have with the applicant)

☐ Recommend denial (Attach reasons for recommending denial).

☐ Recommend preparation of an Environmental Impact Report (attach reasons why an EIR should be required).

☐ Other comments (attach as necessary).

REVIEWED BY:

Signature _____ Department _____ Date _____

CASE: UM_2025-0004

OWNER/ APPLICANT: Mendocino Unified School District

AGENT: Matt Kennedy

REQUEST: Coastal Development Use Permit Modification for the conversion of an existing test well into a supply well, with installation of underground water and power lines and associated trenching.

LOCATION: In the Coastal Zone, 1.0± miles east-southeast of Mendocino Town center, on the north side of Little Lake Rd (CR 408), east of its intersection with Gurley Ln (CR 407Z), located at 44100 Little Lake Rd, Mendocino.

APNs: 119-100-23, 119-100-03, 119-100-04

PARCEL SIZE: 5.6 acres

GENERAL PLAN: Public Facilities

ZONING: Public Facilities

EXISTING USES: Public Facilities

DISTRICT: 5, Williams

	ADJACENT GENERAL PLAN	ADJACENT ZONING	ADJACENT LOT SIZES	ADJACENT USES
NORTH:	RR5	RR5	2.9±, 3.25± ac	Residential
EAST:	PF	PF	2.5± ac	Open Space
SOUTH:	RR5	RR5	2.0±, 5.9± ac	Agricultural
WEST:	RR5	RR5	1.2±, 2.0± ac	Residential

REFERRAL AGENCIES

LOCAL
- ☒ Air Quality Management District
- ☒ Assessor's Office
- ☒ Building Division Fort Bragg
- ☒ Department of Transportation (DOT)
- ☒ Environmental Health (EH)
- ☒ Mendocino City Comm Services Dist
- ☒ Mendocino FPD

STATE
- ☒ CALFIRE (Land Use)
- ☒ California Coastal Commission
- ☒ California Dept. of Fish & Wildlife

FEDERAL
- ☒ US Department of Fish & Wildlife

TRIBAL
- ☒ Cloverdale Rancheria
- ☒ Redwood Valley Rancheria
- ☒ Sherwood Valley Band of Pomo Indians

ADDITIONAL INFORMATION:
This application is a modification of Coastal Development Use Permit U_2023-0004. U_2023-0004 was approved by the Mendocino County Planning Commission on 4/4/2024, then ultimately revised via UM_2024-0008 on 12/5/2024. As then modified, the project comprised the demolition and replacement of two existing water tanks, chlorination and control building, and related infrastructure, including installation of test wells.

One of these test wells proved viable, yielding 6 gallons per minute during a 72 hour pump test with minimal effect on neighboring wells. The applicant now seeks to convert this well to a production well via the proposed permit modification.

One component of the original iteration of this project, approved under U_2023-0004, was the widening of the existing gravel driveway. At the time, the County Department of Transportation requested and the Planning Commission approved a condition requiring repaving of the driveway approach "with asphalt or comparable surfacing to the adjacent road." The subsequent modification to the project, UM_2024-0008, removed the driveway-widening component in light of potential impacts onto water courses and instead proposed the creation of an entirely new driveway, providing more direct access to the tank site. Staff understood that this new driveway was to be the primary access for the project and so removed the Condition requiring improvement of the existing gravel driveway approach from UM_2024-0008. However, it appears the unwidened, unimproved gravel driveway has continued to be used during construction activities.

An Initial Study/Mitigated Negative Declaration was adopted for the project as proposed under U_2023-0004 (SCH 2022020568 - https://ceqanet.opr.ca.gov/2020080439/2). MUSD has declined to prepare an addendum to the MND, so Mendocino County as the Responsible Agency will likely prepare one instead.

STAFF PLANNER: ROB FITZSIMMONS **DATE:** 12/16/2025

ENVIRONMENTAL DATA

1. MAC:
GIS
NO

2. FIRE HAZARD SEVERITY ZONE:
CALFIRE FRAP maps/GIS
Moderate

3. FIRE RESPONSIBILITY AREA:
CALFIRE FRAP maps/GIS
State Responsibility Area

4. FARMLAND CLASSIFICATION:
GIS
Rural Residential and Rural Commercial

5. FLOOD ZONE CLASSIFICATION:
FEMA Flood Insurance Rate Maps (FIRM)
NO

6. COASTAL GROUNDWATER RESOURCE AREA:
Coastal Groundwater Study/GIS
Critical Water Resources (CWR)

7. SOIL CLASSIFICATION:
Mendocino County Soils Study Eastern/Western Part
124 – Caspar-Quinliven-Ferncreek complex, 9-30% slopes
199 – Shinglemill-Gibney complex, 2-9% slopes

8. PYGMY VEGETATION OR PYGMY CAPABLE SOIL:
LCP maps, Pygmy Soils Maps; GIS
NO

9. WILLIAMSON ACT CONTRACT:
GIS/Mendocino County Assessor's Office
NO

10. TIMBER PRODUCTION ZONE:
GIS
NO

11. WETLANDS CLASSIFICATION:
GIS
NO

12. EARTHQUAKE FAULT ZONE:
Earthquake Fault Zone Maps; GIS
NO

13. AIRPORT LAND USE PLANNING AREA:
Airport Land Use Plan; GIS
NO

14. SUPERFUND/BROWNFIELD/HAZMAT SITE:
GIS; General Plan 3-11
NO

15. NATURAL DIVERSITY DATABASE:
CA Dept. of Fish & Wildlife Rarefind Database/GIS
YES

16. STATE FOREST/PARK/RECREATION AREA ADJACENT:
GIS; General Plan 3-10
NO

17. LANDSLIDE HAZARD:
Hazards and Landslides Map; GIS; Policy RM-61; General Plan 4-44
NO

18. WATER EFFICIENT LANDSCAPE REQUIRED:
Policy RM-7; General Plan 4-34
NO

19. WILD AND SCENIC RIVER:
www.rivers.gov (Eel Only); GIS
NO

20. SPECIFIC PLAN/SPECIAL PLAN AREA:
Various Adopted Specific Plan Areas; GIS
NO

21. STATE CLEARINGHOUSE REQUIRED:
Policy
YES

22. OAK WOODLAND AREA:
USDA
NO

23. HARBOR DISTRICT:
Sec. 20.512
NO

FOR PROJECTS WITHIN THE COASTAL ZONE ONLY

24. LCP LAND USE CLASSIFICATION:
LCP Land Use maps/GIS
PF - LCP LAND USE MAP 17: MENDOCINO

25. LCP LAND CAPABILITIES & NATURAL HAZARDS:
LCP Land Capabilities maps/GIS; 20.500
Marine Terrace Deposits (Zone 2) – Strong Shaking;
Timberland – Moderate Productivity

26. LCP HABITATS & RESOURCES:
LCP Habitat maps/GIS; 20.496
Urban; Coastal Forest

27. COASTAL COMMISSION APPEALABLE AREA:
Post LCP Certification Permit and Appeal Jurisdiction maps/GIS; 20.544
NO

28. CDP EXCLUSION ZONE:
CDP Exclusion Zone maps/GIS
NO

29. HIGHLY SCENIC AREA:
Highly Scenic & Tree Removal Area Maps/GIS; Secs. 20.504.015, 20.504.020
NO

30. BIOLOGICAL RESOURCES & NATURAL AREAS:
Biological Resources & Natural Area Map; GIS; General Plan 4-9
YES

31. BLUFFTOP GEOLOGY:
GIS; 20.500.020
NO

COUNTY OF MENDOCINO
DEPT OF PLANNING & BUILDING SERVICES

120 WEST FIR STREET
FORT BRAGG, CA 95437
Telephone: 707-964-5379
Fax: 707-961-2427

Case No(s) _____
CDF No(s) _____
Date Filed _____
Fee $ _____
Receipt No. _____
Received by _____

☐ Material ☐ Immaterial

Office Use Only

COASTAL DEVELOPMENT PERMIT AMENDMENT APPLICATION FORM

Name of Applicant	Name of Owner(s)	Name of Agent
Mendocino Unified School District	Mendocino Unified School District	Matt Kennedy
Mailing Address	**Mailing Address**	**Mailing Address**
44141 Little Lake Road, Mendocino, CA 95460	44141 Little Lake Road, Mendocino, CA 95460	2235 Mercury Way, Suite 150, Santa Rosa, CA 95407
Telephone Number	**Telephone Number**	**Telephone Number**
(707) 937-5868	(707) 937-5868	(707) 540-3376

I certify that the information submitted with this application is true and accurate.

Matthew C. Keenan — 11/17/2025
Signature of Applicant/Agent — Date

Signature of Owner — 11/17/25
Date

Driving Directions

The site is located on the N (N/S/E/W) side of Little Lake Road (name road)

approximately 0.7 miles (feet/miles) E (N/S/E/W) of its intersection with

Highway 1 (provide nearest major intersection).

Assessor's Parcel Number(s)	Previous Coastal Development Permit # (s)
119-100-004	U_2023-0004

Parcel Size

0.25 Acres

☐ Square Feet
☑ Acres

Street Address of Project

44020 Little Lake Road, Mendocino, CA 95460

Please note: Before submittal, please verify correct street address with the Planning Division in Ukiah.

COASTAL DEVELOPMENT PERMIT AMENDMENT APPLICATION QUESTIONNAIRE

The purpose of this questionnaire is to relate information concerning your application to the Planning & Building Services Department and other agencies who will be reviewing your project proposal. The more detail that is provided, the easier it will be to promptly process your application. Please answer all questions. Those questions which do not pertain to your project, please indicate "Not Applicable" or "N/A".

1. Describe your project and include secondary improvements such as wells, septic systems, grading, vegetation removal, roads, etc. (Please describe all proposed modifications to the issued permit.)

Mendocino Unified School District is implementing water supply and storage improvements to address water system deficiencies identified by the State Water Resources Control Board (SWRCB) Division of Drinking Water (DDW) at its water supply and storage site located at 44020 Little Lake Road in the Village of Mendocino. As part of the Mendocino Unified School District's ongoing water supply and storage improvement project (U_2023-0004), two groundwater test wells were installed to assess source capacity and system redundancy. One test well (TW 07) proved viable, yielding 6 gallons per minute (gpm) during a 72-hour pump test with minimal impact on nearby wells and favorable aquifer characteristics. Modeling showed negligible effects on surrounding domestic wells, and adding TW 07 would raise the District's total supply to 18 gpm, meeting regulatory requirements even with the primary well offline. The District now proposes converting TW 07 into a permitted production well for backup and seasonal tank filling, with associated infrastructure improvements.

2. If the project is residential, please complete the following:

TYPE OF UNIT	NUMBER OF STRUCTURES/UNITS	SQUARE FEET PER UNIT
☐ Single Family	Not Applicable	Not Applicable
☐ Mobile Home		
☐ Duplex/Multifamily		

3. Are there existing structures on the property? ☑ Yes ☐ No
If yes, describe below and identify the use of each structure on the plot plan.

The MUSD's water supply and storage site includes two water storage tanks, a water treatment building, groundwater wells, underground piping, maintenance building, pump house that has been converted to a student radio transmission station, and gravel roads.

4. Utilities will be supplied to the site as follows:

A. Electricity
- ☑ Utility Company (service exists to the parcel).
- ☐ Utility Company (requires extension of services to site: _____ feet _____ miles
- ☐ On Site generation, Specify: _____
- ☐ None

B. Gas
- ☐ Utility Company/Tank
- ☑ None

C. Telephone: ☐ Yes ☑ No

5. Will there be any exterior lighting? ☐ Yes ☑ No
If yes, describe below and identify the location of all exterior lighting on the plot plan and building plans.

6. What will be the method of sewage disposal?

☐ Community sewage system, specify supplier _____
☐ Septic Tank (indicate primary + replacement leachfields on plot plan)
☑ Other, specify Not Applicable (Project does not generate sewage)

7. What will be the domestic water source?

☐ Community water system, specify supplier _____
☑ Well
☐ Spring
☐ Other, specify _____

8. Is any grading including road/driveway construction planned? ☐ Yes ☑ No

Estimate the amount of grading (cut and fill quantities) in cubic yards: 0 c.y. Please indicate on the site plan the areas and quantities of grading. **If greater than 50 cubic yards or if greater than 2 feet of cut or 1 foot of fill will result, please provide a grading plan.**

Estimate the length of the proposed road/driveway: 0 feet.

Describe the terrain to be traversed (e.g., steep, moderate slope, flat, etc.).

9. Will vegetation be removed accommodate the proposed project? ☐ Yes ☑ No
If yes, explain:

How many trees will be removed as a result of the project: _____. Indicate on the site plan all trees to be removed which are greater than 12-inches in diameter (measured four feet from the ground). If applicable, please indicate on the site plan the size, location and species of all on-site trees that provide screening from public view areas.

10. Is the proposed development visible from:

A. State Highway 1? ☐ Yes ☑ No
B. Park, beach or recreation area? ☐ Yes ☑ No

If you answered yes to either question, explain.

11. Project Height. Maximum height of structure(s). 1 foot feet

12. Describe all exterior materials and colors of all structures.

Siding material _____. Color _____.
Trim material _____. Color _____.
Chimney material _____. Color _____.
Roofing material _____. Color _____.
Window frame material _____. Color _____.
Door material _____. Color _____.
Fencing material _____. Color _____.
Retaining walls material _____. Color _____.
Other exterior materials _____. Color _____.

Not applicable.

13. Are there any water courses, anadromous fish streams, sand dunes, rookeries, marine mammal haul-out areas, wetlands, riparian areas, pygmy vegetation, threatened, rare or endangered plants/communities, animals or habitat which support rare and endangered species located on the project site or within 100 feet of the project site?

☑ Yes ☐ No

If yes, please describe the resource and attach any biological/botanical reports:

A prior Wetland Delineation and ESHA Buffer Analysis are provided as attachments to this CDPM Application. The proposed well conversion is not located within a an Environmentally Sensitive Habitat Area (ESHA).

14. If the project is **commercial**, **industrial**, or **institutional**, complete the following:

Total square footage of all structures: _____
Estimated employees per shift: _____
Estimated shifts per day: _____
Type of loading facilities proposed: Not Applicable to Project

Will the proposed project be phased? ☑ Yes ☐ No

If Yes, explain your plans for phasing.

This CDP Amendment covers Phase 2 of the District's ongoing water supply and storage improvement project (U_2023-0004). Phase 1 included installing test wells for data collection and resource evaluation. Phase 2 proposes converting one of those test wells into a groundwater supply well.

Parking will be provided as follows:

Number of Spaces Existing Not Applicable Proposed _____ Total _____

Number of standard spaces _____ Size _____
Number of handicapped spaces _____ Size _____



Sources: Esri, HERE, DeLorme, increment P Corp., NPS, NRCan, Ordnance Survey, © OpenStreetMap contributors, USGS, NGA, NASA, CGIAR, N Robinson, NCEAS, NLS, OS, NMA, Geodatastyrelsen, Rijkswaterstaat, GSA, Geoland, FEMA, Intermap and the GIS user community

CASE: UM 2024-0008
OWNER: Mendocino Unified School
APN: 119-100-03, 04 & 23
APLCT: Mendocino Unified School
AGENT: Matt Kennedy
ADDRESS: 44020 Little Lake Rd. Mendocino

Major Towns & Places
Major Roads
Coastal Zone Boundary
Highways

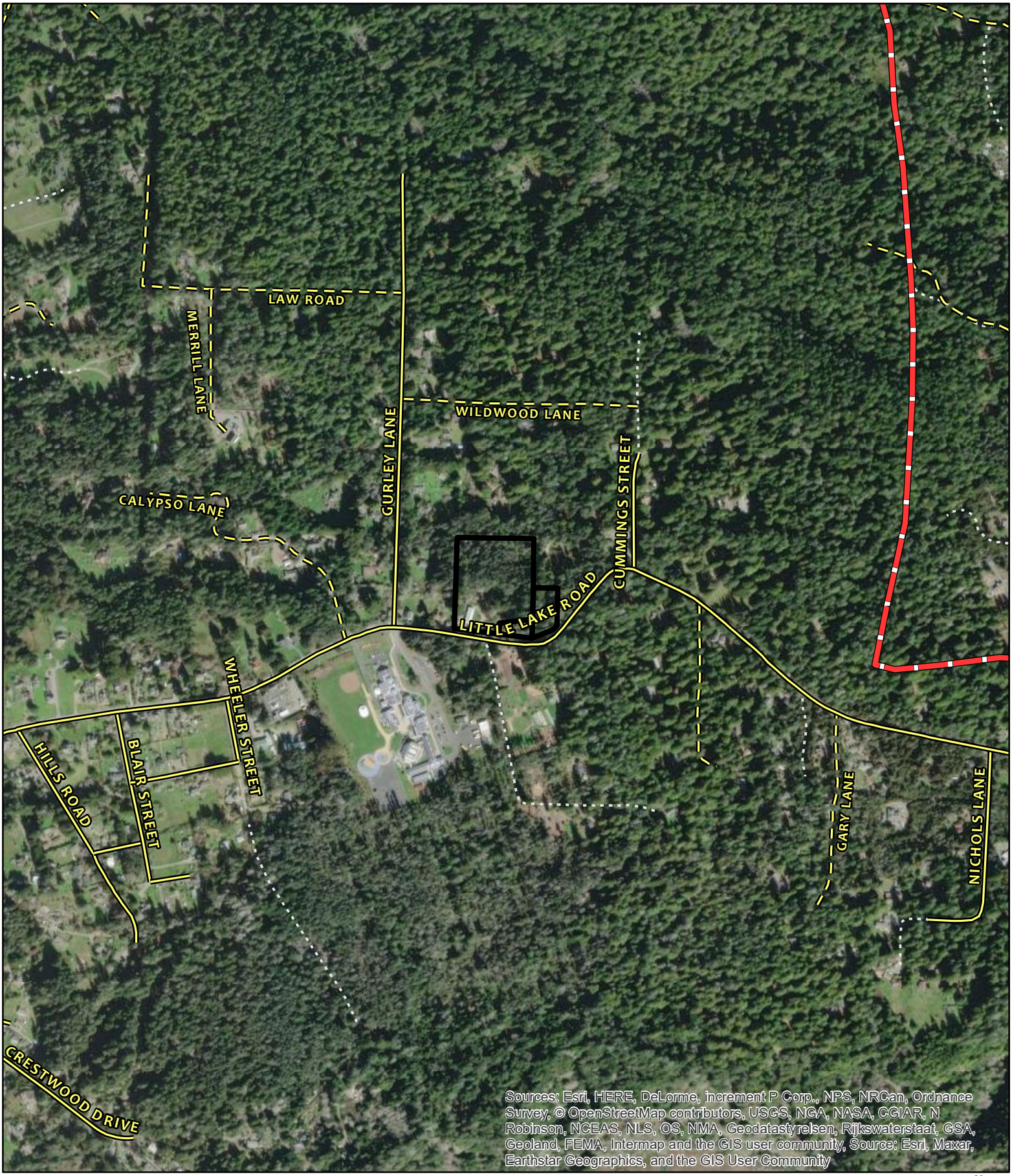
0 2,750 5,500 Feet
0 0.5 1 Miles

N W E S

1:63,360

LOCATION

THIS MAP AND DATA ARE PROVIDED WITHOUT WARRANTY OF ANY KIND.
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CASE: UM 2024-0008
OWNER: Mendocino Unified School District
APN: 119-100-03, 04 & 23
APLCT: Mendocino Unified School District
AGENT: Matt Kennedy
ADDRESS: 44020 Little Lake Rd, Mendocino

Coastal Zone Boundary
Public Roads
Private Roads
Driveways/Unnamed Roads

0 362.5 725 Feet
0 0.05 0.1 Miles

N
W E
S

1:8,000

AERIAL IMAGERY

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CASE: UM 2024-0008
OWNER: Mendocino Unified School District
APN: 119-100-03, 04 & 23
APLCT: Mendocino Unified School District
AGENT: Matt Kennedy
ADDRESS: 44020 Little Lake Rd, Mendocino

Public Roads

Driveways/Unnamed Roads

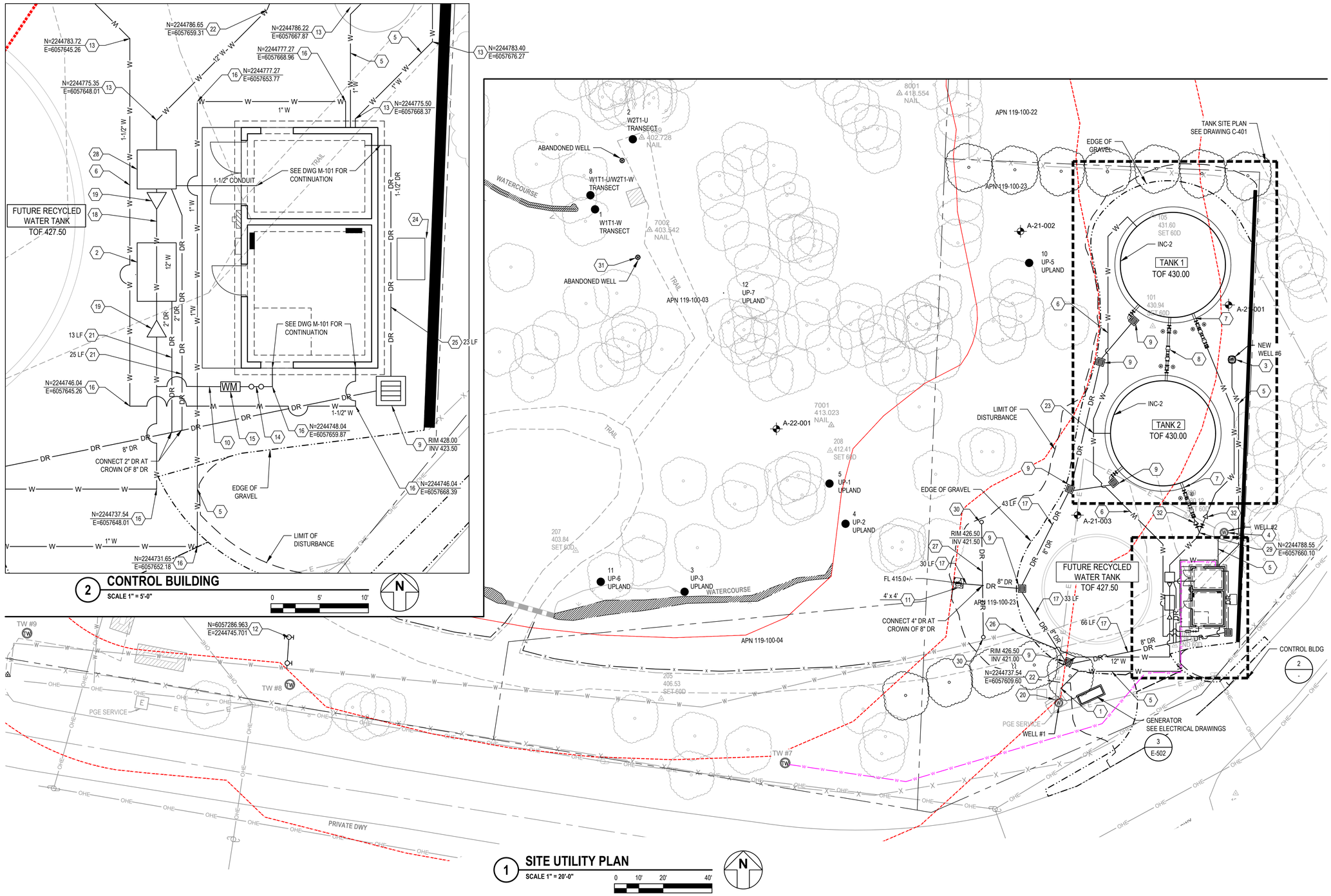
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SS ☑ FLS ☑ ACS ☐
DATE: 07/01/2025

GENERAL NOTES

1. ALL MATERIALS AND APPURTENANCES IN CONTACT WITH POTABLE WATER SHALL BE NSF-61 CERTIFIED.
2. ALL UNDERGROUND WATER PIPES 4" AND LARGER SHALL HAVE RESTRAINED JOINTS AS SPECIFIED IN SECTION 33 11 00. THRUST BLOCKS ARE NOT ALLOWED EXCEPT WHERE SHOWN ON THE DRAWINGS.
3. SEE DRAWING E-101 FOR SITE ELECTRICAL IMPROVEMENTS.
4. INSTALL (N) PIPES IN TRENCHES IN ACCORDANCE WITH DETAIL 1 ON DRAWING C-503.

KEYNOTES

1. INTERCEPT (E) WELL #1 WATER SUPPLY PIPE AND ROUTE (N) 1" SCH 80 PVC RAW WATER SUPPLY LINE TO (N) BUILDING.
2. PROVIDE (N) FLOW METER IN VAULT. SEE DETAIL 2 ON DRAWING C-502.
3. PROVIDE (N) WELL HEAD IMPROVEMENTS. SEE DETAIL 1 ON DRAWING M-501. PERFORM PUMP TEST. SEE SPECIFICATIONS AND PROCEDURES ON DRAWING M-301.
4. DEMOLISH (E) WELL HEAD ENCLOSURE AND REHABILITATE (E) WELL NO.2. SEE DETAILS 1 AND 2 ON DRAWING M-501. SEE WELL NO. 2 REHABILITATION PLAN ON DRAWING M-301.
5. PROVIDE (N) 1" SCH 80 PVC RAW WATER SUPPLY LINE FROM WELL TO (N) CHLORINATION AND CONTROL BUILDING.
6. PROVIDE (N) 1-1/2" SCH 80 PVC TREATED WATER SUPPLY LINE.
7. PROVIDE (N) 10" TANK OUTLET PIPING. SEE DRAWING C-401.
8. PROVIDE (N) 10" TANK INTERCONNECTION PIPING. SEE DRAWING C-401.
9. PROVIDE (N) DROP INLET. SEE DETAIL 5 ON DRAWING C-502.
10. PROVIDE (N) 1" WATER SERVICE. SEE DETAIL 1 ON DRAWING C-504.
11. PROVIDE RIPRAP AT DRAIN PIPE OUTLET TO DRAINAGE SWALE. SEE DETAIL 4 ON DRAWING C-502.
12. PROVIDE FIRE HYDRANT LATERAL PER DETAIL 2 ON DRAWING C-503.
13. PROVIDE 45° BEND. MATCH PIPE SIZE.
14. PROVIDE 1" DOUBLE CHECK BACKFLOW PREVENTER. SEE DETAIL 2 ON DRAWING C-504.
15. PROVIDE 3/4" WATER METER IN BOX. SEE DETAIL 1 ON DRAWING C-504.
16. PROVIDE 90° BEND. MATCH PIPE SIZE.
17. PROVIDE (N) 8" PVC (DR 18) DRAIN LINE.
18. PROVIDE 5 FEET STRAIGHT RUN DI PIPE UPSTREAM AND 2 FEET STRAIGHT RUN DI PIPE DOWNSTREAM OF FLOW METER.
19. PROVIDE 12" x 8" REDUCER.
20. REDEVELOP (E) WELL #1. SEE SPECIFICATIONS AND PROCEDURES ON DRAWING M-301.
21. PROVIDE 2" VAULT DRAIN PIPE. ROUTE DRAIN PIPE PER PLAN.
22. PROVIDE 22.5° BEND. MATCH PIPE SIZE.
23. PROVIDE TEE. MATCH PIPE SIZE.
24. PROVIDE HVAC EQUIMENT PAD. SEE DETAIL 5 ON DRAWING S-502. SIZE AND LOCATION PER DRAWING H-101.
25. PROVIDE 1-1/2" SCH 80 PVC PUMP TO WASTE LINE. CONNECT TO DROP INLET. SEE DRAWING M-101 FOR BUILDING CONNECTION.
26. CONNECT TO (E) 12" DIP WATER LINE.
27. PROVIDE PERFORATE 4" KEYWAY DRAIN PIPE. SEE DETAIL 4 ON DRAWING C-503.
28. PROVIDE CHLORINE CONTROL VAULT. SEE DETAIL 5 ON DRAWING C-505.
29. PROVIDE WYE. MATCH PIPE SIZE.
30. PROVIDE STORM DRAIN CLEANOUT. SEE DETAIL 5 ON DRAWING C-503.
31. CONVERT (E) CAISSON TYPE WELL TO MONITORING WELL PER DETAIL ON DRAWING M-302.
32. PROVIDE 12"x10" REDUCER AND 10" GATE VALVE.

No.	Issue	Drawn	Approved	Date

Bar is one inch on original size sheet
0 1"

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STEVEN GLEN KENNEDY 26304 CIVIL STATE OF CALIFORNIA
6/6/2025

GHD Inc.
2235 Mercury Way Suite 150
Santa Rosa California 95407 USA
T 1 707 523 1010 F 1 707 527 8679 W www.ghd.com

This document shall not be used for construction unless signed and sealed for construction.

Drawn	C. COOK/D. DE LEON	Designer	M. KENNEDY
Drafting Check	M. KENNEDY	Design Check	M. KENNEDY
Project Manager	M. KENNEDY	Date	JUNE 2025
		Scale	SHOWN

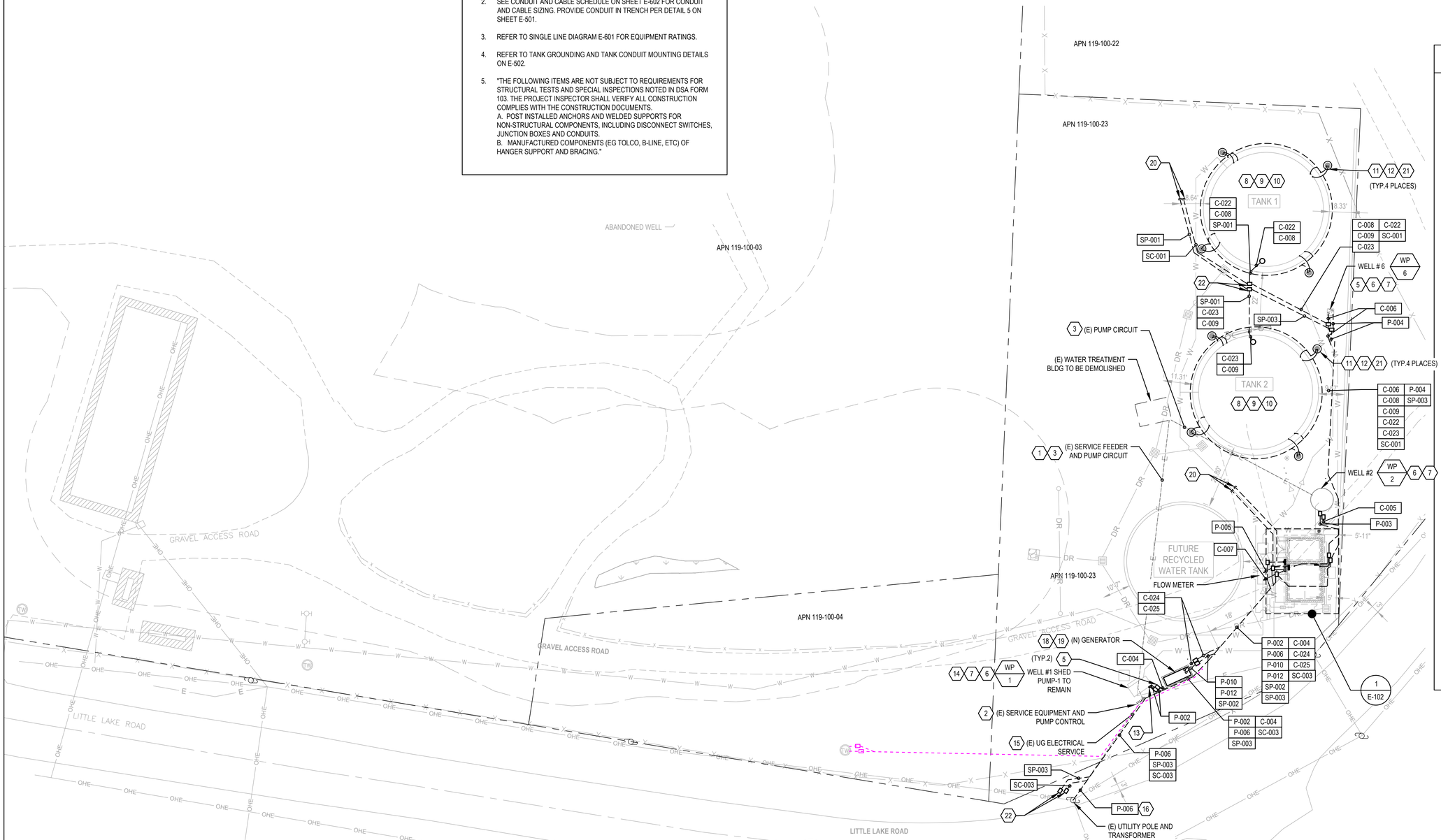
Client MENDOCINO UNIFIED SCHOOL DISTRICT
Project WATER SUPPLY AND STORAGE PROJECT
Title SITE UTILITY PLAN
Project No. 11136611
Original Size ANSI D
Drawing No. C-107
Sheet 17 of 57

Plot Date: 5 June 2025 - 11:37 AM Plotted By: Chris Bach Filename: \\ghdnet\ghd\US\Santa Rosa\Projects\111\11136611 MUSD Grant Assistance and MP\06-CAD\Sheets\11136611_C-107_Utilities.dwg

GENERAL NOTES

1. SITE REQUIRES COORDINATION WITH PG&E FOR NEW SERVICE. CONTRACTOR SHALL INITIATE SERVICE APPLICATION COORDINATE AND SCHEDULE SERVICE IMPROVEMENTS WITH PG&E TO MINIMIZE SITE POWER OUTAGE DURATION. COORDINATE WITH ENGINEER ON ALL SCHEDULING, AND PG&E SERVICE DATES.
2. SEE CONDUIT AND CABLE SCHEDULE ON SHEET E-602 FOR CONDUIT AND CABLE SIZING. PROVIDE CONDUIT IN TRENCH PER DETAIL 5 ON SHEET E-501.
3. REFER TO SINGLE LINE DIAGRAM E-601 FOR EQUIPMENT RATINGS.
4. REFER TO TANK GROUNDING AND TANK CONDUIT MOUNTING DETAILS ON E-502.
5. "THE FOLLOWING ITEMS ARE NOT SUBJECT TO REQUIREMENTS FOR STRUCTURAL TESTS AND SPECIAL INSPECTIONS NOTED IN DSA FORM 103. THE PROJECT INSPECTOR SHALL VERIFY ALL CONSTRUCTION COMPLIES WITH THE CONSTRUCTION DOCUMENTS.
   A. POST INSTALLED ANCHORS AND WELDED SUPPORTS FOR NON-STRUCTURAL COMPONENTS, INCLUDING DISCONNECT SWITCHES, JUNCTION BOXES AND CONDUITS.
   B. MANUFACTURED COMPONENTS (EG TOLCO, B-LINE, ETC) OF HANGER SUPPORT AND BRACING."

IDENTIFICATION STAMP
DIV. OF THE STATE ARCHITECT
APP: 01-122197 INC: 01
REVIEWED FOR
SS ☑ FLS ☑ ACS ☐
DATE: 07/01/2025



KEYNOTES

1. REMOVE (E) SERVICE FEEDER TO OLD TREATMENT BUILDING. ABANDON (E) UG CONDUIT IN PLACE AND REMOVE WHEN IN CONFLICT WITH IMPROVEMENTS.
2. REMOVE (E) PUMP CONTROL PANEL, DISCONNECT SWITCH, METER/MCB PANEL AND ASSOCIATED PUMP EQUIPMENT.
3. REMOVE (E) PUMP CIRCUITS. ABANDON (E) UG CONDUIT IN PLACE AND REMOVE WHEN IN CONFLICT WITH IMPROVEMENTS.
4. NOT USED.
5. PROVIDE 11"X17" TRAFFIC RATED POWER AND CONTROL PULL BOXES WITH STEEL COVERS. SEE DETAIL 3 ON SHEET E-501.
6. PROVIDE PUMP DISCONNECT SWITCH IN NEMA 3RX ENCLOSURE. PROVIDE UNISTRUT MOUNTING FRAME.
7. PROVIDE SUBMERSIBLE LEVEL TRANSDUCER AT EACH WELL. REFER TO DETAILS 1 AND 2 IN SHEET M-501.
8. PROVIDE ULTRASONIC TRANSDUCER AT EACH TANK.
9. PROVIDE SS JUNCTION BOX WITH TERMINAL STRIP AT TOP OF EACH TANK.
10. PROVIDE INTRUSION SWITCH AT TANK ACCESS HATCH. PROVIDE MANUFACTURER WIRES IN CONDUIT FROM SWITCHES TO JUNCTION BOX. PROVIDE CONDUIT AND WIRE FROM JUNCTION BOX TO PLC.
11. PROVIDE 5/8" X 10' LONG COPPER GROUND ROD. PROVIDE #4/0 BARE COPPER WIRE TO GROUND RING. PROVIDE EXOTHERMIC WELDS TO BOTH ROD AND RING. SET GROUND ROD JUST OUTSIDE FOUNDATION AND LEAVE TOP 6" OF ROD EXPOSED ABOVE GRADE FOR TESTING.
12. PROVIDE #4/0 BARE COPPER CABLE GROUNDING RING WITH (4) LEADS UP TO TANK SIDE. PROVIDE CADWELD (EXOTHERMIC WELD) TO SIDE OF TANK AND EACH GROUNDING ROD FOR LIGHTNING PROTECTION PER NFPA 22 SECTION 4.9.
13. PROVIDE DISCONNECT SWITCH, MOUNT TO INSIDE WALL OF SHED.
14. INTERCEPT (E) PUMP CABLE AND PULL BACK TO NEW PULL BOX. SPLICE AND EXTEND TO STARTER IN CONTROL BUILDING.
15. COORDINATE REMOVAL OF (E) SERVICE FEEDER WITH PG&E, ABANDON (E) UG CONDUIT IN PLACE AND REMOVE WHEN IN CONFLICT WITH IMPROVEMENTS.
16. PROVIDE CONDUIT IN TRENCH. CONDUCTORS BY PG&E.
17. NOT USED.
18. PROVIDE AND COMMISSION GENERATOR IN SOUND ATTENUATING ENCLOSURE AND MIN 24 HOUR SUB BASE FUEL TANK. PROVIDE RADIATOR MOUNTED AUTOMATIC 50% LOAD BANK. SEE SINGLE LINE DIAGRAM FOR ADDITIONAL INFORMATION.
19. PROVIDE CONCRETE PAD PER DETAIL 3 ON SHEET E-502.
20. PROVIDE CONDUIT CAP AND MARK END OF CONDUIT.
21. PROVIDE #4/0 BARE COPPER WIRE, BOND GROUNDING RING WITH REBAR IN TANK FOUNDATION.
22. PROVIDE 24"X36" TRAFFIC RATED POWER AND CONTROL PULL BOXES WITH STEEL COVERS. SEE DETAIL 7 ON SHEET E-501.

1 ELECTRICAL SITE PLAN

SCALE 1" = 20'-0"

0 10' 20' 40'

N

No.	Issue	Drawn	Approved	Date

Bar is one inch on original size sheet
0 1"

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REGISTERED PROFESSIONAL ENGINEER ERICK A. OSORNO No. E25987 ELECTRICAL STATE OF CALIFORNIA 6/6/2025

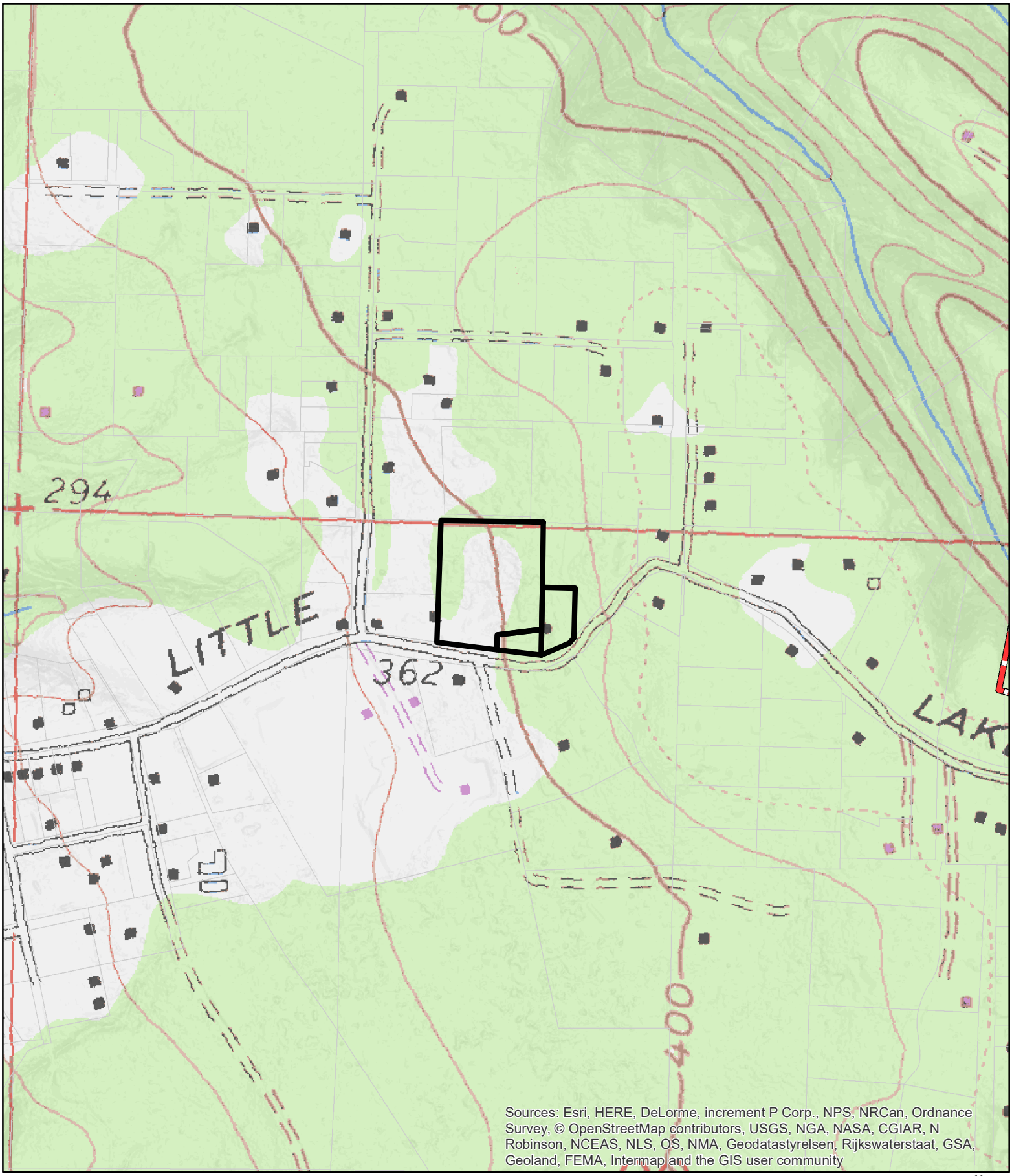
GHD Inc.
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Santa Rosa California 95407 USA
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Drawn	E.OSORNO	Designer	E.OSORNO
Drafting Check	R.GUGGIANA	Design Check	R.GUGGIANA
Project Manager	M. KENNEDY	Date	JUNE 2025
		Scale	SHOWN

Client MENDOCINO UNIFIED SCHOOL DISTRICT
Project WATER SUPPLY AND STORAGE PROJECT
Title ELECTRICAL SITE PLAN
Project No. 11136611
Original Size ANSI D
Drawing No. E-101
Sheet 47 of 57

Plot Date: 6 June 2025 - 12:20 PM Plotted By: Chris Bach Filename: \\ghdnet\ghd\US\Santa Rosa\Projects\111\11136611 MUSD Grant Assistance and MP\06-CAD\Sheets\11136611_E-101_Electrical Site Plan.dwg



CASE: UM 2024-0008
OWNER: Mendocino Unified School
APN: 119-100-03, 04 & 23
APLCT: Mendocino Unified School
AGENT: Matt Kennedy
ADDRESS: 44020 Little Lake Rd. Mendocino

Coastal Zone Boundary

Assessors Parcels

0 270 540 Feet
0 0.05 0.1 Miles

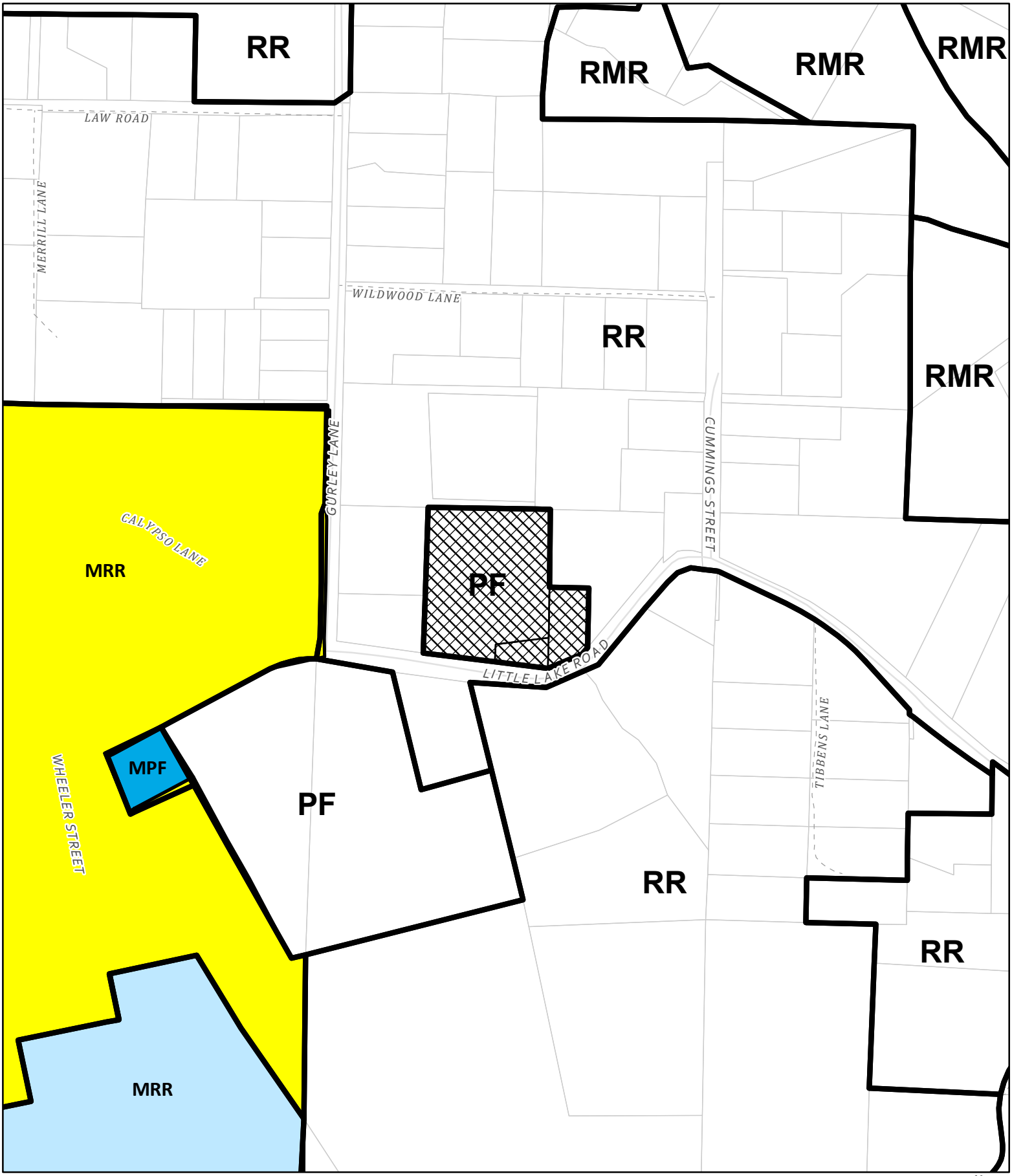
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TOPOGRAPHIC MAP

CONTOUR INTERVAL IS 40 FEET

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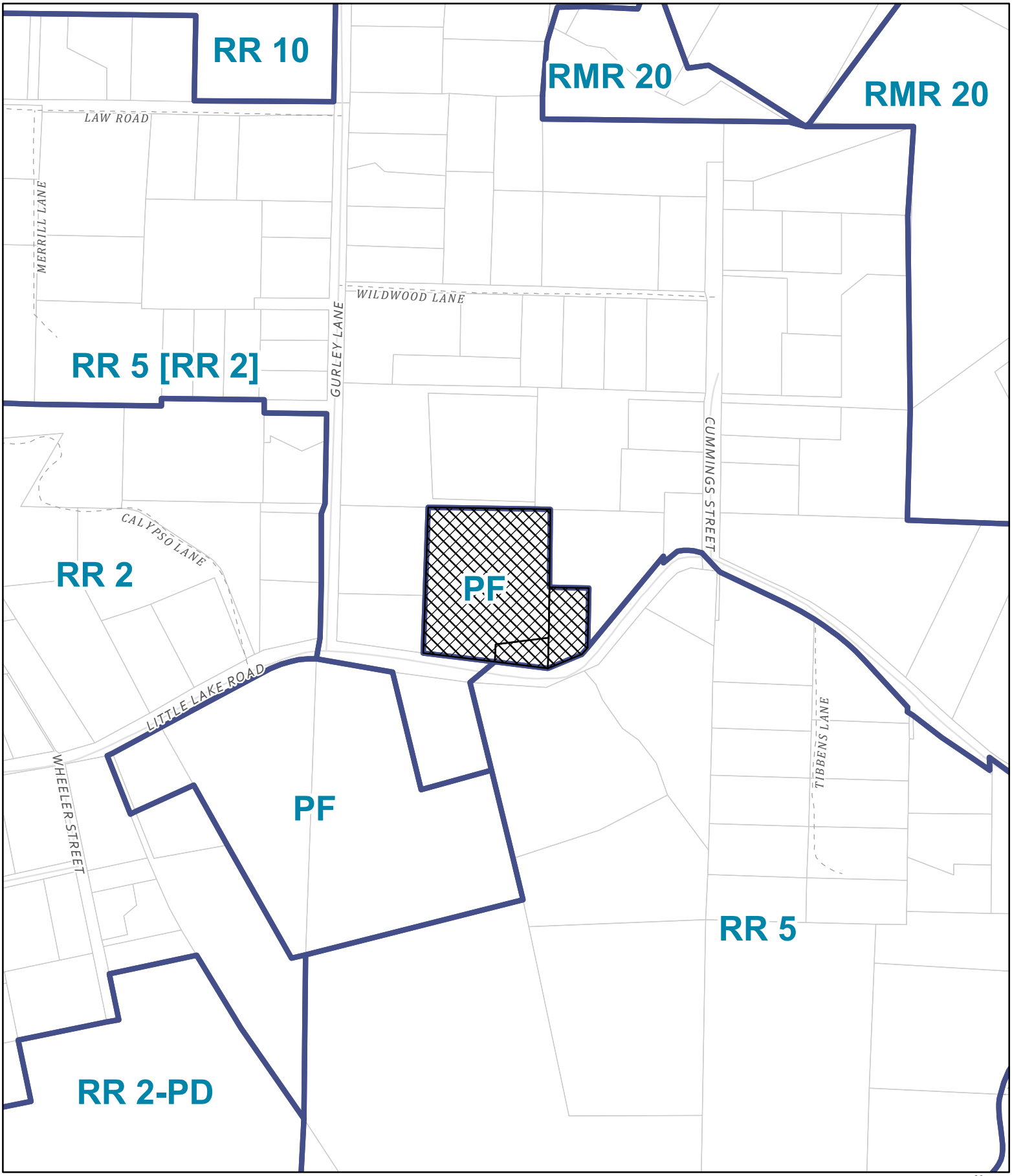


CASE: UM 2024-0008
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APN: 119-100-03, 04 & 23
APLCT: Mendocino Unified School District
AGENT: Matt Kennedy
ADDRESS: 44020 Little Lake Rd, Mendocino

Zoning Districts
Mendocino Town Zoning 020521
ZONEDISP
MRR-2
MRR-2-PD
MPF
Public Roads
Private Roads
Assessors Parcels
0 225 450 Feet
0 0.04 0.08 Miles
N
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ZONING

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Public Roads
Private Roads
Assessors Parcels

0 225 450 Feet
0 0.04 0.08 Miles

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GENERAL PLAN

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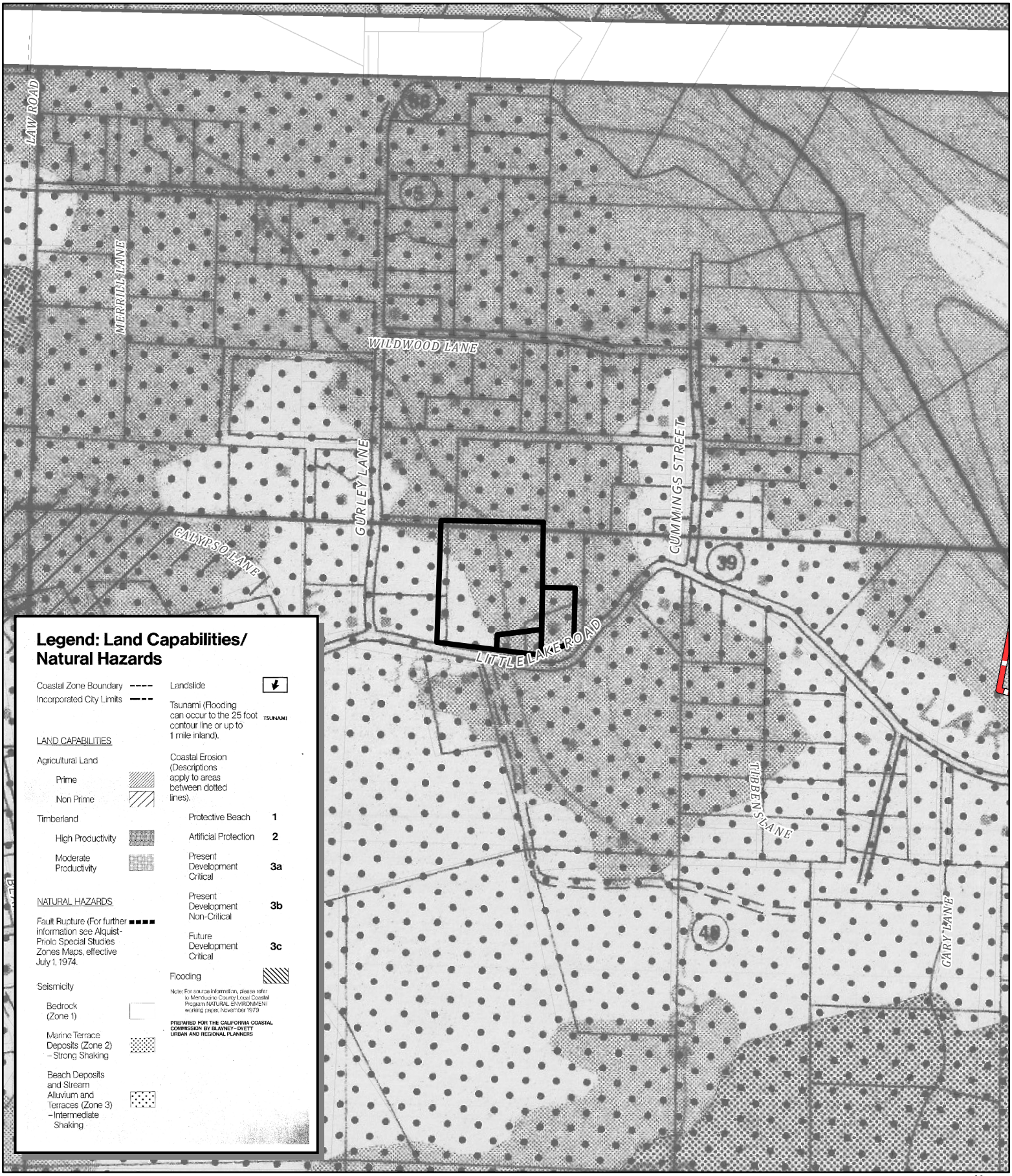
Coastal Zone Boundary
Public Roads
Private Roads
Assessors Parcels

0 270 540 Feet
0 0.05 0.1 Miles
1:6,000

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LCP LAND USE MAP 17: MENDOCINO

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Legend: Land Capabilities/ Natural Hazards

Coastal Zone Boundary ----
Incorporated City Limits ---

LAND CAPABILITIES

Agricultural Land
- Prime
- Non Prime

Timberland
- High Productivity
- Moderate Productivity

NATURAL HAZARDS

Fault Rupture (For further information see Alquist-Priolo Special Studies Zones Maps, effective July 1, 1974.

Seismicity
- Bedrock (Zone 1)
- Marine Terrace Deposits (Zone 2) – Strong Shaking
- Beach Deposits and Stream Alluvium and Terraces (Zone 3) – Intermediate Shaking

Landslide

Tsunami (Flooding can occur to the 25 foot contour line or up to 1 mile inland). TSUNAMI

Coastal Erosion (Descriptions apply to areas between dotted lines).
- Protective Beach 1
- Artificial Protection 2
- Present Development Critical 3a
- Present Development Non-Critical 3b
- Future Development Critical 3c

Flooding

Note: For source information, please refer to Mendocino County Local Coastal Program NATURAL ENVIRONMENT working paper, November 1979.

PREPARED FOR THE CALIFORNIA COASTAL COMMISSION BY BLAINEY–DYETT URBAN AND REGIONAL PLANNERS

CASE: UM 2024-0008
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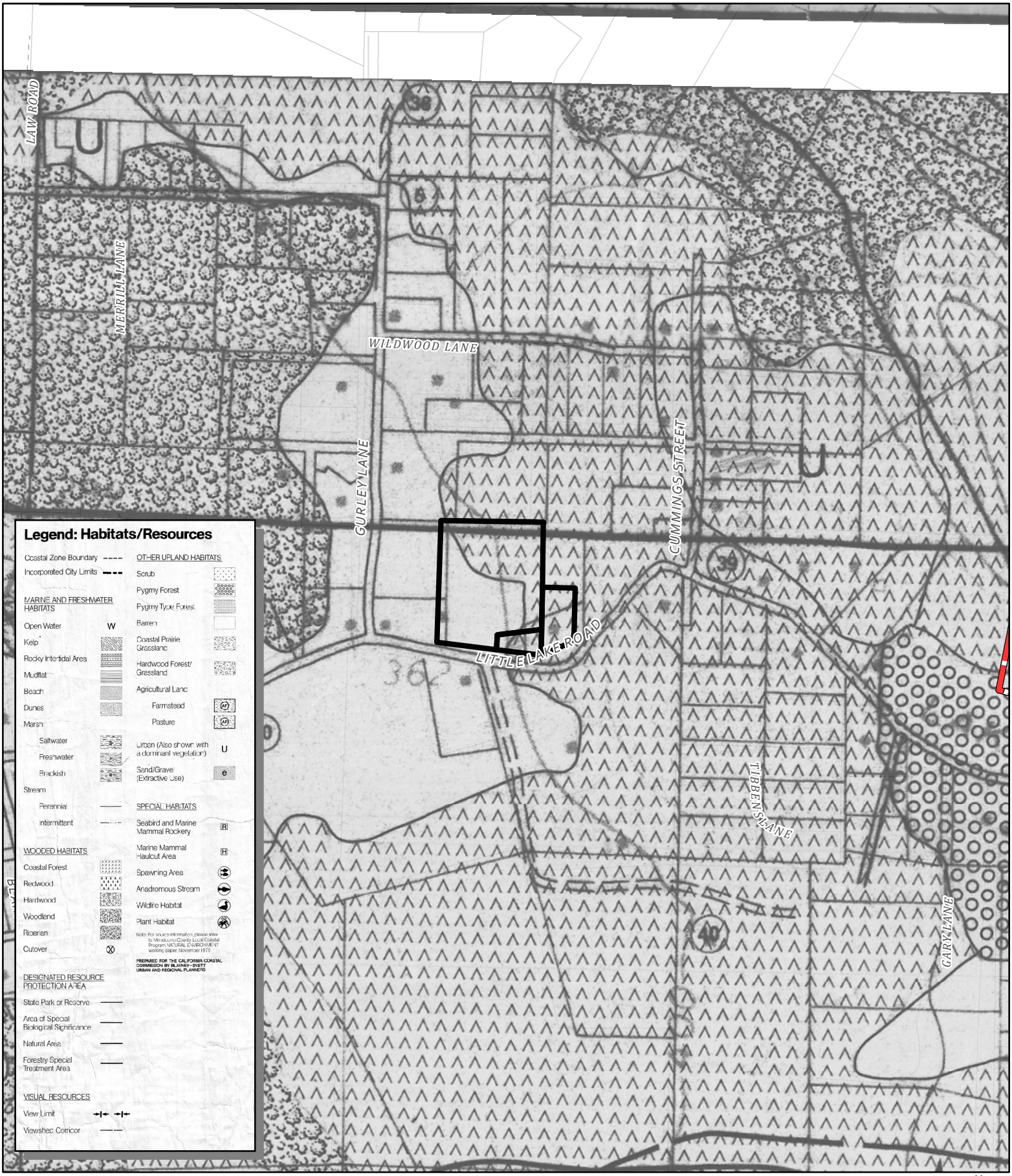
Coastal Zone Boundary
Public Roads
Private Roads
Assessors Parcels

0 270 540 Feet
0 0.05 0.1 Miles
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LCP LAND CAPABILITIES & NATURAL HAZARDS

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Legend: Habitats/Resources

Coastal Zone Boundary
Incorporated City Limits

MARINE AND FRESHWATER HABITATS
Open Water (W)
Kelp
Rocky Intertidal Area
Mudflat
Beach
Dunes
Marsh
Saltwater
Freshwater
Brackish
Stream
Perennial
Intermittent

WOODED HABITATS
Coastal Forest
Redwood
Hardwood
Woodland
Riparian
Cutover (X)

DESIGNATED RESOURCE PROTECTION AREA
State Park or Reserve
Area of Special Biological Significance
Natural Area
Forestry Special Treatment Area

VISUAL RESOURCES
View Limit
Viewshed Corridor

OTHER UPLAND HABITATS
Scrub
Pygmy Forest
Pygmy Type Forest
Barren
Coastal Prairie Grassland
Hardwood Forest/ Grassland
Agricultural Land
Farmstead (AF)
Pasture (AP)
Urban (Also shown with a dominant vegetation) (U)
Sand/Gravel (Extractive Use) (e)

SPECIAL HABITATS
Seabird and Marine Mammal Rookery (R)
Marine Mammal Haulout Area (H)
Spawning Area
Anadromous Stream
Wildlife Habitat
Plant Habitat

Note: For source information, please refer to Mendocino County Local Coastal Program NATURAL ENVIRONMENT working paper November 1978

PREPARED FOR THE CALIFORNIA COASTAL COMMISSION BY BLAYNEY-DYETT URBAN AND REGIONAL PLANNERS

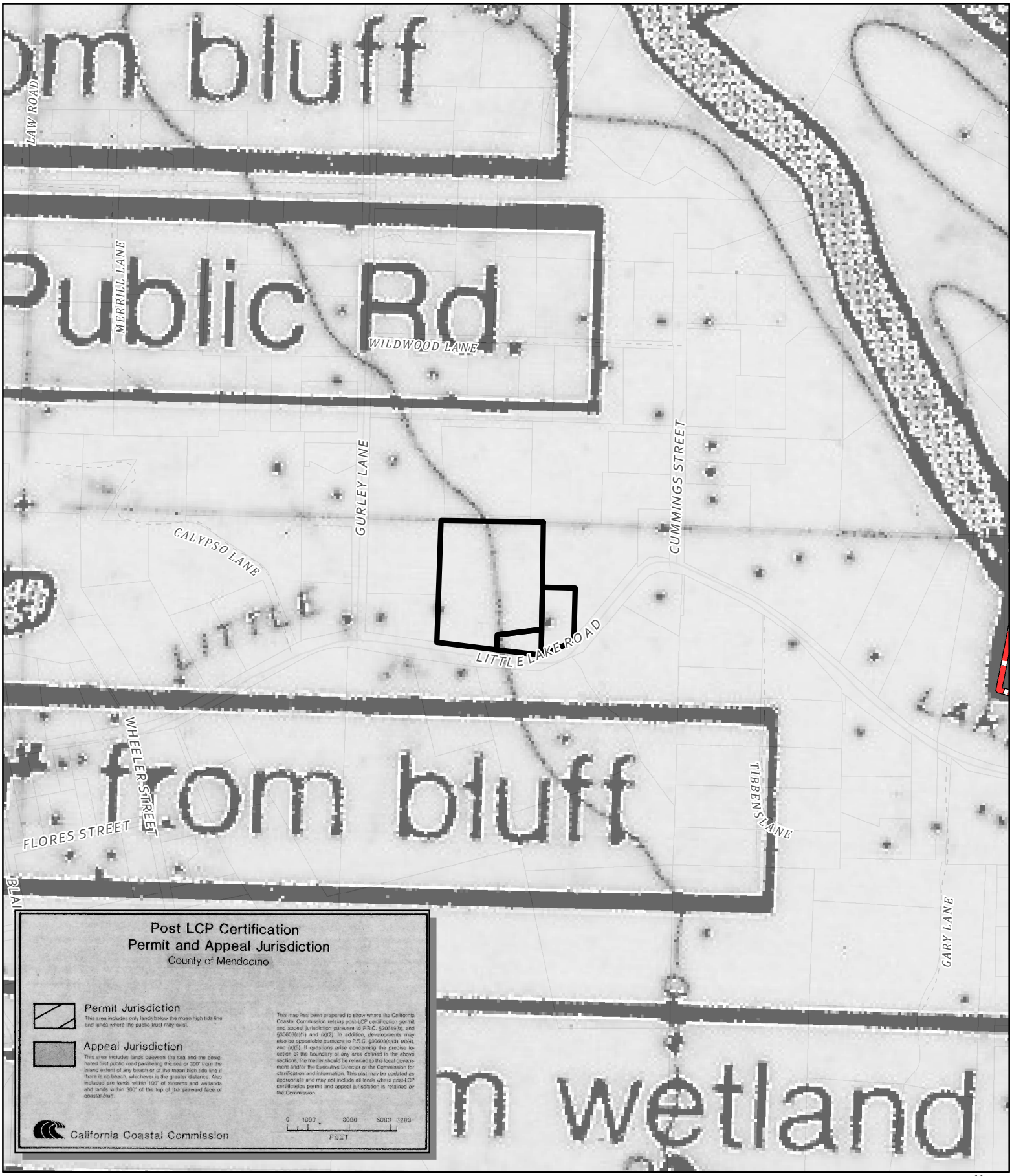
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Coastal Zone Boundary
Assessors Parcels
Public Roads
Private Roads

0 270 540 Feet
0 0.05 0.1 Miles
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LCP HABITATS & RESOURCES

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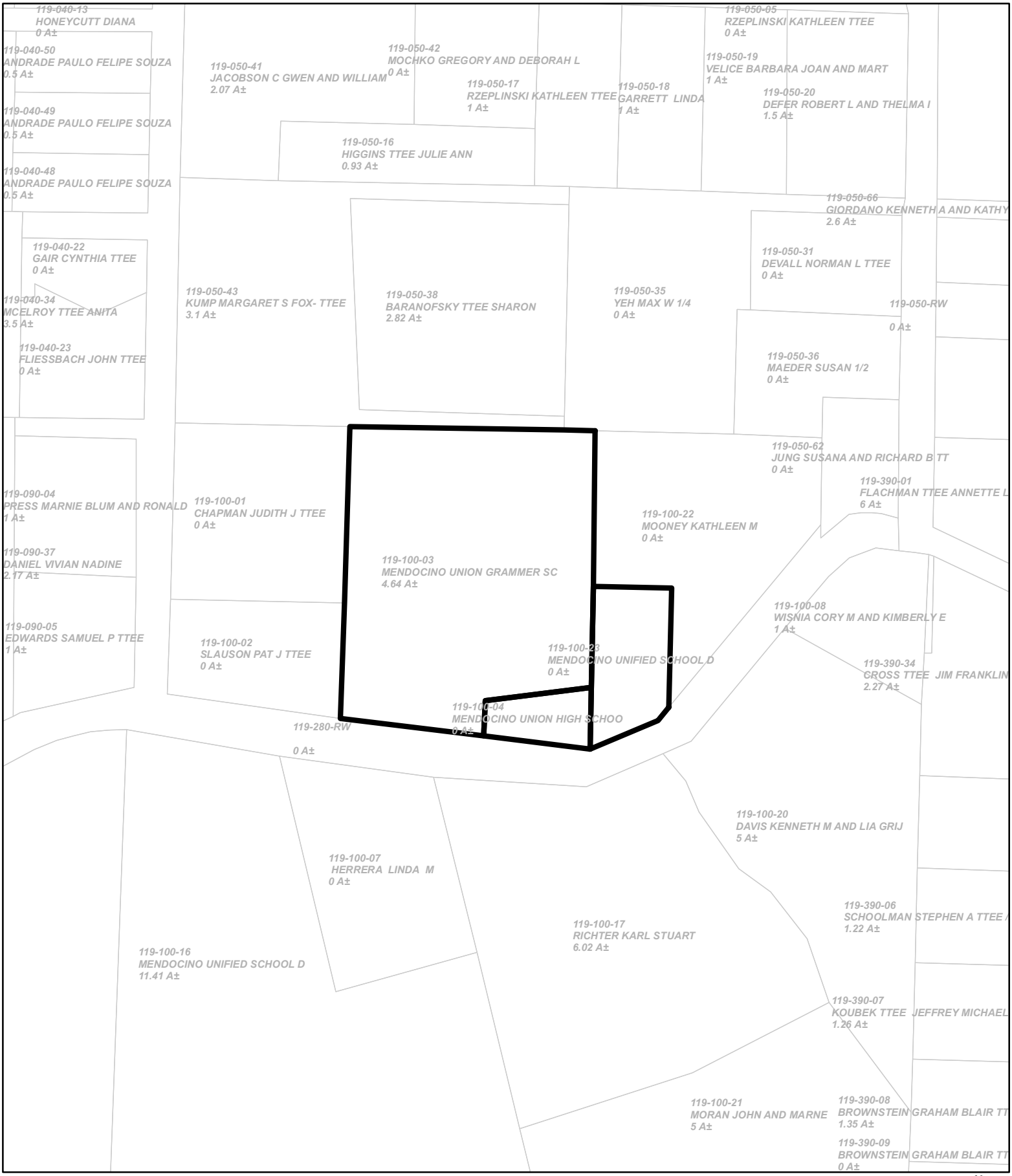
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Coastal Zone Boundary
Assessors Parcels
Public Roads
Private Roads

0 270 540 Feet
0 0.05 0.1 Miles
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POST LCP CERTIFICATION & APPEAL JURISDICTION

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Assessors Parcels

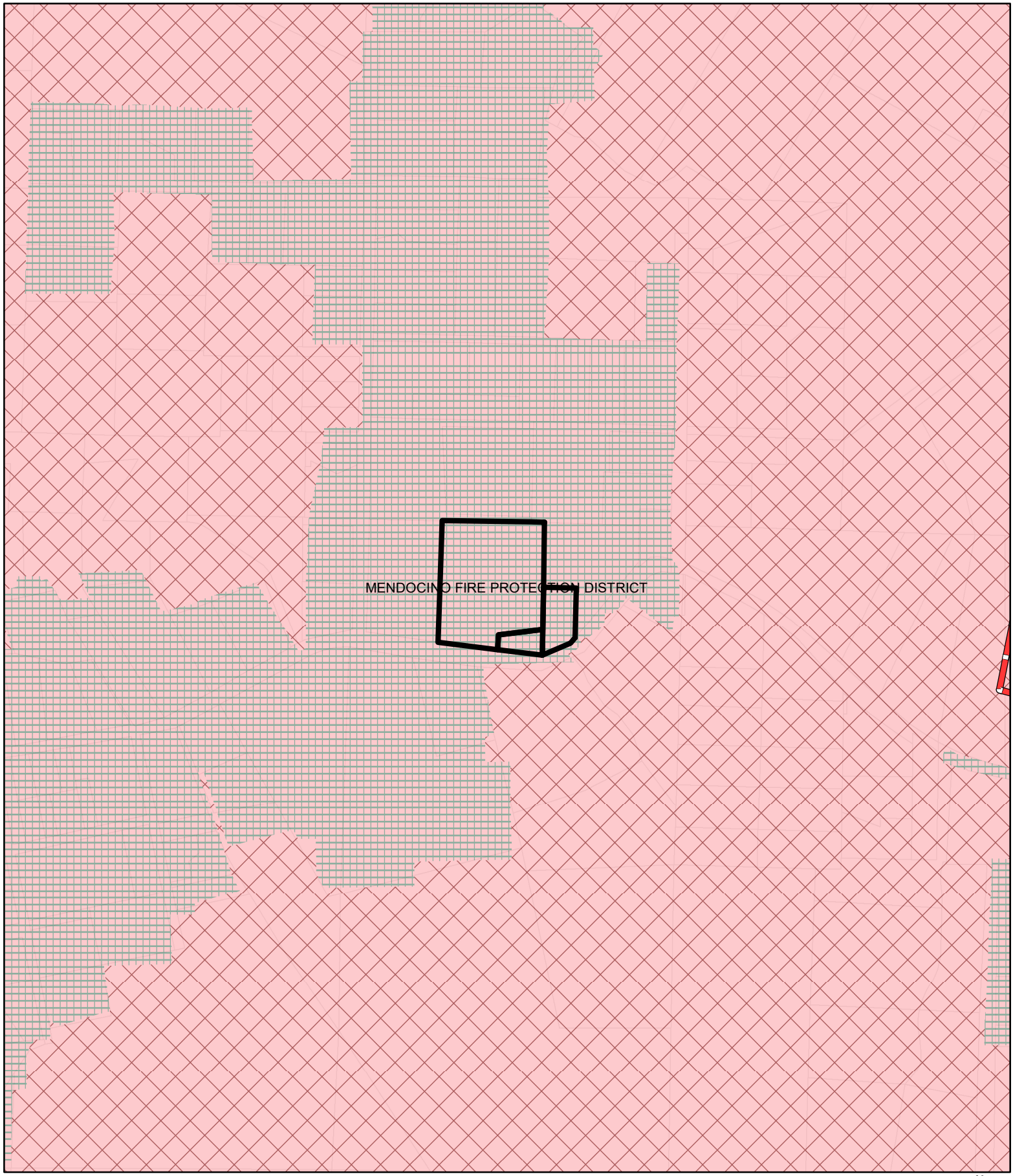
0 112.5 225 Feet
0 0.02 0.04 Miles

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ADJACENT PARCELS

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APLCT: Mendocino Unified School District
AGENT: Matt Kennedy
ADDRESS: 44020 Little Lake Rd, Mendocino

Coastal Zone Boundary
High Fire Hazard
Moderate Fire Hazard
County Fire Districts
Assessors Parcels

0 270 540 Feet
0 0.05 0.1 Miles

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FIRE HAZARD ZONES & RESPONSIBILITY AREAS
STATE RESPONSIBILITY AREA

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Coastal Zone Boundary

Assessors Parcels

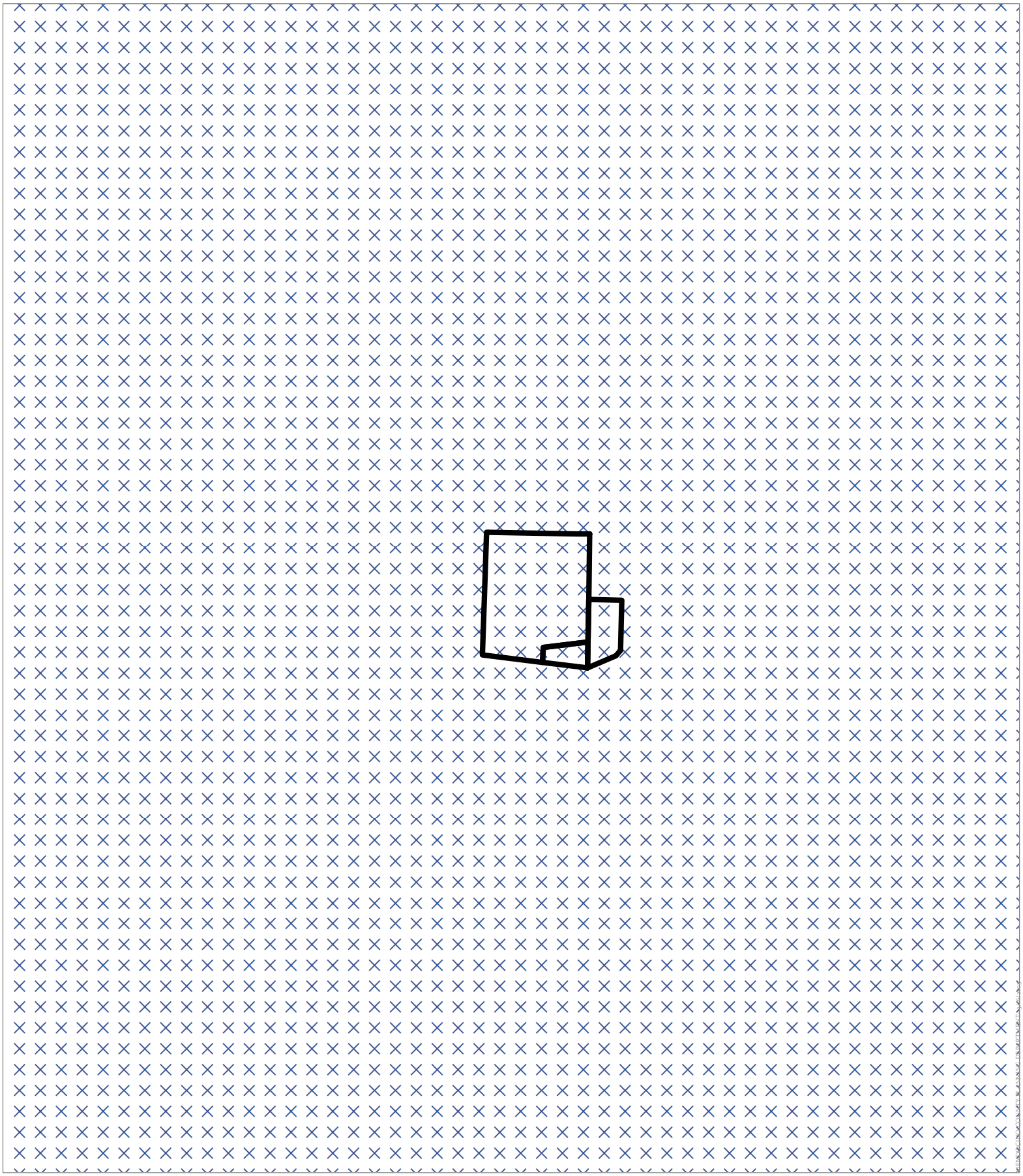
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WILDLAND-URBAN INTERFACE

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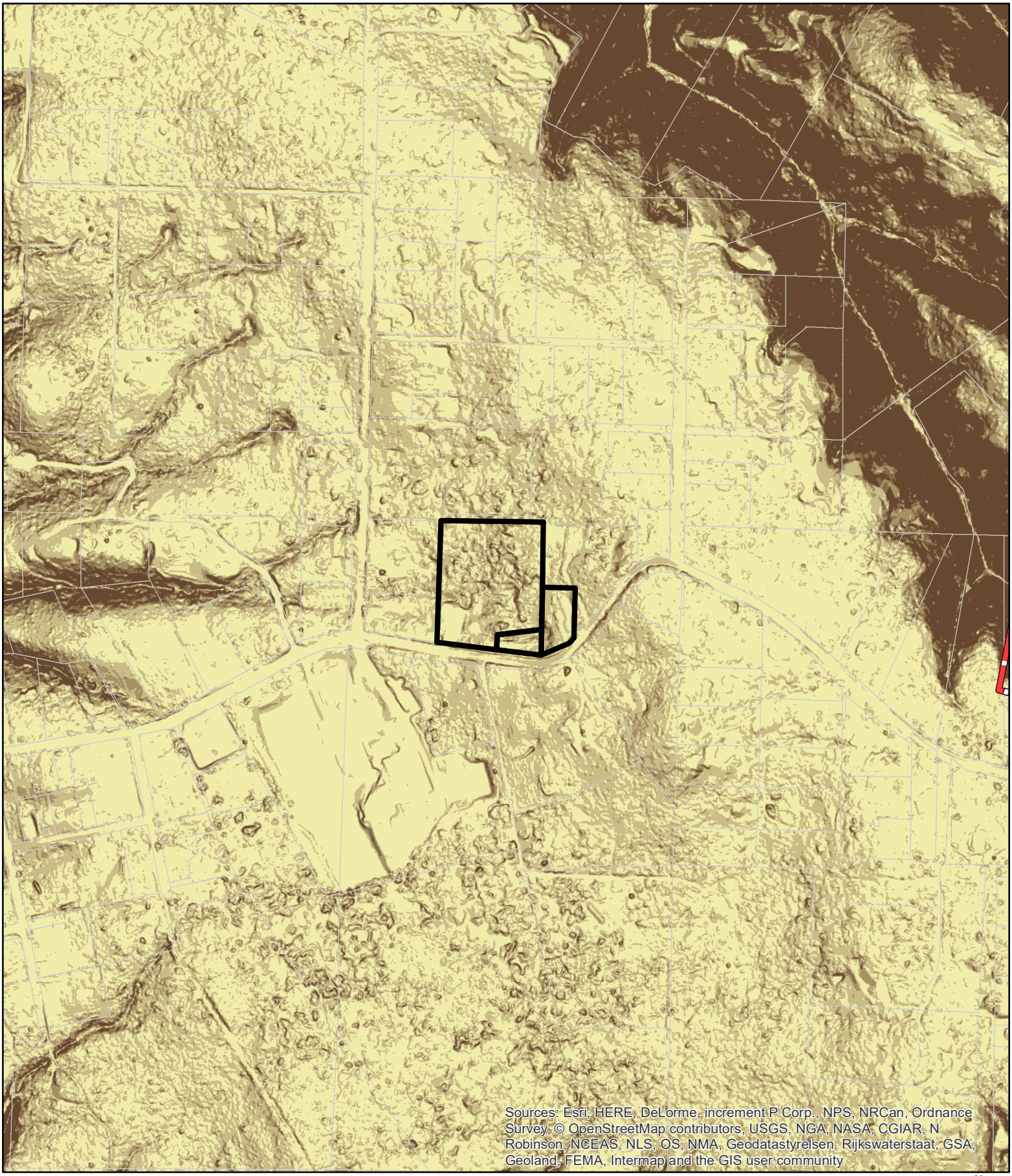
CASE: UM 2024-0008
OWNER: Mendocino Unified School District
APN: 119-100-03, 04 & 23
APLCT: Mendocino Unified School District
AGENT: Matt Kennedy
ADDRESS: 44020 Little Lake Road

Critical Water Resources

0 250 500 Feet
0 0.045 0.09 Miles
1:6,000

COASTAL GROUND WATER RESOURCES

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Coastal Zone Boundary
Assessors Parcels
0 - 10%
10% - 20%
20% - 30%
30% - 40%
40% - 50%

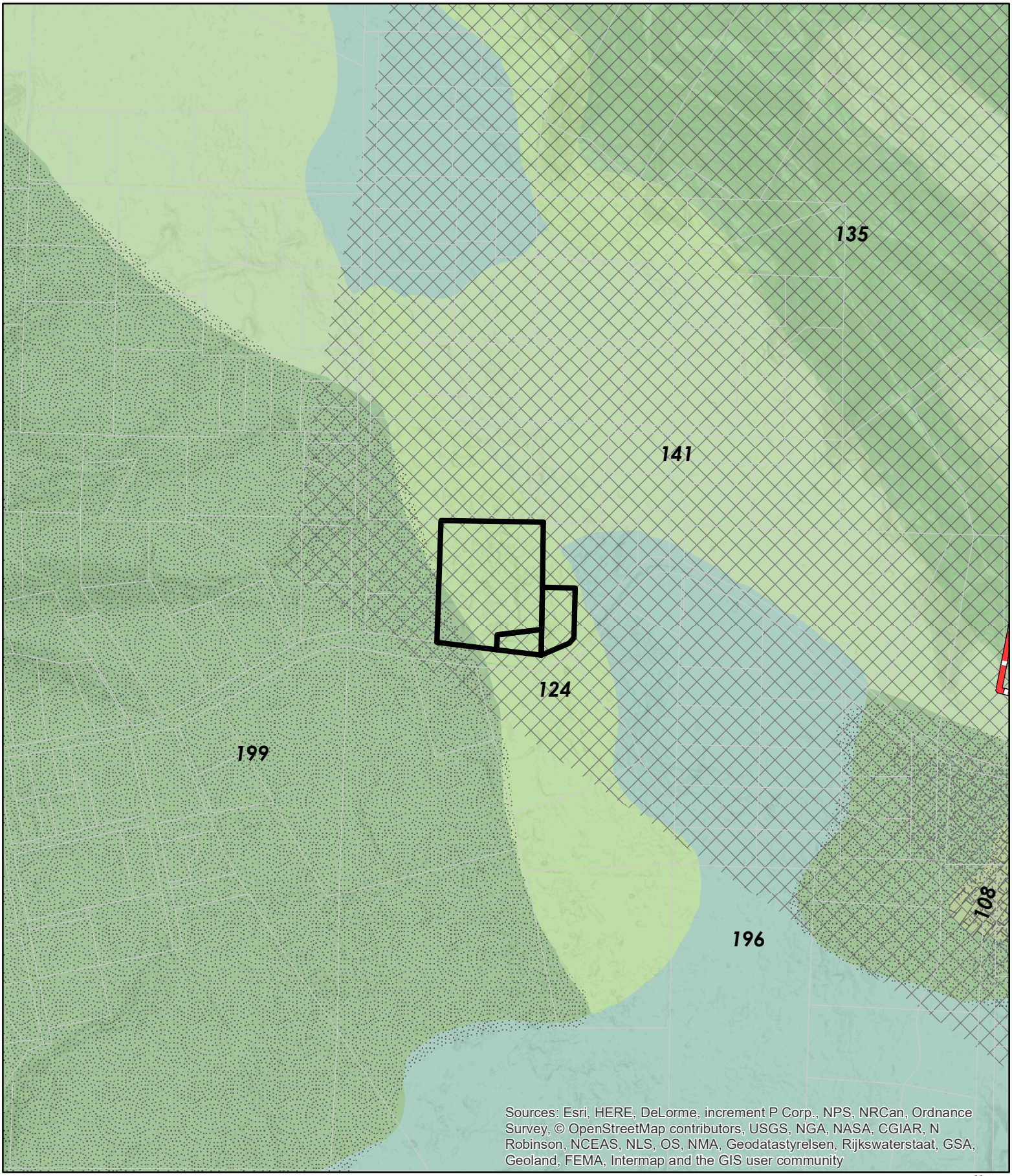
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ESTIMATED SLOPE

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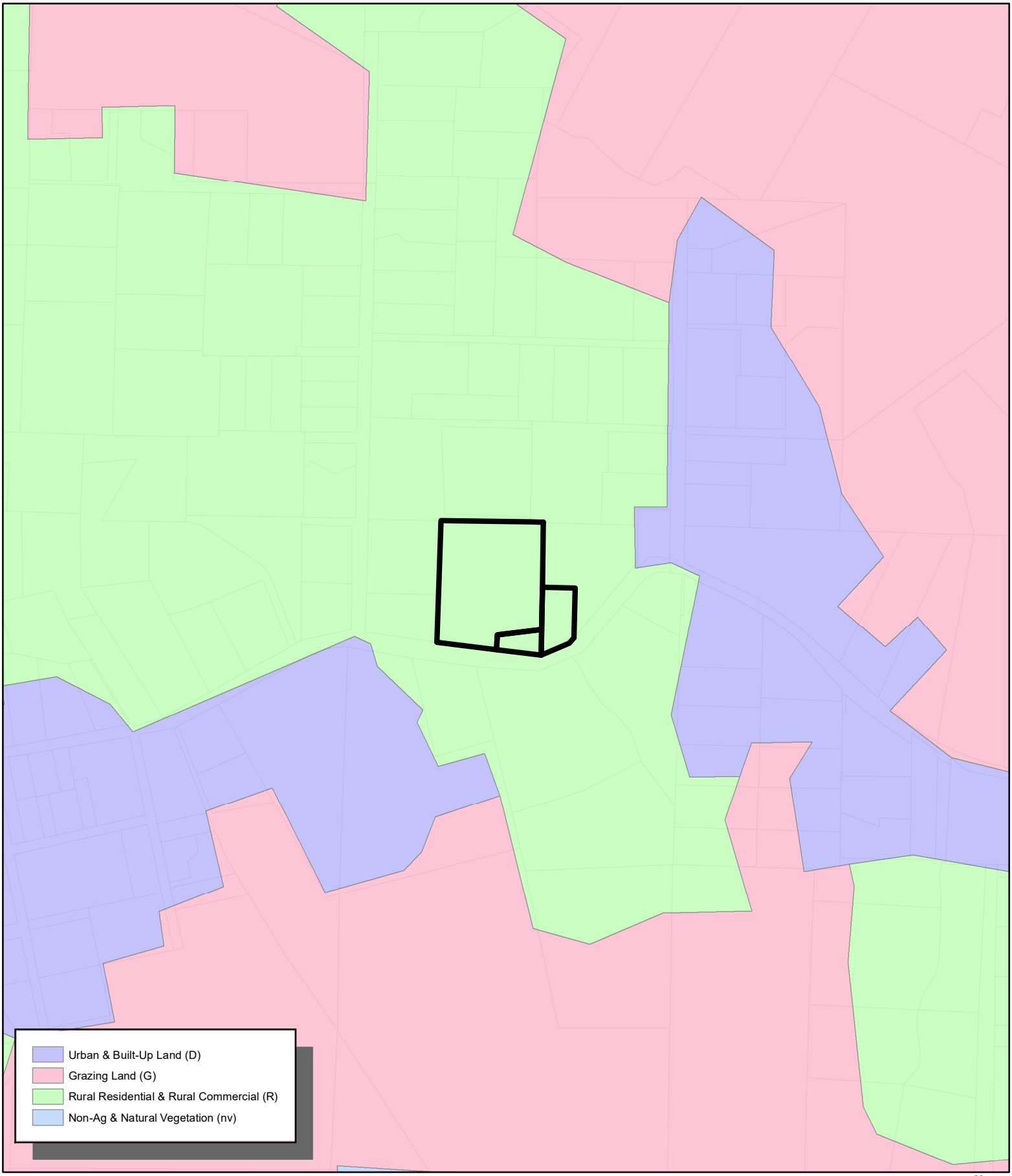
CASE: UM 2024-0008
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Coastal Zone Boundary
Assessors Parcels
Mendocino Cypress 110922
Blacklock & Aborigine
Shinglemill-Gibney Complex
Bishop Pine

0 270 540 Feet
0 0.05 0.1 Miles
N W E S
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WESTERN SOIL CLASSIFICATIONS

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Assessors Parcels

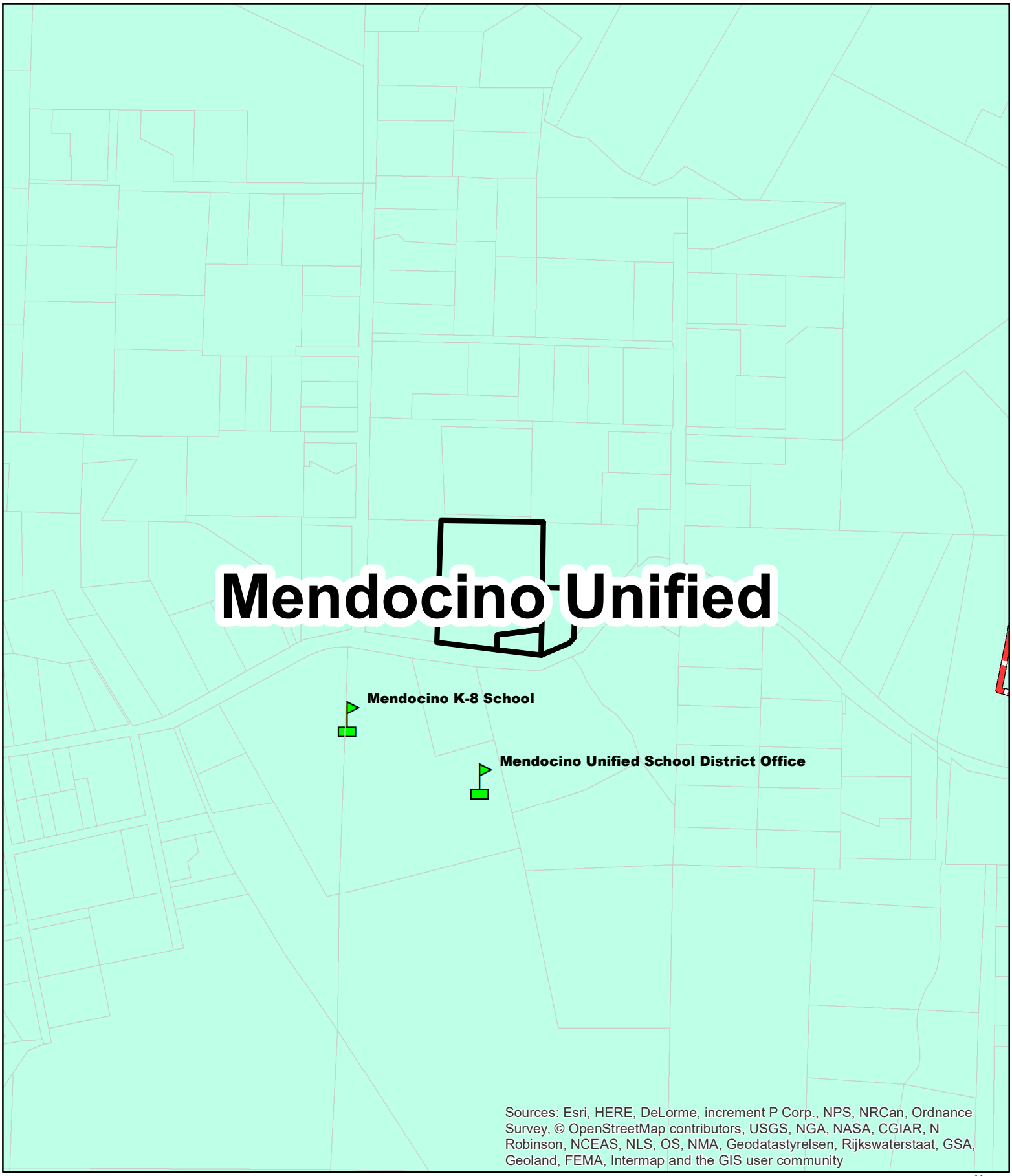
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IMPORTANT FARMLANDS

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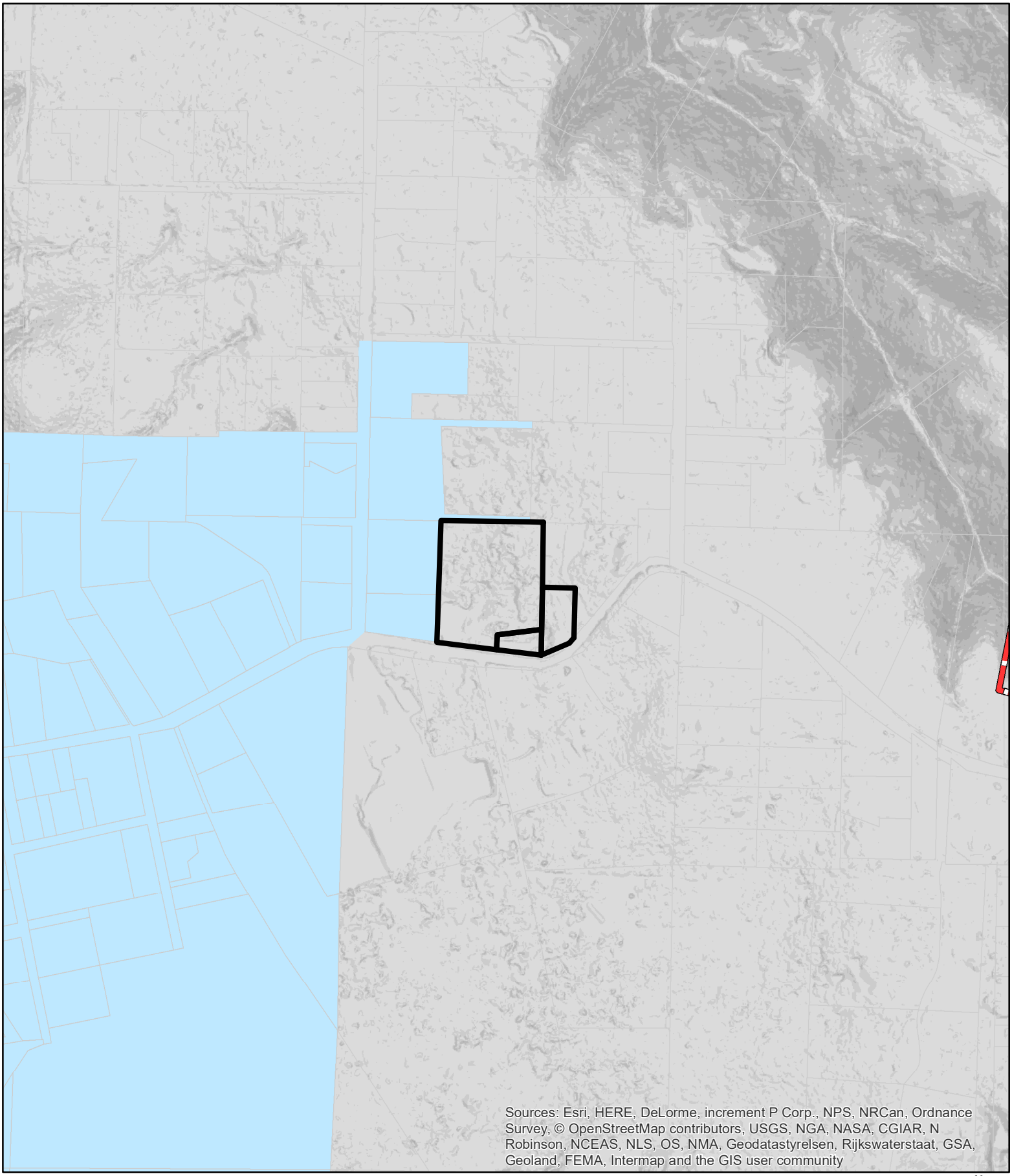
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Coastal Zone Boundary
Assessors Parcels
School Buildings

0 270 540 Feet
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SCHOOL DISTRICT

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Coastal Zone Boundary
Assessors Parcels
County Water Districts

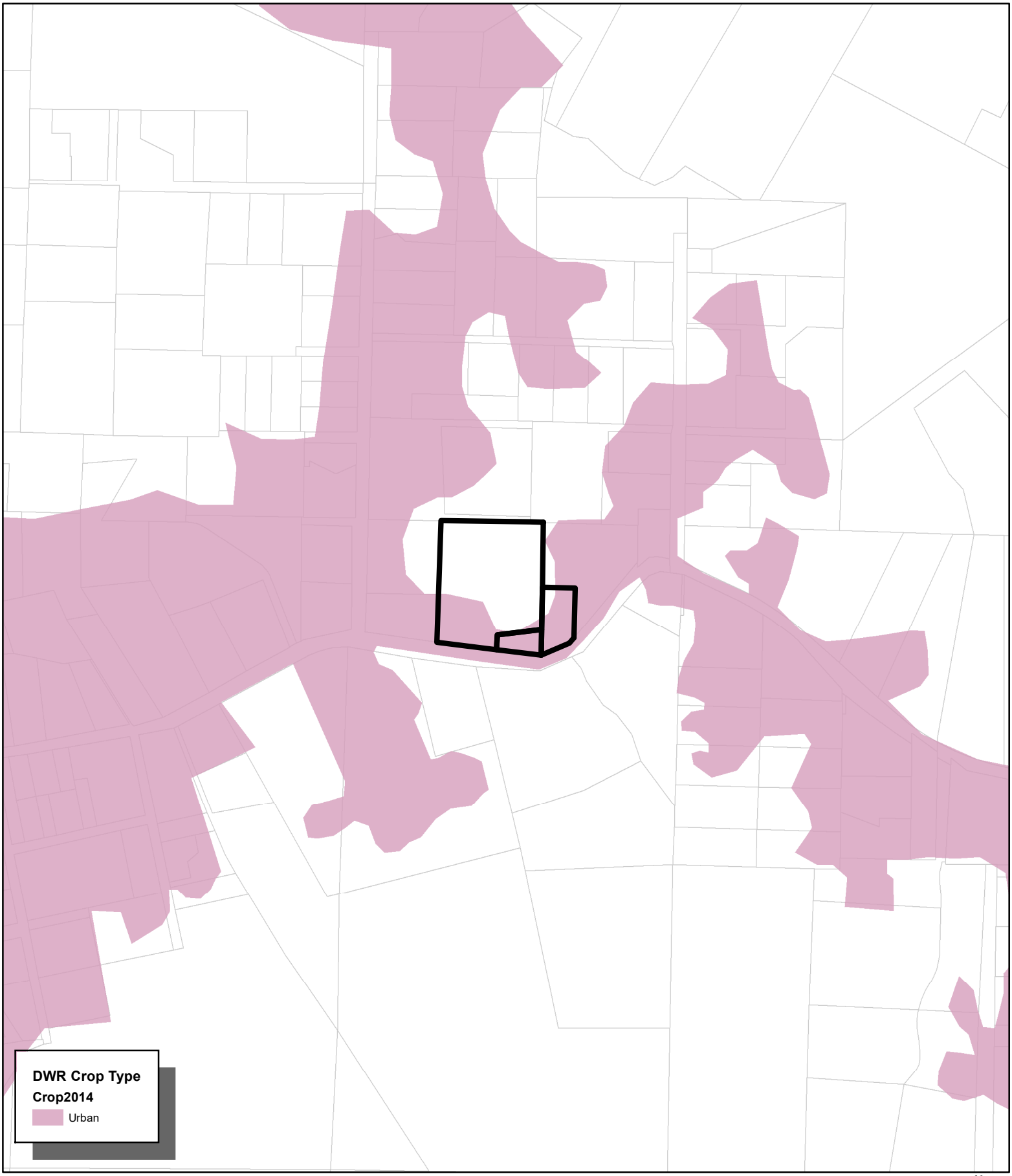
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WATER DISTRICT

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Assessors Parcels

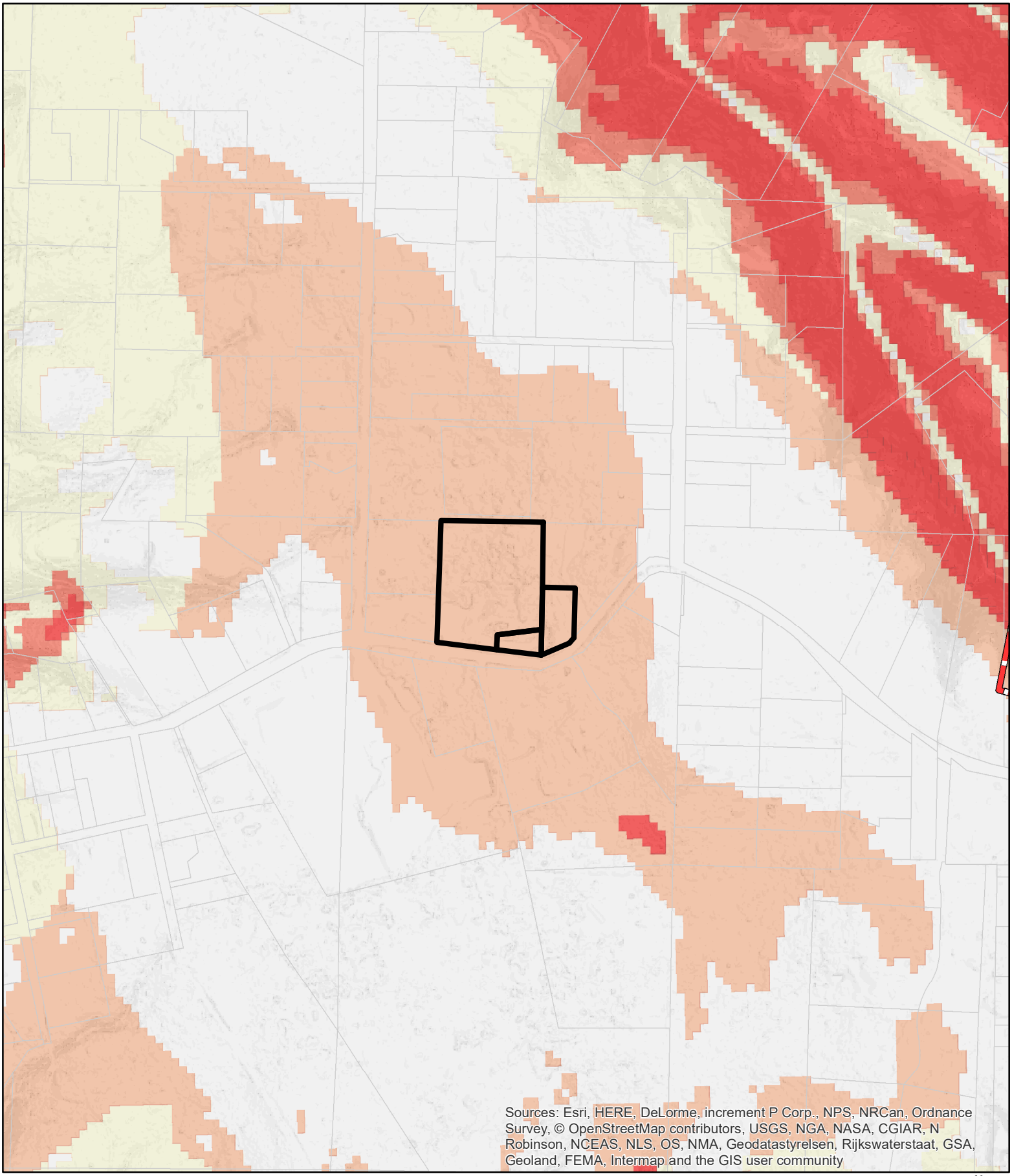
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CROP TYPES

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Coastal Zone Boundary
Assessors Parcels
0
0 - 5
5 - 7
7 - 8
8 - 10

0 270 540 Feet
0 0.05 0.1 Miles

N W E S

1:6,000

LANDSLIDE HAZARDS

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Mendocino Unified School District (MUSD)
Revised Water Supply and Storage Project

Supplemental Project Description in Support of CDP Amendment Application

Project Title	Water Supply and Storage Project
Applicant Name & Address	Mendocino Unified School District 44141 Little Lake Road, Mendocino, CA 95460
Applicant Contact Person & Phone Number	Jason Morse, Superintendent, Mendocino Unified School District (707) 937-5868 / **jmorse@mcn.org**
Authorized Representative	Matt Kennedy, Engineer, GHD, (707) 540-9687 **Matt.Kennedy@ghd.com**
Project Overview	Mendocino Unified School District is implementing water supply and storage improvements to address water system deficiencies identified by the State Water Resources Control Board (SWRCB) Division of Drinking Water (DDW) at its water supply and storage site located at 44020 Little Lake Road in the Village of Mendocino. As part of the Mendocino Unified School District's ongoing water supply and storage improvement project (U_2023-0004), two groundwater test wells were installed to collect data and assess source capacity. One well (TW 07) proved viable, yielding 6 gallons per minute (gpm) during a 72-hour pump test with minimal impact on nearby wells and favorable aquifer characteristics. Modeling showed negligible effects on surrounding domestic wells, and adding TW 07 would raise the District's total supply to 18 gpm, meeting regulatory requirements even with the primary well offline. The District now proposes converting TW 07 into a permitted production well for backup and seasonal tank filling, with associated infrastructure improvements.
Project Location	The Project site includes three MUSD-owned parcels (119-100-03, 04, & 23) located at 44020 Little Lake Road within unincorporated Mendocino County. The proposed test well to be converted to a production well is located on parcel 119-100-004.

Project Background

MUSD Water System Improvements

The MUSD owns, operates and maintains a potable and fire water system to serve its K-8 School, High School and District Office, as well as Friendship Park, the Community Center of Mendocino, and several irrigation areas affiliated with these primary consumers. The water supply and storage site is located at 44020 Little Lake Road in Mendocino.

A previous inspection conducted by the SWRCB DDW identified several system deficiencies, and key components of the MUSD's water system infrastructure have reached the end of their useful life. The MUSD prepared a Water System Plan Report (GHD 2020a) to address water system deficiencies and to evaluate alternatives for water sources, water storage and water treatment design. Based on the Water System Plan Report, the MUSD plans to improve its potable water system operations, including meeting regulatory requirements, making system improvements to meet long-term service needs, providing sufficient storage to meet NFPA and California Fire Code requirements, protecting the integrity of the water system, and ensuring the health and safety of students, faculty and public who rely upon the potable and fire water system.

Emergency Water Supply Test Wells

The drought of 2020-2022 was the worst multi-year drought in recorded State history. The ongoing drought highlights the need for improved water security in the face of climate change and natural disasters. The Mendocino City Community Services District (MCCSD) is the groundwater management authority within its service area boundary and is responsible for the management of the local aquifer to help prevent overdraft and maintain equitable access to groundwater for the residents, business, and property owners in the MCCSD service area. MCCSD has a Groundwater Management Program and Water Shortage Contingency Plan, but even with such plans in place, some wells in its service area run dry each summer and others cannot keep up with demand.

The recent drought also showed that MCCSD customers cannot wholly depend on neighboring water districts to meet water demand short falls during dry periods. During the most recent drought condition, approximately 28,000 gallons of potable water per day was being imported from other water districts to address water shortages within the MCCSD service area over a two-month period from late September to mid-November in 2021. During this period, up to 8 trucks loads of water per day was being transported into the MCCSD service area from the City of Fort Bragg and the City of Ukiah.

The availability of such emergency supplies in times of need is non-guaranteed. In 2022, MCCSD, in cooperation with the MUSD, received a grant in response to a drought scenario from the State of California Department of Water Resources through the Urban and Multibenefit Drought Relief (UMBDR) grant program (Agreement No. 4600014624) to help serve community emergency water needs. The UMBDR grant Agreement identifies the MUSD and MCCSD as Implementing Agencies and includes the development of 500,000 gallons of potable water storage at the MUSD's water supply and storage site, and the drilling of up to ten new groundwater supply test wells at the MUSD's water supply and storage site to explore the viability of an additional water source for emergency water supply purposes. Viable wells would also help to meet source production and supply reliability required by DDW.

Project Description for CDP Amendment

As part of an ongoing water supply and storage improvement project (U_2023-0004), two groundwater test wells were installed along the property frontage at the Mendocino Unified School District's water supply and storage site located at 44020 Little Lake Road in the Mendocino community. The test wells were installed to evaluate the viability of water source capacity and redundance, a key issue identified by the Division of Drinking Water for the District's water system.

One of the test wells, (TW 07), demonstrated viability as a water source by consistently yielding 6 gallons per minute during a 72-hour pump test, with minimal impact on nearby wells. Located in marine terrace deposits, the well showed favorable aquifer characteristics, including a transmissivity of 420 ft²/day, storativity of 0.0082, a specific capacity of 0.33 gpm/ft, and an efficiency of 18% at the tested pumping rate.

Modeling of drought and cumulative pumping scenarios showed negligible drawdown effects in nearby domestic wells, with projected impacts well within acceptable limits. With the addition of TW 07, the District's total available water supply would increase to 18 gpm, meeting the Division of Drinking Water's requirement of 17.7 gpm even with the highest-capacity well offline.

Based on these findings, the District proposes converting TW 07 into a permitted production well to serve as a supplemental source and to fill fire protection and water supply storage tanks during the wet season, without increasing overall water use. This would include installation of a submersible pump and the well head would be housed in an above grade locking enclosure. Underground piping and electrical would be installed to connect the well to the water treatment building and storage tanks.

Hydrological Study

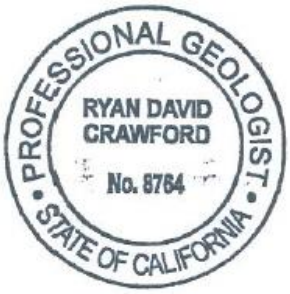
Drought Tolerance Emergency Water and Storage Improvements

Mendocino Unified School District

20 October 2025

→ **The Power of Commitment**







Project name		PW Drought Tolerance Emergency Water Supply and Storage Improvements					
Document title		Hydrological Study | Drought Tolerance Emergency Water and Storage Improvements					
Project number		12584992					
File name		Hydrological Study-MUSD Property.docx					
Status Code	**Revision**	**Author**	**Reviewer**		**Approved for issue**		
			Name	**Signature**	**Name**	**Signature**	**Date**
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1. Introduction

GHD Inc. (GHD) was engaged by the Mendocino Unified School District (MUSD) to prepare this report summarizing the results of a hydrological study of new wells and groundwater data collected by GHD in support of the MUSD Water Supply and Storage Project. The purpose of the information provided herein is to support the environmental review and permitting of one new production well (TW 07) on the MUSD property. This scope of work supports the Water Supply and Storage Project that is jointly supported by the MCCSD and MUSD and funded by the California Department of Water Resources Urban and Multibenefit Drought Relief Grant program and a California Water Resources Control Board Proposition 1 Drinking Water State Revolving Fund Grant.

The project Site is located on MUSD property located north of the K-8 School campus (APN 119-100-03, 119-100-04 and 119-100-23) and west of the school's existing supply wells and storage tanks, shown Figure 1. Groundwater data was collected from MUSD wells and near vicinity domestic wells using manual depth-to-water (DTW) meters and where possible, by installing continuous data logging pressure transducers directly within each well casing.

1.1 Scope and limitations

This report: has been prepared by GHD for Mendocino Unified School District and may only be used and relied on by Mendocino Unified School District for the purpose agreed between GHD and Mendocino Unified School District as set out in section 1 of this report.

GHD otherwise disclaims responsibility to any person other than Mendocino Unified School District arising in connection with this report. GHD also excludes implied warranties and conditions, to the extent legally permissible.

The services undertaken by GHD in connection with preparing this report were limited to those specifically detailed in the report and are subject to the scope limitations set out in the report.

The opinions, conclusions and any recommendations in this report are based on conditions encountered and information reviewed at the date of preparation of the report. GHD has no responsibility or obligation to update this report to account for events or changes occurring subsequent to the date that the report was prepared.

The opinions, conclusions and any recommendations in this report are based on assumptions made by GHD described in this report (refer section(s) 1 of this report). GHD disclaims liability arising from any of the assumptions being incorrect.

1.2 Previous Studies

GHD previously conducted a series of studies for MUSD for future additional production capacity and source water supply resiliency. These included a source water well inspection and specific capacity testing (GHD, 2019b), a well siting study (GHD, 2019c), a test well drinking water source assessment and protection and water quality study (GHD, 2020), construction of a new test well (MUSD Well 06) with pump and specific capacity testing (GHD, 2021), and two studies for the newest test wells (MUSD Test Wells TW 07 and TW 08) in the form of a hydrogeologic report (GHD, 2024) and a well siting study (GHD, 2023).

2. Estimated Water Allotment

This project does not propose an increase in annual water allotment or expected water use by MUSD. The proposed new production well (TW 07) will be used to meet the Division of Drinking Water requirement for MUSD to maintain sufficient source capacity to meet their maximum day water demand (MDD), 25,500 gallons (17.7 gallons per minute) as as reported in the Division of Drinking Water's August 23, 2016 Inspection of Findings. During the wet season wells may be used to refill the emergency fire and water supply tanks as conditioned in the Coastal Development Permit.

3. Hydrological Setting

The MUSD currently operates two active wells (MUSD Well 01 and MUSD Well 02) at the Site. GHD previously conducted a series of studies for MUSD for future additional production capacity and source water supply resiliency. These included a source water well inspection and specific capacity testing study (GHD, 2019b), a well siting study (GHD, 2019c), a test well drinking water source assessment and protection and water quality study (GHD, 2020), construction of MUSD Well 06 with pump and specific capacity testing (GHD, 2021), a Hydrogeological Report for the project location (GHD, 2024), and a well siting study for the new MUSD Test Wells 07 and 08 (GHD, 2023).

In addition to previous GHD studies, numerous hydrological studies were performed in the 1980s through at least the early 2000s by Don Clark Engineering and Hydrology, and other regional firms. Hard copies were reviewed by GHD as provided by several domestic well owners downgradient to the MUSD.

The MCCSD monitors precipitation and groundwater (since at least 2002) within the MCCSD service district area. In an effort to monitor water resources they also used and annually updated a computational groundwater model developed and maintained by Todd Groundwater (Todd) through 2022. The MCCSD service area and a number of monitoring wells located west of the project area are shown in Figure 1.



Figure 1 MCCSD Monitoring Well Locations (TODD 2021)

In addition to the monitoring wells, data has previously been collected from private water supply wells, shown in Figure 2, that were also incorporated into the MCCSD groundwater model.



Figure 2 Private Water Supply Wells Identified by MCCSD (TODD 2021)

The project location is adjoining the northeast boundary of the groundwater model, however some of eleven documented private wells within the MCCSD boundary are within the vicinity of this project and were reviewed as potential continuous data monitoring locations.

3.1 Topographic Setting

The Site is located approximately 1 mile east of the Pacific Ocean on the Mendocino Headlands, on the outskirts of the village of Mendocino. The Mendocino Headlands consist of a series of relatively flat terraces that form benches into the surrounding bedrock. The headlands protrude approximately ½ a mile into the Pacific Ocean and terminate with nearly vertical cliff faces that generally extend between 40 and 60 feet above sea level.

The Site is situated on the north side of Little Lake Road, approximately 0.7 miles east of the intersection of Little Lake Road and State Route 1 at an elevation ranging from 385- to 425- feet NAD88. The Site slopes to the west at a consistent 10 percent grade and is heavily forested throughout with exception to the southwest corner where there is an existing MUSD maintenance building and driveway that leads east to the existing MUSD wells and water tanks.

3.2 Geologic Setting

Regional geology of the project area consists of the Coast Ranges geomorphic province which is comprised of northwest-trending mountain ranges, typically between 2,000- and 4,000-feet above sea level. The northern Coast Ranges are dominated by irregular, knobby, landslide-topography of the Franciscan Complex that in large areas are overlain by volcanic cones and flows of the Quien Sabe, Sonoma and Clear Lake volcanic fields (CGS, 2002). Ongoing tectonic forces resulting from the collision of the North American Plate with the Pacific Plate have created a broad zone of active, dormant, and inactive faults that are dominated by the San Andreas Fault system which trends along the western coast of the County, the Maacama Fault zone running parallel to State Route 101, and the Bartlett Springs Fault system that runs through Lake Pillsbury. The fault system results in a north-western structural alignment that controls the overall orientation of Mendocino County's ridges and valleys through a series of thrust faults, smaller

right lateral faults, the largest documented and active on-land fault ruptures being the San Andreas Fault located approximately 22 miles to the south at State Route 1 and Alder Creek and the Maacama Fault zone located approximately 24-miles west of the Site.

The Site is located on Pleistocene aged marine terrace deposits that are underlain by Franciscan Complex Coastal Belt. A relatively shallow organic soil horizon overlays the terrace deposits that range from 1- to 4-feet in depth. Marine terraces represent former beach and near shore environments and consist of silty sand that form essentially flat stratigraphic surfaces that cover the underlying Franciscan bedrock (DWR, 1985). There are four primary marine terraces that have been documented by Todd and others that constitute the Mendocino Headlands aquifer:

- **Casper Point**: Occurs between elevation of 40- to 80-feet elevation and is the youngest terrace (approximately 100,000 years old). The terrace is composed of medium-grained loose sand with few fines and is generally about 10 feet thick.
- **Jughandle Terrace**: Occurs between 80- to 160-feet elevation and is the second youngest terrace (about 200,000 years old). The terrace is composed of fine-grained silty sand and is generally about 20 feet thick with a maximum thickness of 35 feet.
- **Railroad Terrace**: Occurs between 160- to 200-feet elevation and is the third youngest terrace (about 300,000 years old). The terrace is composed of fine-grained sand with a higher percentage of silt and clay than the younger terraces.
- **Fern Creek Terrace**: Occurs between 300- to 400-feet elevation and is the oldest marine terrace (about 400,000 years old). The terrace is composed of fine-grained silt and clayey sand and is generally up to 15 feet thick.

Franciscan bedrock consists of interbedded greywacke sandstone and shale that is pervasively fractured. The bedrock holds very little potential for water storage however the fractures allow for groundwater storage and transmissivity and is generally understood to decrease with depth and distance from the coastline (DWR, 1985).

The Site is located beyond the traditionally mapped extent of the Fern Creek Terrace, located approximately ¼ mile northeast. Nearby well completion reports and onsite borings indicate that the alluvial thickness on the western half of the site is similar to that of the Fern Creek Terrance (around 15 feet) however there is a grade break that increases the elevation by approximately 30 feet which directly translates to increase of the marine terrace thickness to approximately 50 feet. This increase could be an unmapped separate marine terrace.

3.2.1 Site Hydrogeological Conceptual Groundwater Model

Briefly developed here from this study and review of previous studies, is a general hydrogeological conceptual model (HCM) for groundwater underlying the Project Site and the immediate vicinity aquifers downslope. This is intended to aid in the design of the proposed test wells recommendations and for future surface and groundwater monitoring protocols.

Directly down gradient of the study area (MUSD) and to the west are three principal aquifer types – alluvial aquifers, marine terrace aquifers, and Franciscan bedrock aquifers. The marine terrace (Fern Creek Terrace or separate older terrace) of up to 50-feet thick occupies the MUSD parcel and transmits relatively shallow groundwater within a generally unconfined aquifer ranging in approximately 10- to 30-feet of aquifer saturated thickness (location, seasonally, and rain type year dependent) that flows to the west. Locally confined conditions are observed due to the overlying silt and clay from the ground surface that ranges from approximately 10- to 20-feet in thickness. The three existing MUSD wells are constructed up to 50-feet deep and have the highest relative specific capacities and long-term yields in the nearby area, ranging from approximately 6 to 9 gallons per minute (gpm). This older marine terrace thins immediately to the west as the topography lowers, and a few springs and wetlands emerge downslope where the marine terrace has been naturally eroded from surface water incision and bedrock is correspondingly encountered at shallower depths. Bedrock forces groundwater to the surface of the thin marine terrace portions, as evident in the springs located west of the MUSD water tanks and east of the MUSD maintenance building and flow year-round, even during severe droughts as groundwater levels decline over the summer months. These springs represent a portion of Slaughterhouse Gulch headwaters and its first surface flows in the immediate area. Another distinct spring fed branch

to Slaughterhouse Gulch begins offsite approximately 1,000-feet to the northwest on the northeast portion of Gurley Lane. The two spring systems flow westerly downslope and converge near Calypso Lane to form the defined Slaughterhouse Gulch stream, with year-round surface flows even during periods of severe drought.

The alluvial (creek) deposits are thought to be generally 10 to 20-feet or less, in thickness and have formed from overland flow incising and eroding the various upland marine terraces. This is shown in the numerous older caisson wells installed in or adjacent to Slaughterhouse Gulch which are generally less that 20-feet deep. The relatively thin and shallow alluvial aquifers have developed from the deposition, erosion, and redepositing cycle of those sediments along the creek banks and gulches as the surface water has migrated westerly to the Pacific Ocean over time. The alluvial groundwater is a very shallow unconfined aquifer that ranges from approximately 5 to 15-feet in saturated thickness.

The Site and lower elevation marine terraces and alluvial terraces are underlain by Franciscan hard rocks of graywacke to slatey materials of relatively very low permeability and transmissivity, that also contain variable aquifer properties with groundwater that moves via fracture flow. The Franciscan rocks have variable long-term yields in wells, approximately ranging from 0.1- to 3-gpm in near vicinity wells, have variable to unknown total depths of groundwater, have a relatively low storage potential, and are recharged much more slowly by the overlying marine and alluvial terraces over longer periods of time. Bedrock completed wells generally range from 100 to 300-feet or more in depth, and likely exhibit mostly confined to semi-confined conditions.

3.3 Hydrologic Setting

The Mendocino Headlands aquifer is located within the Sustainable Groundwater Management Area designated the Fort Bragg Terrace Area which does not have a current Groundwater Sustainability Plan, however, the wells and aquifer within the MCCSD service area are regulated by MCCSD which maintains a Groundwater Sustainability Plan. The project site and wells are located outside of the MCCSD service area and are within the jurisdiction of the County of Mendocino. The Fort Bragg Terrace Area is a series of discontinuous uplifted marine terrace deposits located along the Mendocino County coastline (DWR, 2004).

The primary method of recharge for the aquifer is precipitation infiltration with excess surface runoff flowing into creeks and ultimately the Pacific Ocean to the west. Areas that have exposed bedrock tend to have poor infiltration rates resulting in the alluvial and marine terraces being primary recharge and storage areas. Due to the topographic setting of the Mendocino Headlands, a major portion of the annual groundwater outflow is through shallow springs along the surrounding cliffs resulting in the shallow aquifer(s) having reduced long-term storage capacity and influenced by the annual weather patterns much more than typical alluvial California aquifers. This means that, in general, the Mendocino water supply is very closely associated with year-to-year precipitation and is vulnerable to short period (single and multi-year) droughts. Annual average rainfall for the village of Mendocino is about 40-inches with 97 percent of annual rainfall occurring in the rainy season (October to May). Annual rainfall records spanning from 1901 to 2025 are shown in Figure 3.

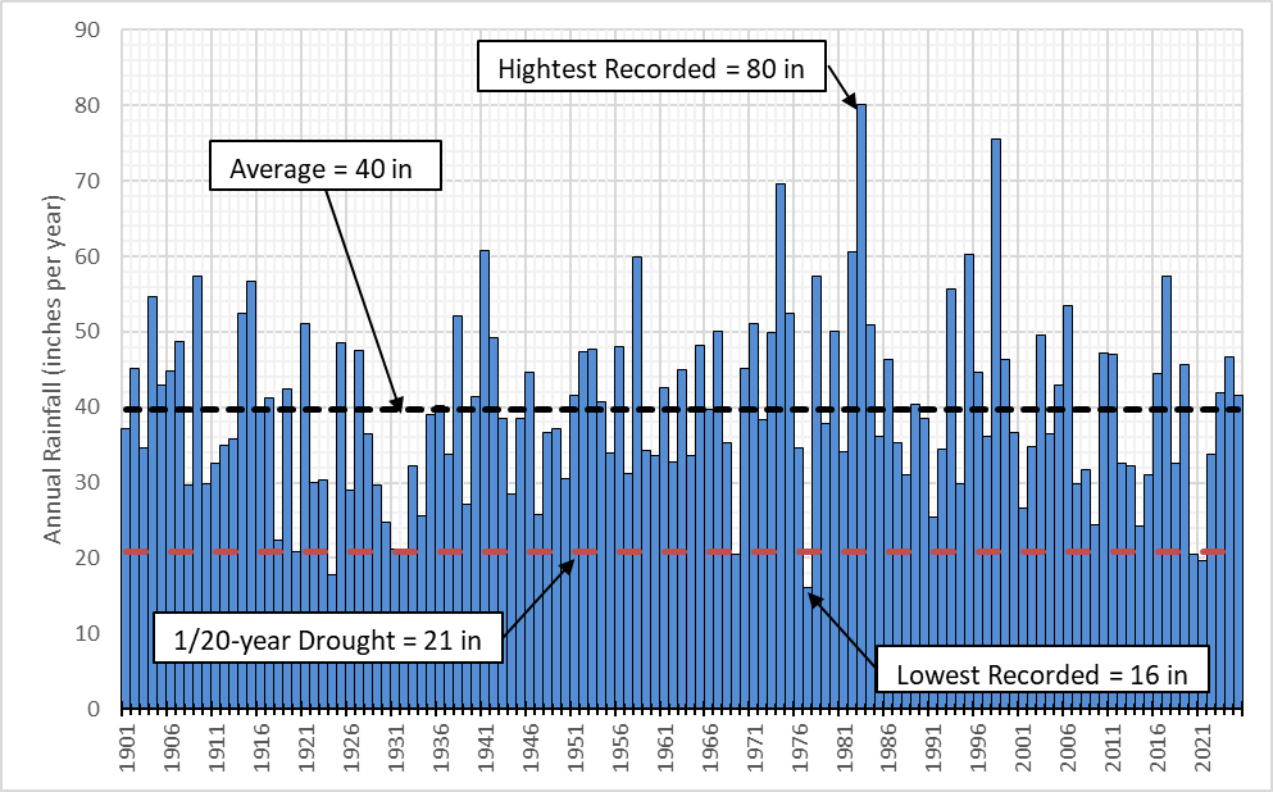


Figure 3 Mendocino Annual Rainfall from 1901 to 2025

Topography and groundwater flow to the northwest towards Slaughterhouse Gulch and is disconnected from the Big River Watershed located south of the village of Mendocino. Groundwater levels are typically lowest in the fall prior to the first substantial rainfall of the rainy season and they begin to rise after about 9-inches of precipitation (DWR, 1985). Due to its small area, the Slaughterhouse Gulch groundwater basin divide is estimated as the approximate watershed boundary, which is located about 800-900 feet east and 1,800 feet north of the Project Site. North and east of this divide is the Jack Peters Gulch watershed.

During droughts, the highest groundwater levels occur during the winter and are several feet lower than the same months in an above average rainfall year. During severe droughts, the average depth-to-water falls below 20 feet and results in several of the very shallow wells going dry in the area. The dry wells are generally old, sub-standard, shallow, hand-dug, or near the basin divide where there is less tributary area. These wells can be a threat to water quality and can act as a conduit for bacteria and other contaminants into the aquifer. Modern wells in the immediate vicinity of these shallow wells generally do not go dry. Groundwater pumping within the MCCSD boundaries is generally metered for both commercial and domestic uses with total annual extractions for the region ranging from 65 to 74 acre-feet over the span of 2016-2022 (Todd 2022).

3.4 Existing Wells

On the MUSD property there are three existing production wells (Wells 01, 02, and 06) with Wells 01 and 02 in use and Well 06 offline (recently equipped and slated to be brought into service). In addition to the production wells there are two old, decommissioned caisson wells that are no longer in use by the school, called here in this study the North and South Caisson wells (also referred to as “abandoned well” on other GHD project design drawings) that are located near the headwaters of the south fork of Slaughterhouse Gulch. Both caisson wells are of concrete construction, approximately 3-feet in diameter, and are 29-feet deep.

3.5 Constructed Wells

Three locations onsite were drilled for potential new wells, labelled MUSD Test Wells 07, 08 and 09. Test wells were drilled and constructed by Clear Heart Drilling between August 7th through the 13th. Of the three locations, one test well was not constructed (Test Well 09) due to a lack observed groundwater and shallow bedrock and the boring was subsequently backfilled with cement grout after drilling. Test Wells 07 and 08 were drilled to depths of 40 and 30-feet, respectively, and constructed with 20-foot sanitary seals approved by the Division of Drinking Water. Free standing water was found at approximately 20 feet below ground surface for both wells. Geologic logs and well construction details for the borings and constructed test wells are shown in Appendix A. Following construction, wells were developed through air lifting and purging.

4. Performance of Pump Test

4.1 Public Notice

On June 5, 2025, property owners within ¼ mile of the project site were notified of the construction of the test wells and the corresponding 72-hour pump tests required. Mailing addresses were obtained from county parcel records and a total of 112 letters were sent out. Of the 122 sent, 68% certified received, the remaining were returned to sender. Outreach letters notified property owners of the upcoming pump tests and invited them to opt into a monitoring program to establish background groundwater levels within their wells and monitor their water levels during the testing. Several of the returned to sender owners separately reached out prior to the well testing and their wells were included in the monitoring program.

On August 8th, notices of the upcoming tests were posted at the project location, MCCSD office, and around the village of Mendocino, and on August 14th, a notice of the upcoming pump test was published in the Mendocino Beacon. Outreach letters and the public notice are included as Appendix B.

Upon notice to GHD that a well owner was interested in being included in the monitoring, correspondence and updates of the pump testing were provided via email and phone calls and information of their wells were requested from them by GHD (Well Completion Reports and any previous hydrologic studies).

4.2 Pump Test Method

The pumping test method for MUSD TW 07 was a constant rate 72-hour pumping test, in accordance with the Mendocino County Coastal Groundwater Development Guidelines and the MCCSD Ordinance 2020-1. Groundwater levels were measured using digital data loggers (transducers) that measured pressure and temperature at short intervals (ranging from 1 minute in the pumping wells to 1 hour in distant wells monitored) to monitor groundwater levels before, during, and after the 72-hour pump test. Baseline groundwater level recordings were initiated by GHD starting July 2025.

MUSD test well TW 07's pump test was performed from September 3rd through the 6th by Clear Heart Drilling with oversight by GHD staff. Onsite wells were turned off 24 hours prior to the start of the test to allow for groundwater levels to recover before the pump test. Private well owners in the monitoring program were asked to not use their wells 24-hours before or during the test to best observe potential drawdown effects.

A temporary submersible pump was installed at a depth of approximately 38-feet below the ground surface for the test. The pump was equipped with a check valve to prevent backflow at the completion of the test. A totalizer and flow meter was used to monitor the pumping rate and the total volume of water pumped from the test well. The pump test began at 11am with a pumping rate of 6 gpm, which was deemed the maximum pumping rate based on drawdown within the well. Water discharged from the pump test was conveyed into 1,800-gallon water tank trucks and emptied at the waste water treatment plant. Approximately 25,900 gallons of groundwater was pumped over the duration of the

pump test. According to Clear Heart Drilling, on the very early morning of 2nd day of the test the generator stopped due to a low oil level alert. A back-up generator was then swapped into place and the pump brough back with depth-to-water levels quickly drawing down to the prior levels. The pump equipment was removed on the afternoon of August 6th, and a transducer continued to monitor groundwater recovery and levels for the next week or more.

A pump test for MUSD test well TW 08 started on September 10th but it was not completed as the well sustained less than 1 gpm while continuing to decline and was deemed insufficient for permitting into the MUSD system. TW 08 will either be kept as an onsite monitoring well or destroyed under a separate permit at a future time.

4.3 Monitoring Wells

Transducers were installed by GHD staff in onsite wells and nearby private wells with the owner's permission. Seven transducers were initially installed to collect background data on July 3rd and were reprogramed August 26th with a shorter time step for monitoring the pump test. Four additional transducers were installed on August 26th. Table 1 below shows the full list of monitoring wells and their construction details. In addition to the onsite creek manual read gauge, monitoring wells with transducers consisted of the onsite site wells (six total), a transducer in the creek, and five private wells.

Table 1 Monitoring Wells

Location	Wel Log No.	Surface Elevation (ft)	Total Depth (ft)	Pumping During Test Period	Drill Date
MUSD Well 01	141427	414.7	35	No	3/23/1976
MUSD Well 02[2]	Unknown	426.2	40	No	Unknown
MUSD Well 06	2021-001445	435.8	45	No	12/11/2020
MUSD Test Well 07 (new)	2025-09670	408.9	40	Yes	8/8/2025
MUSD Test Well 08 (new)	2025-09674	405.1	30	No	8/6/2025
MUSD N. Caisson (site wetland)	112963	400.6	29	No	10/14/1963
MUSD Creek Gauge[3]		374.4			
10800 Cummings Ln	Unknown	466.0[1]	27	No	Unknown
10600 Gurley Ln	Unknown	326.8[1]	18	Yes	Unknown
10601 Gurley Ln	Unknown	360.6[1]	16	Yes	Unknown
10651 Gurley Ln	Unknown	376.0[1]	147	No	Unknown
44150 Little Lake Rd	Unknown	374.5[1]	18	No	Unknown

[1] Surface elevations were obtained using an Arrow Gold GNSS Eos Position System and reported in NAVD 88 elevations.
[2] MUSD Well 02 was manually measured and did not have a transducer installed inside the well due to a lack of wellhead access for the transducer to be installed through.
[3] MUSD Creek Gauge is a manual gauge that was read via visual observations. A transducer was also installed in the creek near the manual gauge.

4.3.1 Surrounding Private Wells Monitored

In addition to the monitoring wells, a number of private wells had depth-to-water measurements taken before, during and after the pump test to evaluate potential interference effects from the pump tests. Private wells were monitored at homeowner request following the public notice program. Manual water level measurements were performed by GHD staff between July 3rd to September 17th. Measurements were generally taken once per week with an additional measurement taken each day of the pumping test for a total of 194 water level measurements collected between the

16 domestic wells monitored. Table 2 below shows the wells monitored and their construction details. Ground surface elevations were obtained using an Arrow Gold GNSS Eos Position System and reported in NAVD 88 elevations. These elevations have a vertical uncertainty of up to a couple of feet which is an acceptable level of accuracy for the analysis in this report as the primary concern is the relative change in groundwater elevations at each location. Transducer measurements and manual depth to water measurements are accurate to 0.01-ft (one hundredth) of a foot.

Manual depth-to-water measurements were performed using a water level indicator that was disinfected by soaking the indicator cord and probe in 3% hydrogen peroxide for a minimum of 10 minutes. The well casing cover was removed, and a measurement was taken by lowering the indicator probe until the unit beeped continuously and the corresponding cord height at a marked reference point on top of the well casing was recorded to the nearest 0.01-foot. Measurements were often taken twice by lifting the indicator probe several feet and lowering again until the unit beeped continuously.

Table 2 Private Wells Monitored During Pump Testing

Location	Wel Log No.	Surface Elevation (ft)[1]	Total Depth (ft)	Pumping During Test Period[2]	Total Number of Depth-to-Water Measurements
10750 Cummings Ln	Uknown	459.1	18	No	12
10780 Cummings Ln	Uknown	470.6	32	No	11
10781 Cummings Ln	Uknown	458.3	72[3]	No	12
10800 Cummings Ln	Uknown	466.0	27	No	13[4]
10833 Cummings Ln	Uknown	452.3	21	No	6
10600 Gurley Ln	140367	326.8	18	Yes	15[4]
10601 Gurley Ln	Uknown	360.6	15.5	Yes	15[4]
10651 Gurley Ln	0924893	376.3	140	No	15[4]
43901 Little Lake Rd	Uknown	457.4	38	No	9
43970 Little Lake Rd	Uknown	454.9	35	No	14
44000 Little Lake Rd	407185	412.8	150 / 78[5]	No	15
44150 Little Lake Rd	Uknown	374.5	18	No	12[4]
44460 Little Lake Rd	Uknown	322.4	32	Yes	9
10851 Merrill Ln	Uknown	343.0	100	No	8
43906 Tibbens Ln	Uknown	436.6	45	No	14
10511 Wheeler St	Uknown	329.2	18	No	14

[1] Surface elevations were obtained using an Arrow Gold GNSS Eos Position System and reported in NAVD 88 elevations.
[2] Pumping during the test period is based off field observations of pump motor activity during depth-to-water sampling.
[3] An obstruction at 72-ft stopped tool, it is unknown if the well extends deeper.
[4] In addition to the manual measurements a transducer was installed to continuously monitor water levels.
[5] Well completion report indicates 150-ft, manual measurement was only able to get to 78-ft.

In addition to the locations listed above, four additional locations were reviewed and attempted to collect depth-to-water measurements, however, well conditions were not suitable for obtaining accurate measurements. Figure 4 and Figure 5 below show the locations of the monitoring wells and surrounding private wells monitored. Depth-to-Water records are included in Appendix C.

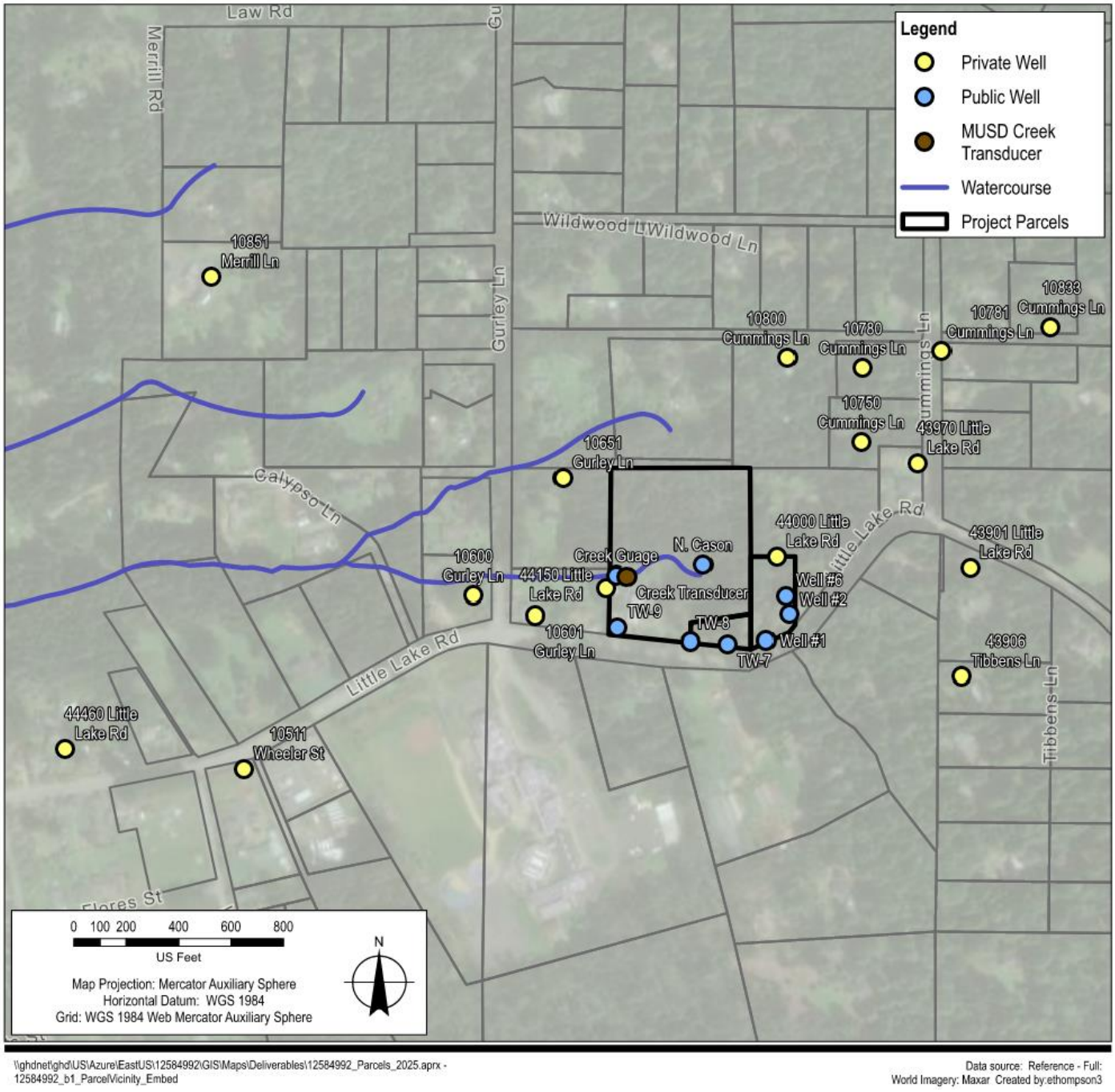


Figure 4 Vicinity Map of Wells Monitored

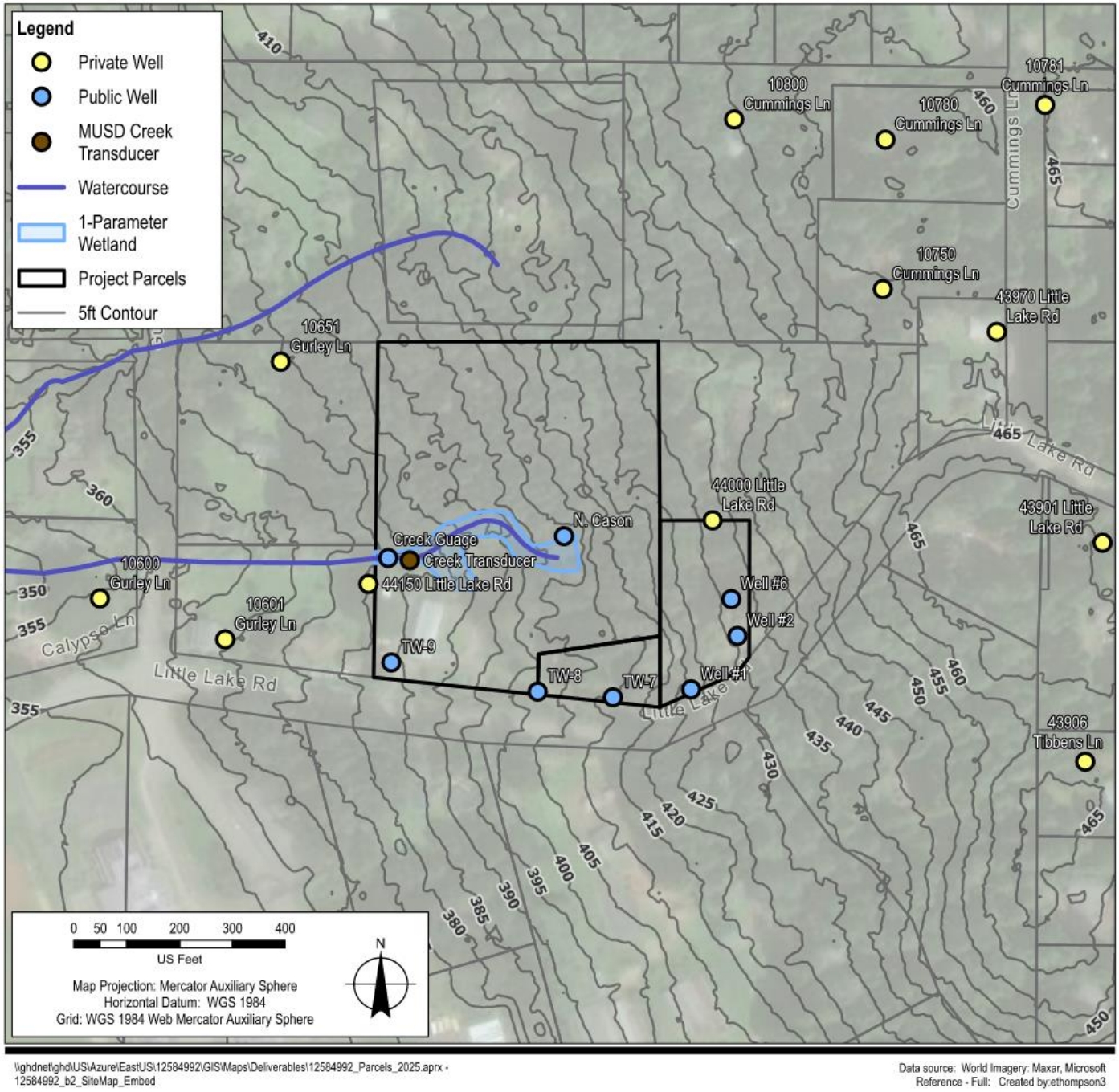


Figure 5 *Topography of Onsite and Neighbouring Private Wells Monitored*

5. Data Analysis

Data from both manual depth-to-water measurements and the installed transducers were reviewed and are presented in the form of hydrographs for each well and are included in Appendix C. Groundwater elevations were calculated using the ground surface elevation, adding the measured casing height and subtracting the depth-to-water measurement. Figure 6 shows the combined hydrograph of all the manual measurements. Figure 7 shows the

combined hydrographs of all wells with transducers installed. Figure 8 displays the same hydrographs limited to the MUSD onsite wells monitored.

Rainfall records over the course of monitoring onsite and domestic wells (July 3rd – September 22nd) was obtained from MCCSD with a total of 0.46-inches recorded of which 0.33 inches were after August 20th. Recorded rain events were less than 0.04 inches per day with exception to September 8th where 0.23 inches were recorded. Rainfall recorded over the course of the monitoring period is viewed as minimal and did not significantly influence the recorded groundwater levels.

Water levels recorded by the transducer installed inside the creek showed several abrupt spikes and dips in stage height that do not align with observed field observations and weather conditions. These discrepancies persist despite efforts to correct for repositioning the transducer following reinstallations after data retrieval. We suspect that the device may have interference from debris, sunken into the soft mud of the creek bed or other unknown factors that compromised the data integrity. For this reason, only transducer data for the creek up to August 23rd is presented in this report. However, the regular manual field measurements of the onsite stream gauge were taken over the course of the monitoring period and are seen as the most reliable data source for the remaining duration of the monitoring period.

Observed Background Groundwater Trends

Background static groundwater levels indicate that groundwater levels were declining over the summer months in the range of approximately 0.4- to 4.5-inches a week. Of the 23 wells reviewed, 14 have a clear groundwater declining trend from static groundwater levels with the remaining 9 pumping too often to obtain reliable static groundwater level measurements for any analysis. Table 3 below shows the comparison from the earliest background measurement obtained to the latest static groundwater measurement obtained and the corresponding trend for the 14 wells with reliable static groundwater levels.

Table 3 Background Groundwater Level Trend

Location	Date	Groundwater Elevation (NAVD 88 ft)	Date	Groundwater Elevation (NAVD 88 ft)	Water Level Change (ft)	Period (days)	Change over Time (ft/day)
North Caisson	7/3/25	398.11	9/18/25	397.75	0.36	77	0.005
TW 08	8/26/25	396.93	9/18/25	396.78	0.15	23	0.007
44150 Little Lake	8/26/25	369.21	9/17/25	368.82	0.39	22	0.018
10800 Cummings Ln	7/10/25	453.47	9/17/25	450.28	3.20	69	0.046
10651 Gurley Ln	7/3/25	360.66	9/17/25	359.48	1.17	76	0.015
10750 Cummings Ln	7/23/25	446.37	9/17/25	443.80	2.57	56	0.046
10780 Cummings Ln	7/31/25	452.57	9/17/25	450.81	1.76	48	0.037
10781 Cummings Ln	7/23/25	439.88	9/17/25	437.59	2.29	56	0.041
10833 Cummings Ln	7/23/25	436.16	8/29/25	434.78	1.38	37	0.037
43901 Little Lake	8/14/25	440.76	9/17/25	439.34	1.42	34	0.042
43970 Little Lake	7/10/25	439.75	9/17/25	436.62	3.13	69	0.045
44000 Little Lake	7/10/25	392.70	9/17/25	391.53	1.17	69	0.017
43906 Tibbens Ln	7/10/25	417.46	9/17/25	413.83	3.63	69	0.053
10511 Wheeler St	7/10/25	323.52	9/17/25	321.37	2.15	69	0.031
				Minimum	**0.15**	**22**	**0.005**
				Maximum	**3.63**	**77**	**0.053**
				Average	**1.77**		**0.031**

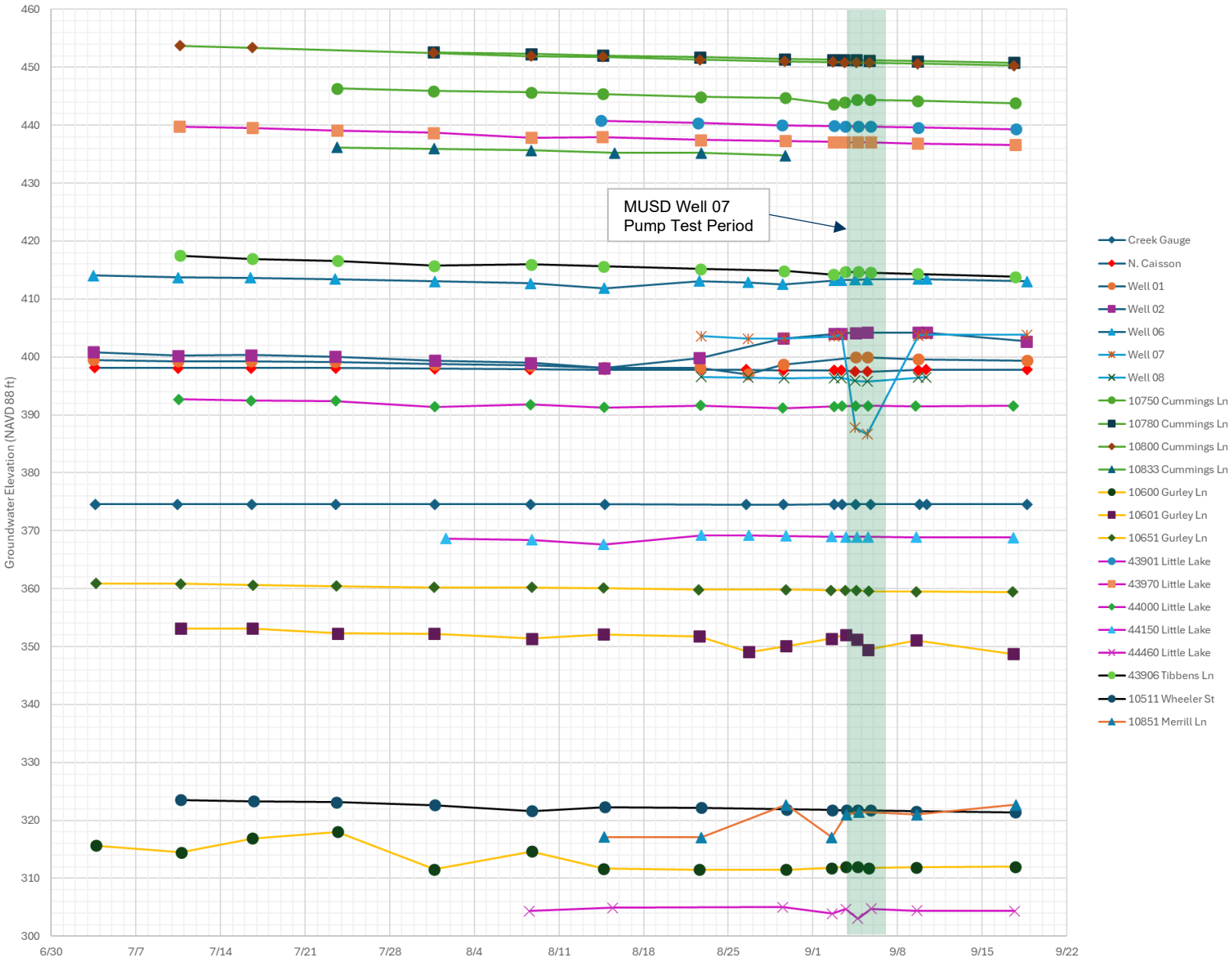


Figure 6 ***Manual Depth-to-Water Measurements***

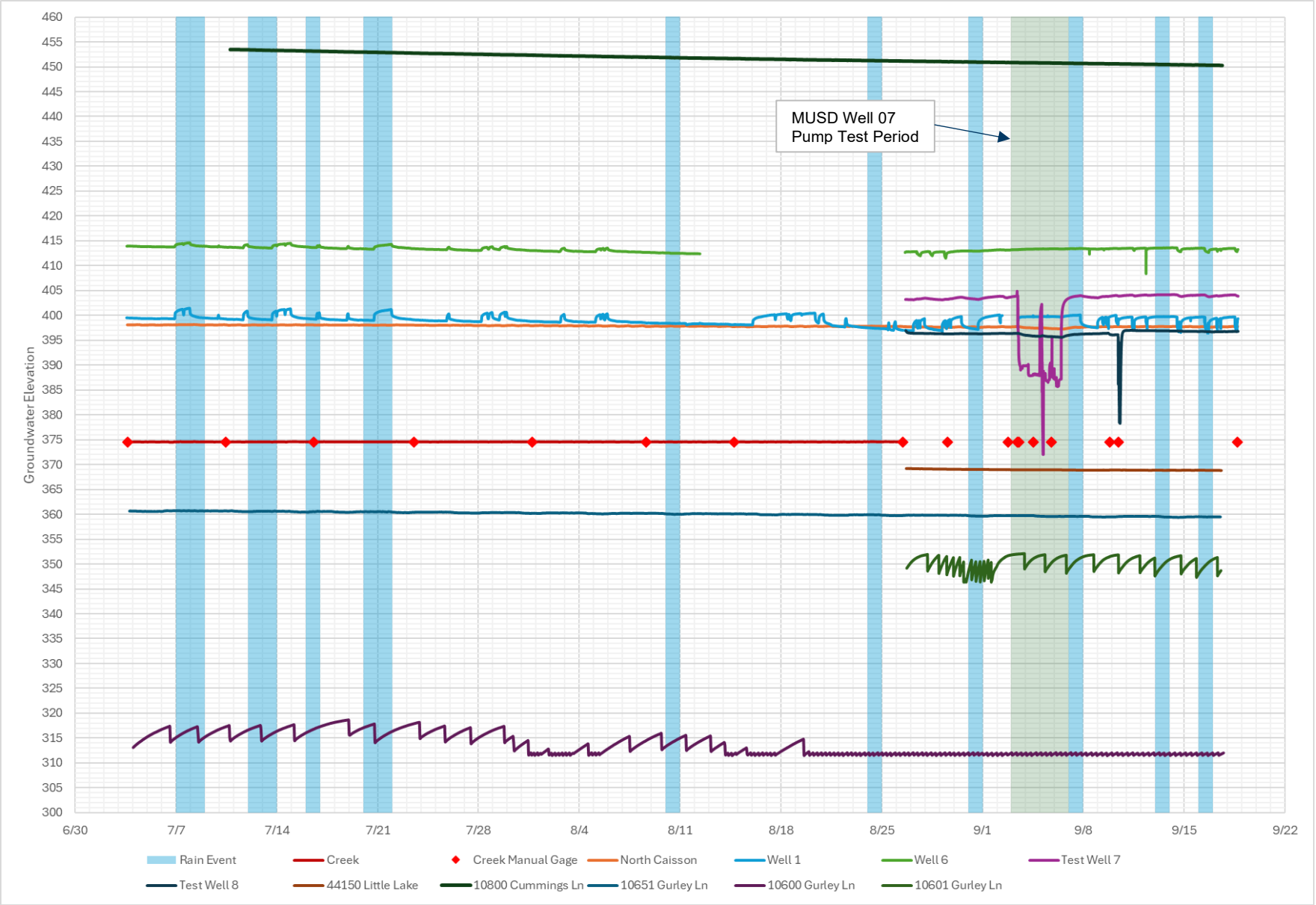


Figure 7 ***Transducer Records of Groundwater Levels***

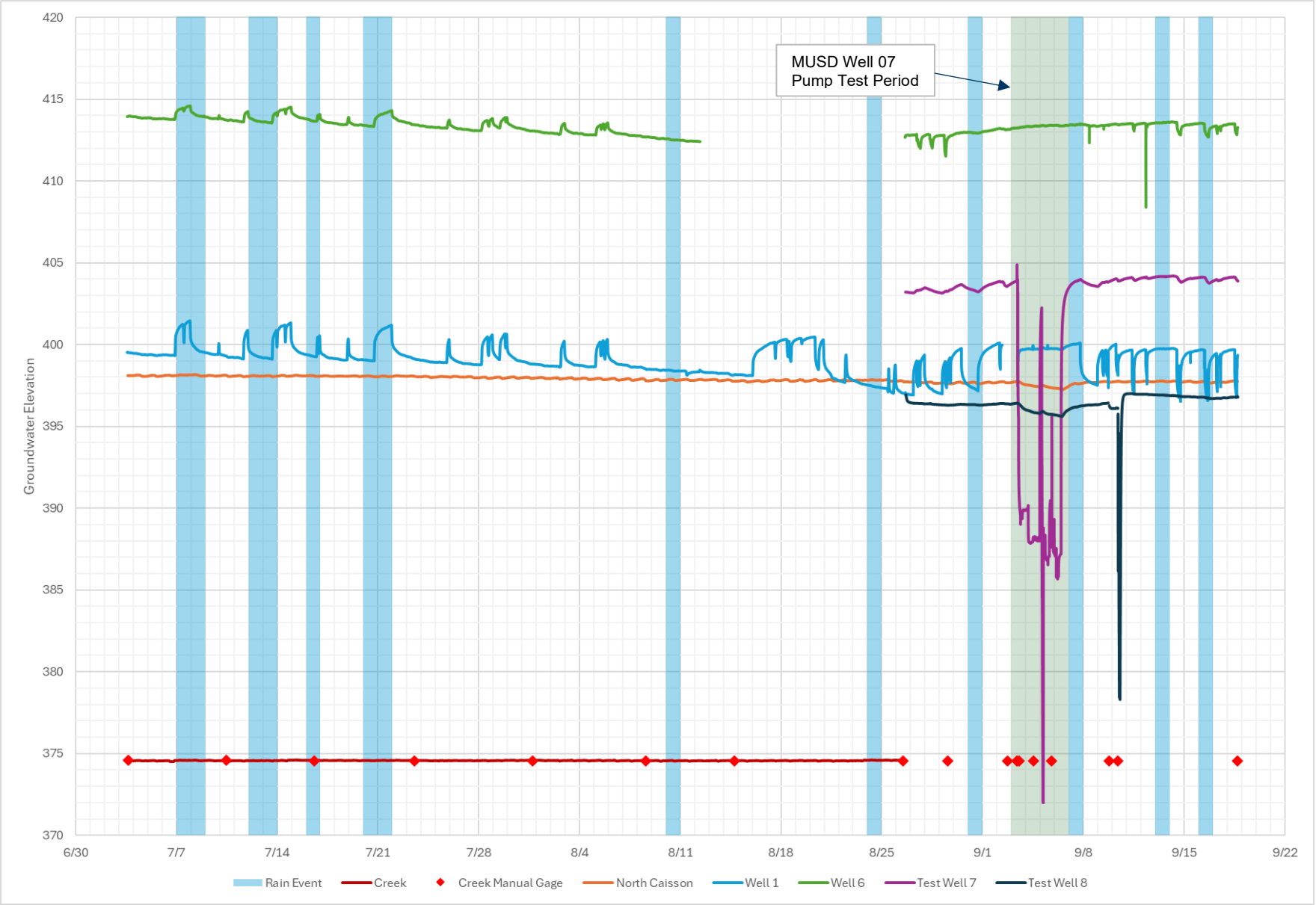


Figure 8 ***Groundwater Levels of MUSD Onsite Wells***

5.1 Well and Aquifer Characteristics

Groundwater level data beginning 24-hours before the pump test and including the 24-hours after the test were reviewed for drawdown effects in all monitoring wells and private wells. Groundwater levels did not reach a true steady state condition over the duration of the test (static drawdown at a constant pumping rate) and therefore unsteady flow analysis methods were used. Additionally, drawdown data was reviewed for apparent unconfined and confined conditions. Unconfined conditions were evaluated via Neuman's curve-fitting method for unsteady-state flow (Kruseman and Ridder, 1994) and confined conditions were evaluated with Theis's curve fitting method for unsteady-state flow. Based on drawdown over log time graphs the local aquifer around TW 07 appears locally confined as there is not the typical S-shape in the drawdown data that correspond to a delayed water table response typical of unconfined conditions. Instead, the data fits a typical Theis curve for confined conditions, shown in Figure 9 and Figure 10, and therefore the Theis method of analysis for determining aquifer parameters was used.

5.1.1 Theis Confined Aquifer Analysis – Unsteady Flow

Theis's curve-fitting method uses the relationship derived from the Theis equation to fit the drawdown of the observation well vs the time divided by the square distance from a well pumping at a constant rate. A plot on logarithmic paper of W(u) versus u, known as a type curve, is used in combination with a plot of time-drawdown data, plotted on logarithmic paper of the same size and scale as the type curve. The observed time-drawdown data is superimposed on the type curve and adjusted until a position is found where most of the plotted points of the observed data fall on a segment of the type curve. Any convenient point is then selected (the "match point"), and the coordinates of this match point are recorded for both the type curve and the time-drawdown plot and used in the Theis equation, shown below, to estimate aquifer parameters.

$$s = \frac{Q}{4\pi KD} W(u) \quad \text{and} \quad u = \frac{r^2 S}{4KDt}$$

where:

s = the drawdown (ft) measured in the observation well at a distance r (ft) from the pumping well.
Q = discharge from the well (ft^3/min), assumed to be constant.
K = hydraulic conductivity of the aquifer (ft/day).
D = Depth of the aquifer (ft), assumed to be the height of the static water level within the well with the bottom of the well fully penetrating the aquifer.
W(u) = Theis well function, evaluated for values of u (Todd and Mays, 2005).
r = radial distance (ft) between pumping and observation well.
S = the dimensionless storativity of the aquifer.
t = time (min) since pumping started.

Assumptions:

- The aquifer is confined.
- The aquifer has a seemingly infinite areal extent.
- The aquifer is homogeneous, isotropic, and of uniform thickness over the area influenced by the test.
- Prior to pumping, the piezometric surface is horizontal over the area that will be influenced by the test.
- The aquifer is pumped at a constant discharge rate.
- The well penetrates the entire aquifer and thus receives water by horizontal flow.
- The flow to the well is in an unsteady state, i.e. the drawdown differences with time are not negligible, nor is the hydraulic gradient constant with time.

These assumptions are rarely, if ever, fully met; and highlights the inherent approximations from the mathematical idealized conditions to field conditions.

Nearby onsite wells TW 08 and the North Caisson well were used to estimate aquifer parameters from the TW 07 pump test. Figure 9 shows the graphs used for curve fitting with Table 4 showing the results from the Theis equation.

Table 4 Theis Equation Values

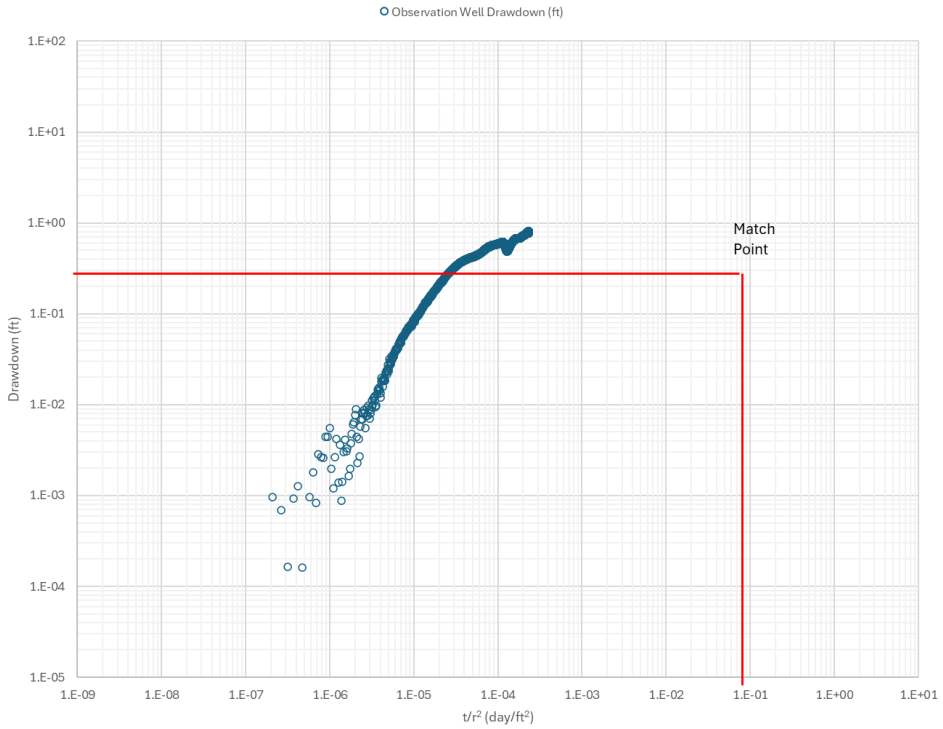
Known / Assumptions			
	TW 08	**North Caisson**	
Q	6	6	gpm
	1,155	1,155	ft^3/day
r	115	226	ft
D	19.5	23	ft
From Curve Fitting			
s	2.9.E-01	1.8.E-01	ft
t/r^2	8.0.E-02	2.1.E-02	day/ft^2
1/u	1.E+04	1.E+04	
W(u)	1.E+00	1.E+00	
Results			
Transmissivity (K*D)	320	510	ft^2/day
K	16	22	ft/day
K	1.9.E-04	2.6.E-04	ft/sec
S	1.2.E-02	4.3.E-03	

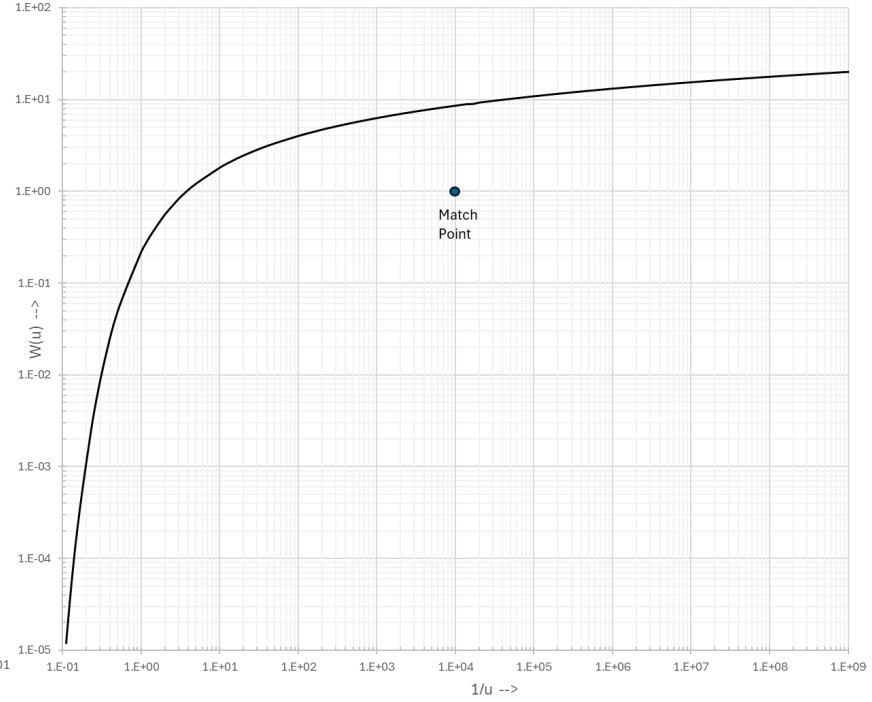
Transmissivity describes the ability of the aquifer to transmit groundwater throughout its entire saturated thickness and is measured as the rate at which groundwater can flow through an aquifer section of unit width under a unit hydraulic gradient. Based on the nature of the assumptions within the Theis equation estimation, an average of values calculated from monitoring wells should be used resulting in a value of 415 ft^2/day. This is within the range of anticipated values as previous estimations for transmissivity of Wells 01 and Wel 06 were 42 and 130 ft^2/day (GHD, 2024), and were estimated while multiple wells were pumping which would effectively decrease the transmissivity value. Therefore, the increase in transmissivity is expected will all onsite wells off.

Hydraulic conductivity is a measure of how easily water can pass through soil or rock. High values indicate permeable material through which water can pass easily, and low values indicate that the material is less permeable. Estimated hydraulic conductivities show good agreement with each other, averaging 19 ft/day, and are generally consistent with what would be expected from relatively fine silty sand to coarse sand which range from 0.03 to 300 ft/day (Fetter, 2001). Previous estimated hydraulic conductivities for Wells 01 and 06 were 2.8 and 5.5 ft/day, respectively, where again, the analysis period was previously during a period where multiple wells were pumping for sustained periods (i.e., not a dedicated pump test with nearby wells shut off) so an increase in estimated hydraulic conductivity is expected.

Storativity (or storage coefficient) is the volume of water that an aquifer releases from storage under a unit decline in hydraulic head per unit area of the aquifer (Freeze and Cherry, 1979). Storativity is dimensionless and in confined aquifers, values typically range from 0.005 to 0.00005 (Todd and Mays, 2005). It should be noted that for unconfined applications, storativity has an additional term, the specific yield (denoted S_y), which comes from the fact that in unconfined conditions drawdown in the water table results in water being released from within the aquifer soil pores of the aquifer (aka dewatering). This additional term is generally much greater than the volume of water released from the secondary effects of water expansion and aquifer compaction caused by changes in fluid pressure in confined conditions. Specific yield values generally range between 0.10-0.30 (Lohman, 1972) and are often used to approximate the storativity value of an unconfined aquifer, neglecting the secondary effects. The average storativity

value estimated from the two monitoring wells is 0.0082. This is on the high end of typical confined conditions and may be due to the locally confined conditions with influences of unconfined conditions elsewhere within the aquifer.


Observation Well Drawdown (ft)
Drawdown (ft)
1.E+02
1.E+01
1.E+00
1.E-01
1.E-02
1.E-03
1.E-04
1.E-05
1.E-09
1.E-08
1.E-07
1.E-06
1.E-05
1.E-04
1.E-03
1.E-02
1.E-01
1.E+00
1.E+01
t/r² (day/ft²)
Match
Point


W(u) -->
1.E+02
1.E+01
1.E+00
1.E-01
1.E-02
1.E-03
1.E-04
1.E-05
1.E-01
1.E+00
1.E+01
1.E+02
1.E+03
1.E+04
1.E+05
1.E+06
1.E+07
1.E+08
1.E+09
1/u -->
Match
Point

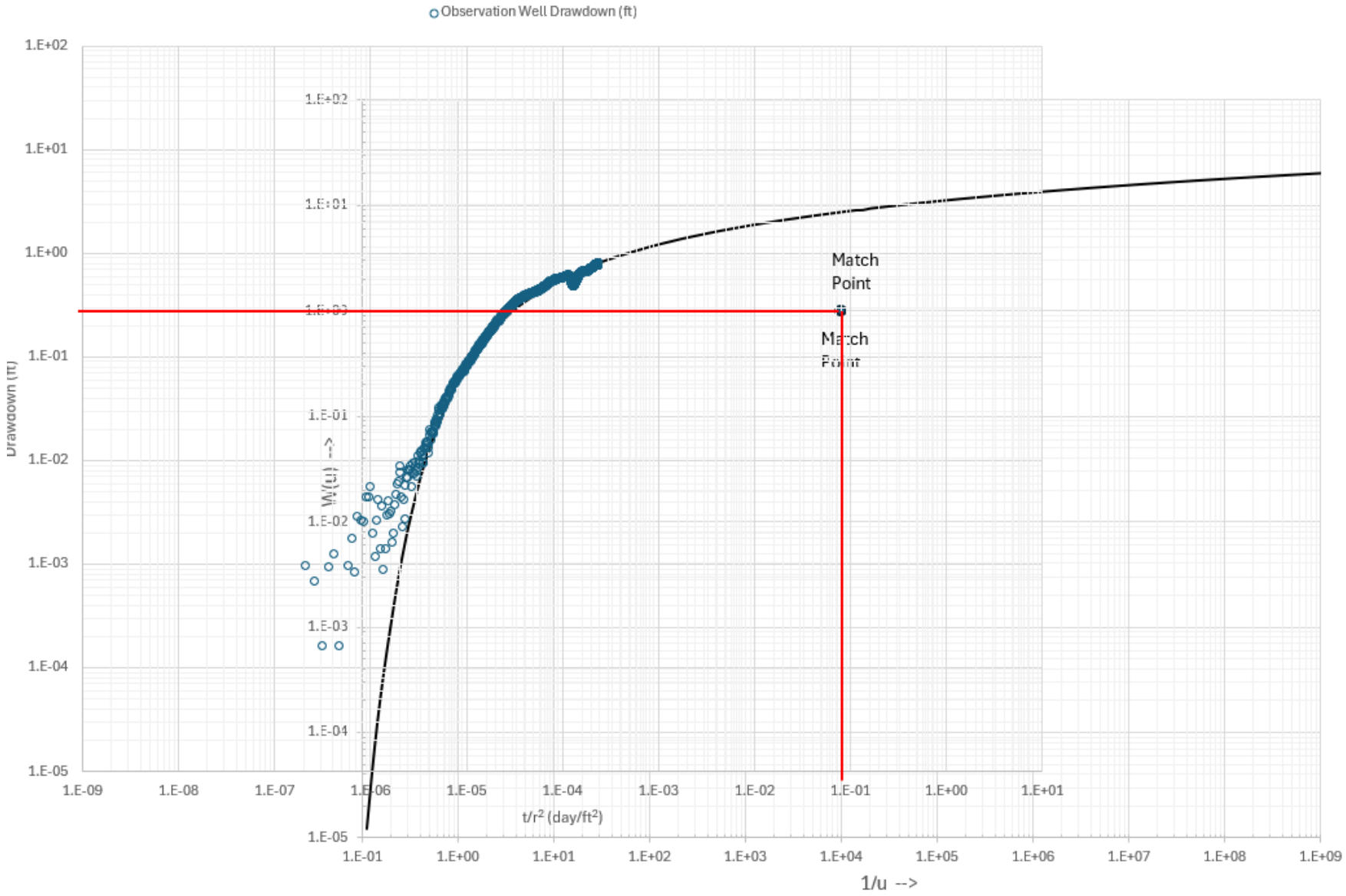
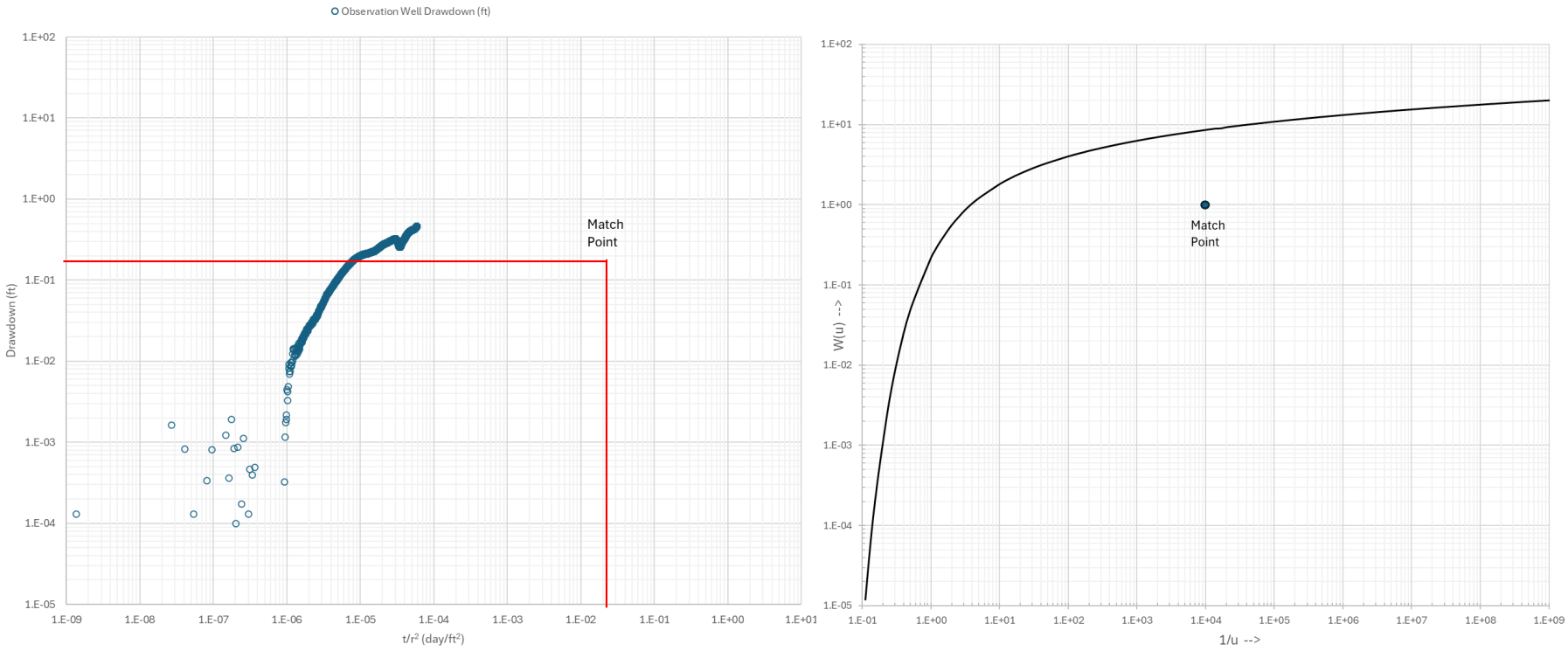


Figure 9 *TW 07 - Theis Curve Matching Graphs*


Observation Well Drawdown (ft)
Drawdown (ft)
1.E+02
1.E+01
1.E+00
1.E-01
1.E-02
1.E-03
1.E-04
1.E-05
Match Point
1.E-09
1.E-08
1.E-07
1.E-06
1.E-05
1.E-04
1.E-03
1.E-02
1.E-01
1.E+00
1.E+01
t/r² (day/ft²)
W(u) -->
Match Point
1.E-01
1.E+00
1.E+01
1.E+02
1.E+03
1.E+04
1.E+05
1.E+06
1.E+07
1.E+08
1.E+09
1/u -->

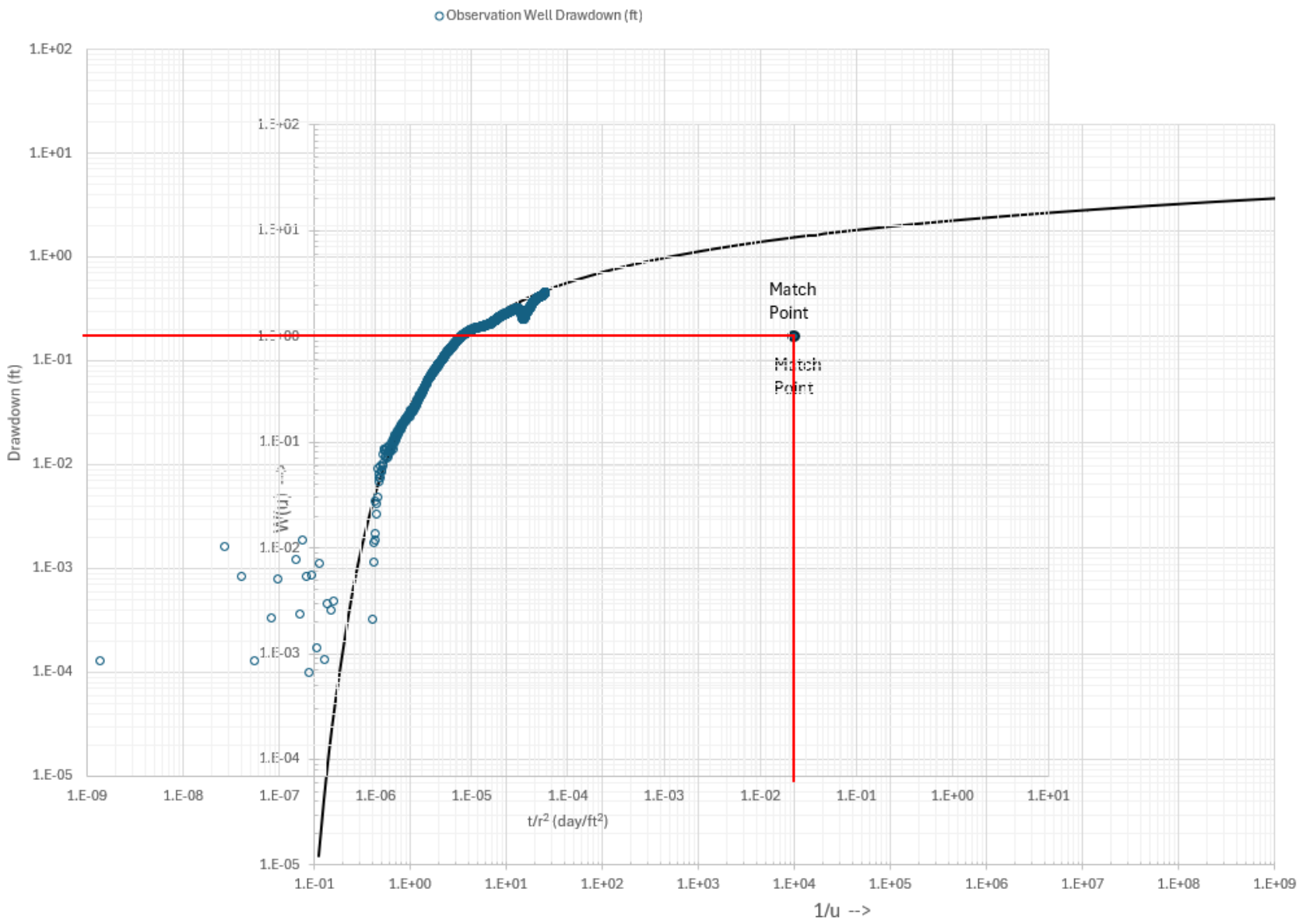


Figure 10 *North Caisson Well - Theis Curve Matching Graphs*

5.1.2 Well Efficiency and Specific Capacity

Specific capacity of a well is the discharge divided by the drawdown in a pumping well and shows a measure of productivity of a well. At the end of the 72-hr pump test TW 07 had 18.29 ft of drawdown from the sustained 6 gpm of pumping, a specific capacity of 0.33 gpm/ft, and recovered 90 percent of its water levels within 206 minutes, shown in Figure 11.

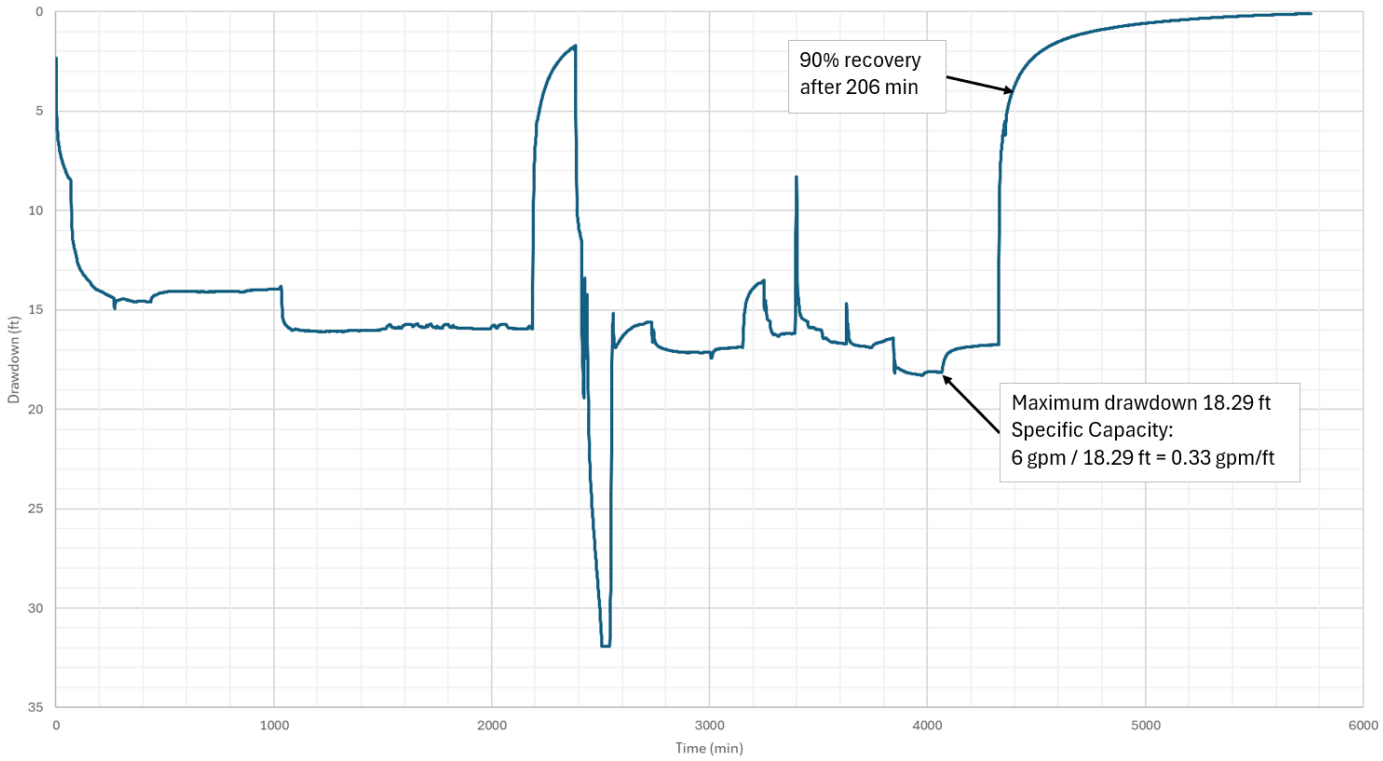


Figure 11 TW 07 Time Drawdown During 72-hr Pump Test

Well efficiency is the evaluation of the theoretical drawdown of a 100-percent efficient well to the actual drawdown observed during pumping. This can be estimated using a distance-drawdown curve by extending the straight line representation of the cone of depression line from two or more observation wells to the edge of the well casing, shown in Figure 12 below. Using the line of best fit a drawdown at the edge of the TW 07's well casing (0.25 ft) is estimated to be 3.3 ft. Using the well efficiency equation below, TW 07's estimated well efficiency is 18%.

$$Well\ Efficiency = \frac{S_{actual}}{S_{ideal}} * 100$$

$$18\% = \frac{18.29\ ft}{3.3\ ft} * 100$$

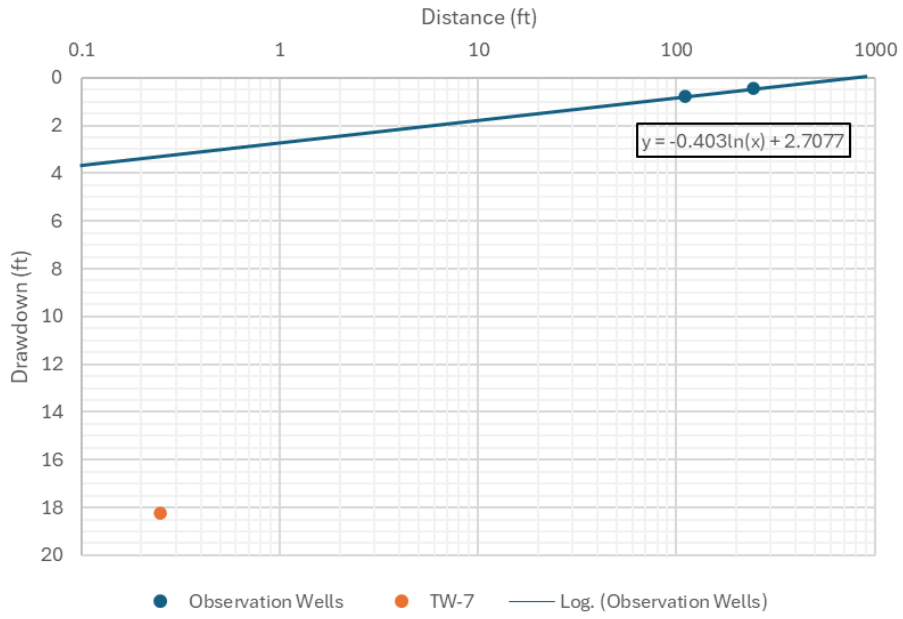


Figure 12 Distance-Drawdown Plot

5.2 Proof of Adequate Water Supply

There is no proposed development and no increase in proposed water use associated with the new well. MUSD's water use is anticipated to remain the approximately same as its historical use following completion of the project. The new well is needed to meet the Division of Drinking Water requirement for MUSD to maintain sufficient well source capacity to meet their maximum day water demand. Completion of a new recycled water system in the next 2 years is expected to decrease the amount of well water used for playfield irrigation, thereby reducing MUSD's water use.

5.3 Aquifer Effects

Monitoring well groundwater levels with observed drawdown effects from the pump test of TW 07 include the North Caisson Well and the MUSD TW 08, as shown in Figure 8. There are also what appears to be observed depression effects in MUSD Well 01 and Well 06 as their groundwater level recovery rate increased after the pump test ended. As groundwater levels in these two wells were still slightly recovering during the test from previous pumping activities, it isn't possible to quantify the exact effect TW 07 had during the pumping test and their data was not used for calculation of aquifer parameters.

Observed drawdown effects in effected onsite MUSD wells were relatively small, peaking at 0.81 feet in TW 08 and 0.46 feet the North Caisson wells at the end of the 72-hour test. Groundwater levels in Well 01 and Well 06 rose 0.51 feet and 0.13 feet, respectively over the course of the 72-hour test.

There were no observable drawdown effects in off-site private wells or at the creek gauge corresponding to the pump test of TW 07, shown in Figure 6 or in the hydrographs in Appendix D.

5.3.1 Radius of Influence

Using the Theis equation a radius of influence can be estimated from transient pumping drawdown data to evaluate potential drawdown effects in relation to distance from the well.

$$s = \frac{Q}{4\pi T} W(u)$$ solved for s in units of ft

Where:

s = drawdown (ft) in well at distance r
Q = pumping rate (ft^3/day)
T = transmissivity (415 ft^2/day)
W(u) = Theis well function; evaluated for values of u (Todd and Mays, 2005)
u = $r^2S/(4Tt)$
where:
r = radial distance (ft) between pumping and observation well
S = storativity (dimensionless), estimated to be 0.0082 and within the range of one order of magnitude – shown as dashed lines in Figures.
T = transmissivity (415 ft^2/day)
t = time (3, 90, and 180 days)

The projected drawdown from the MUSD wells was evaluated under three different scenarios:

1. Maximum daily demand (MDD) for 3-days
2. 90-day dry weather conditions
3. 180-day drought conditions

For the drought conditions it is assumed that rainfall is not recharging groundwater levels.

As previously stated, the MDD for the MUSD system is estimated to be 17.7 gpm. This is greater than the maximum supply capacity of TW 07 and therefore the maximum supply capacity of 6 gpm was used for this analysis. Aquifer parameters were taken as the average values estimated from Table 4. The radius of influence graph under these conditions is shown in Figure 13. For the 90- and 180-day scenarios, it was assumed that TW 07 was used for the entire duration at 6 gpm and the other MUSD wells were not in operation. Pumping well Distance-Drawdown (cone of depression) estimates are shown in Figure 14 and Figure 15, respectively.

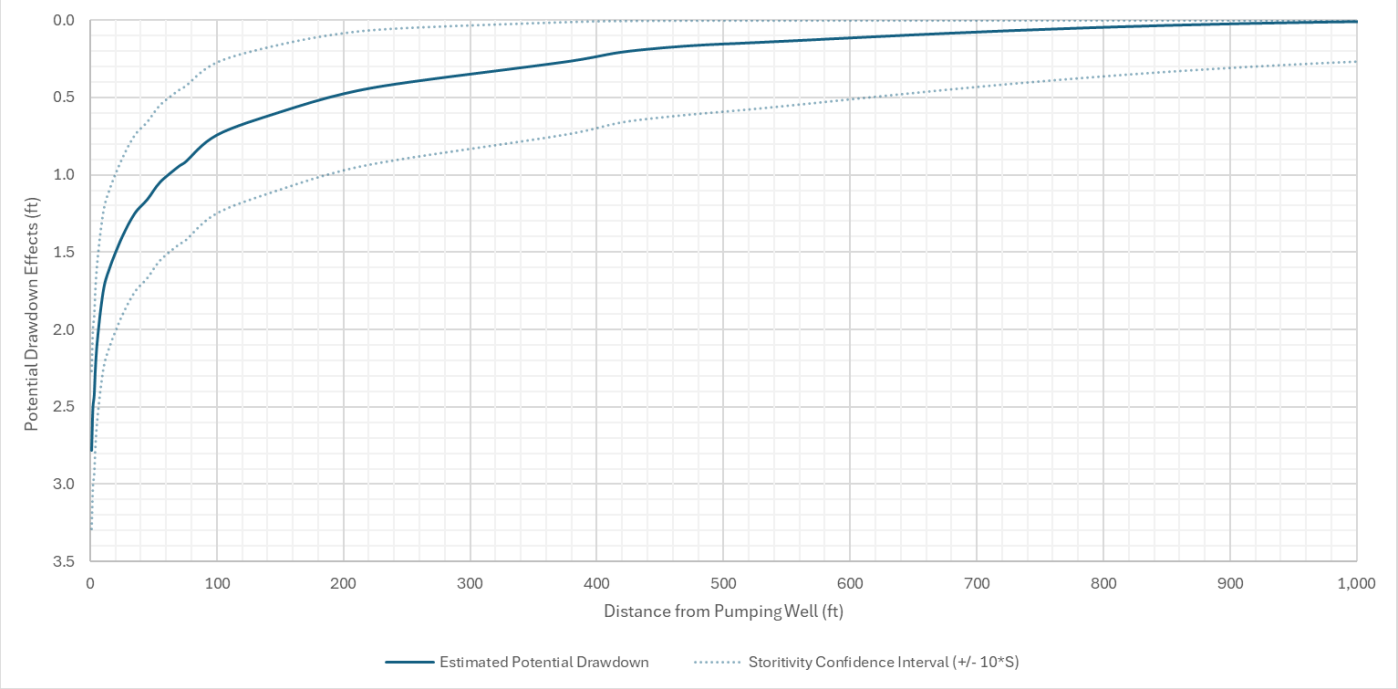


Figure 13 Radius of Influence of TW 07 after 3-days of pumping at 6 gpm

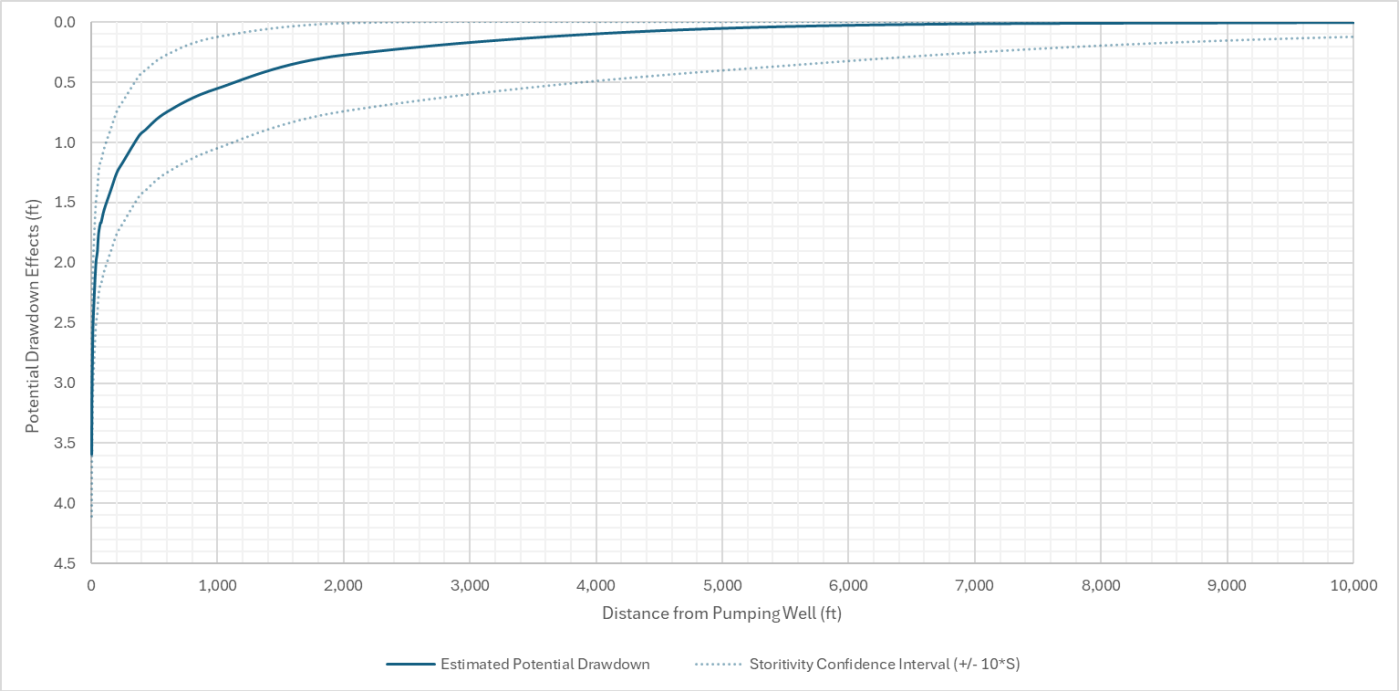


Figure 14 Radius of Influence of TW 07 after 90-days of pumping at 6 gpm

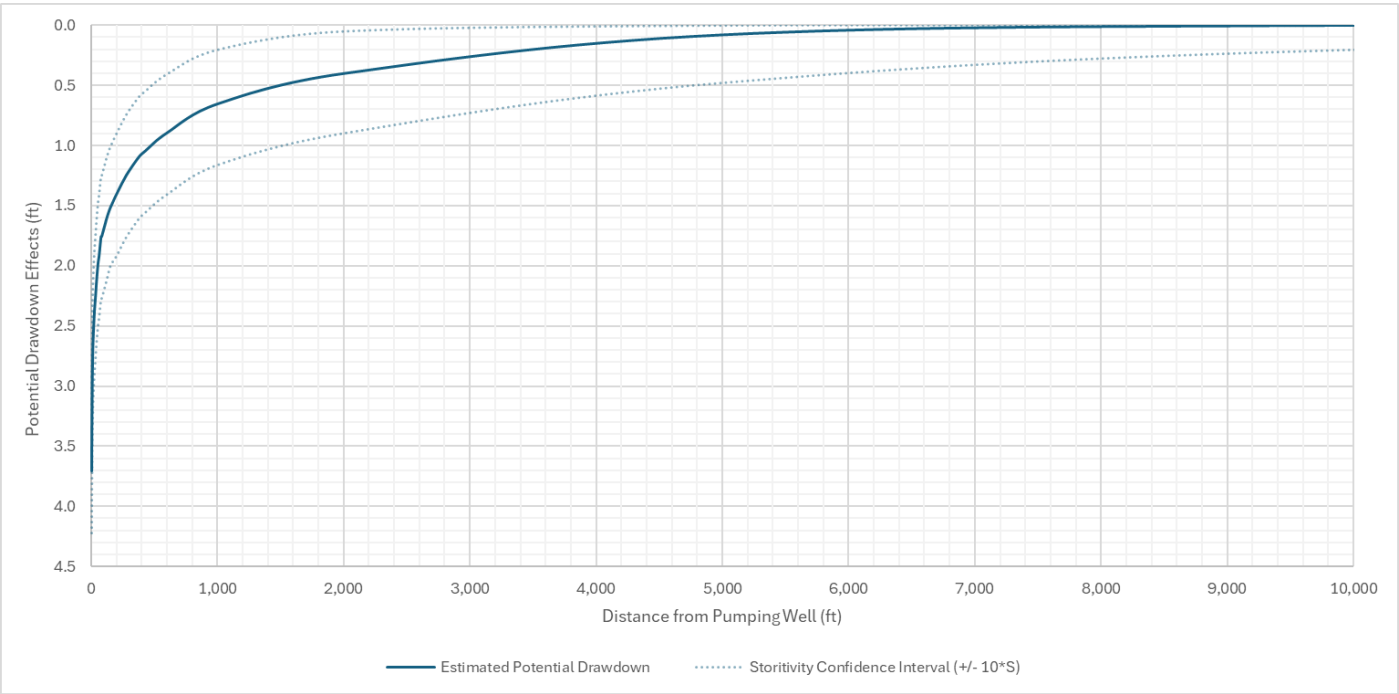


Figure 15 Radius of Influence of TW 07 after 180-days of pumping at 6 gpm

5.3.2 Evaluation of Potential Adverse Effects

As stated in Section 5.3 and shown in the hydrographs (Appendix D) **there were no observable drawdown effects in offsite private wells corresponding to the pump test of TW 07.**

The estimate of drawdown below assumes that effected wells operate under similar hydrogeologic conditions and have similar physical characteristics as the pumped well. This is not true for bedrock wells in the vicinity, noted in Table 5, and is questionable for wells at significant distances. As previously discussed in Section 5 not all domestic wells with depth-to-water measurements had reliable static water levels (due to domestic pumping demands), all wells have been included in Table 5 for the sake of the theoretical projected drawdown, however wells under known pumping conditions or unreliable data for estimation of the available water column has been labelled Not Applicable (NA). The estimated available static water column thickness in each well was calculated by taking the total depth of the well (as measured by GHD field staff) minus the depth-to-water measurement the on 9-2-2025 (day before pumping test). Calculations are shown in Appendix E.

Table 5 Theoretical Drawdown in Nearby Wells from TW 07 Pumping

Location	Distance from TW 07 (ft)	Total Depth of Well (ft)	Estimated Available Static Water Column Thickness in Well (ft)	Theoretical Drawdown after 3-days (ft)	Percent Theoretical Drawdown of Available Water Column after 3-days pumping	Theoretical Drawdown after 90-days (ft)	Theoretical Drawdown after 180-days (ft)
TW 08	111	31.8	20.9	0.74	4%	1.48	1.67
Well 01[1]	115	36.1	19.0	0.74	4%	1.48	1.61
Well 02	203	40	16.8	0.48	3%	1.25	1.40
Well 06	225	45.8	22.4	0.45	2%	1.16	1.40
N. Caisson	246	29.0	23.0	0.40	2%	1.16	1.25
44000 Little Lake[2]	297	78	55.5	0.40	1%	1.05	1.25
44150 Little Lake Rd	395	18.3	11.2	0.20	2%	0.92	1.10
10601 Gurley Ln	574	15.8	NA	0.12	NA	0.74	0.92
10651 Gurley Ln[2]	691	147	129.2	0.07	0%	0.66	0.89
43906 Tibbens Ln	699	45	21.0	0.07	0%	0.66	0.89
10750 Cummings Ln[1]	716	18	1.9	0.07	4%	0.66	0.89
43901 Little Lake Rd	752	38	20.3	0.06	0%	0.66	0.74
10600 Gurley Ln	765	18.2	NA	0.05	NA	0.66	0.74
43970 Little Lake Rd	776	35	16.9	0.05	0%	0.66	0.74
10800 Cummings Ln	863	27	10.7	0.05	0%	0.59	0.74
10780 Cummings Ln	907	32	11.5	0.05	0%	0.59	0.74
10781 Cummings Ln[2]	1073	72	50.7	0.01	0%	0.51	0.66
10833 Cummings Ln[1]	1337	21	2.6	0.00	0%	0.40	0.55
10511 Wheeler St	1476	18	NA	0.00	NA	0.40	0.51
10851 Merrill Ln[2]	1870	100	NA	0.00	NA	0.27	0.40
44460 Little Lake Rd	1982	32	NA	0.00	4%	0.27	0.40

[1] Well was pumping or did not have a depth-to-water measurement on 9-2-2025 and therefore the closest previous measurement was used. See Appendix C for all depth-to-water measurements.

[2] Well penetrates significantly into bedrock and is likely not under similar hydrogeologic conditions and physical characteristics as the pumping well.

Theoretical drawdown calculations, shown in Table 5 indicate that under 3-days of sustained pumping from TW 07 would cause up to 0.4-feet (less than 5-inches) of interference effects in the nearest domestic well. No domestic well has more than a 4% decrease in the available water column from the theoretical pumping effects after 3-days of 6 gpm pumping. Sustained pumping for 180 days indicates a maximum theoretical pumping drawdown in the nearest domestic well of 0.67-feet (8-inches).

5.3.3 Evaluation of Potential Adverse Cumulative Effects

Hydrologic reports for the domestic wells in the vicinity of TW 07 were not available, so potential cumulative effects of MUSD wells in combination with domestic wells cannot be evaluated. Domestic wells with transducer water level data were reviewed for potential background pumping effects prior to the pump testing period and only one monitored well showed interference effects, 10651 Gurley Ln shown in Appendix D. Transducer data showed approximately 0.2 feet of pumping effects, lasting for 1-2 days once or twice a week on an irregular schedule. This is believed to come from another nearby domestic well(s) as when compared to MUSD pumping cycles observed in their well's hydrographs the drawdown pattern observed in 10651 Gurley Ln does not match. Additionally, the interference effect is observed through a portion of the pump test of TW 07 and no additional drawdown is seen due to the pump test.

To evaluate the cumulative effects from all the MUSD wells operating simultaneously, the same radius of influence calculation was used to evaluate the effects of pumping from each individual well and added together to represent a cumulative impact of a theoretical 3-day pumping event at MUSD's MDD (17.7 gpm). Pumping was assumed to be continuous, simultaneous, and proportional to their percentage of the MUSD total supply capacity (3.8 gpm for TW 07, 6.3 gpm for Well 01, 4.4 gpm for Well 02, and 3.2 gpm for Well 06). Pumping effects based on distance from each well were evaluated using the same assumptions and aquifer parameters as the evaluation of TW 07 pumping effects. A summary of pumping effects are shown in Table 6, calculations are shown in Appendix E.

After 3-days of pumping at the MUSD's MDD the theoretical cumulative drawdown in the nearest domestic well would be up to 1.47-feet and would not exceed 5 percent drawdown of the available water column with exception to 10750 Cummings Ln where an estimated 0.3-feet (3.6-inches) would cause 16 percent drawdown due to its extremely shallow available water column of 1.9-feet.

Table 6 Theoretical Drawdown in Nearby Wells from MDD Pumping from MUSD Wells 01 ,02, 06, and TW 07 for 3-days.

Location	Theoretical Drawdown TW 07 (ft)	Theoretical Drawdown Well 01 (ft)	Theoretical Drawdown Well 02 (ft)	Theoretical Drawdown Well 06(ft)	Theoretical Cumulative Drawdown (ft)	Available Water Column (ft)	% Drawdown of Available Water Column
TW-7	-	0.78	0.35	0.24	NA	NA	NA
TW-8	0.47	0.47	0.20	0.14	1.28	20	6%
Well 01	0.47	-	0.55	0.35	NA	NA	NA
Well 02	0.30	0.78	-	0.55	NA	NA	NA
Well 06	0.28	0.69	0.77	-	NA	NA	NA
N. Caisson	0.25	0.42	0.30	0.21	1.19	23	5%
44000 Little Lake	0.25	0.42	0.40	0.39	1.47	55.5	3%
44150 Little Lake Rd	0.13	0.16	0.09	0.07	0.45	11.2	4%
10601 Gurley Ln	0.08	0.07	0.04	0.03	0.22	NA	NA
10651 Gurley Ln	0.04	0.05	0.04	0.03	0.16	129.2	0%
43906 Tibbens Ln	0.04	0.11	0.09	0.07	0.31	21	1%
10750 Cummings Ln	0.04	0.09	0.09	0.08	0.30	1.9	**16%**
43901 Little Lake Rd	0.04	0.09	0.09	0.07	0.28	20.3	1%
10600 Gruely Ln	0.03	0.05	0.04	0.03	0.14	NA	NA
43970 Little Lake Rd	0.03	0.07	0.07	0.07	0.24	16.9	1%
10800 Cummings Ln	0.03	0.05	0.04	0.04	0.16	10.7	1%
10780 Cummings Ln	0.03	0.05	0.04	0.04	0.16	11.5	1%
10781 Cummings Ln	0.01	0.01	0.04	0.03	0.08	50.7	0%
10833 Cummings Ln	0.00	0.00	0.01	0.01	0.02	2.6	1%
10511 Wheeler St	0.00	0.00	0.00	0.00	0.00	NA	NA
10851 Merrill Ln	0.00	0.00	0.00	0.00	0.00	NA	NA
44460 Little Lake Rd	0.00	0.00	0.00	0.00	0.00	NA	NA

5.4 Regional Aquifer Impact

Annual recharge to the marine terrace (limited to the MUSD parcel boundaries) from deep percolation of rainfall is estimated to be 12 inches (DWR, 1982) based on the average annual rainfall in the Mendocino area. The total area of the three adjacent MUSD parcels is a combined 5.703 acres resulting in approximately 5.703 acre-feet of annual recharge.

As the local shallow aquifer around the new wells appears locally confined the total storage within the aquifer is not possible to estimate without a specific yield value as the aquifer dewaters.

Assuming a conservative value for specific yield of 0.1, the storage capacity of the aquifer can be very roughly estimated through the combination of using the calculated storativity value to estimate the volume required to lower the pressure surface to the top of the saturated thickness of the aquifer and then using the specific yield to estimate the volume of water within the saturated thickness of the aquifer. To add to the uncertainty, the aquifer is not of uniform thickness across the entirety of the site and has therefore been roughly estimated from well construction logs, groundwater monitoring data and the topography of the Site. The aquifer thickness is roughly estimated to have an equivalent height of 10 feet of saturated thickness and 10 feet of pressure head on top of the saturated thickness.

$$Volume\ of\ Confined\ Water = SA\Delta h$$

$$37{,}000\ ft^3 = 0.0082 * 450{,}000 ft^2 * 10\ ft$$

$$Volume\ of\ Unconfined\ Water\ for\ a\ change\ in\ Head = S_y A\Delta h$$

$$450{,}000\ ft^3 = 0.1 * 450{,}000 ft^2 * 10\ ft$$

where:

S = Storativity (0.0082)

Sy = Specific Yield (0.01 estimated)

A = area of which the water table changes (5.703 acres or 450,000 ft^2)

Δh = change in water table height (ft)

This results in a total of 487,000 ft^3 (3.6 million gallons or 11.2 acre-feet).

As previously stated, there is no new use associated with the test well. The existing MUSD usage, as previously estimated in Section 5.3 MUSD's average daily demand is between 4,200-5,600 gallons, equivalent to between 1.6-2.1 million gallons (4.9-6.4 acre-feet) a year.

These estimates indicate the pumping roughly matches recharge which agrees with the hydrogeologic conceptual model of the site, where recharge fills the aquifer to or near capacity in the winter months through precipitation induced recharge which slowly declines over the summer months out the bottom of the aquifer through the onsite springs, and creek alluvium and the aquifer itself has relatively little storage capacity resulting in low water levels during periods of drought.

5.5 Mitigation of Adverse Effect and Adverse Cumulative Effect

No adverse effects as defined by the MCCSD Ordinance or County guidelines were observed during the testing period, therefore no mitigation measures are proposed on pumping quantities or schedule of TW 07.

No adverse cumulative effects were observed from the simulated MUSD MDD 3-day pumping event with exception to 10750 Cummings Ln which is a substandard private well with an extremely shallow available water column of 1.9-feet. It theoretically could experience a drawdown of up to 0.3-feet (3.6-inches) which is 16 percent of the available water column. This drawdown is unlikely to occur because the well is located upgradient (upslope) of MUSD's wells. It is

more likely that this private well could be impacted by the pumping of the neighboring wells from the parcels immediately adjacent.

No mitigations are proposed from this potential effect due to the following factors:

1. The private well in question is only 18-feet deep and does not meet modern well construction standards.
2. Groundwater levels rapidly returned to baseline conditions following the TW 07 pump test.
3. Measured groundwater level decline observed in the well over the observation period of July 23rd to September 17th shows a total decline of 2.57 feet over the 56-day monitoring period (3.8-inches per week, see hydrograph in Appendix D). This equates to a 73 percent drop in the available water column from the beginning to end of the monitoring period. In comparison to the observed background groundwater level decline, a temporary 3.6-inch drop in groundwater levels within the well is de minimis as by the end of the monitoring period 1.1-inches of drawdown effects would technically constitute an adverse effect.

6. Conclusions

Two test wells (TW 07 and TW 08) and one boring (that was subsequently abandoned) were installed as part of this study. Of the two test wells, only TW 07 was found to be a viable new source of water supply during pump testing. Test well TW 08 was tested for a short time and found to produce less than a gallon a minute, and declining, and deemed not likely able maintain adequate water for the remaining days of the 72-hour testing period.

Test well TW 07 performed adequately and was able to maintain 6 gpm for the 72-hour testing period, drawdown of onsite wells was very minimal, and did not drawdown water levels in offsite domestic wells monitored during that time. The average transmissivity and storativity of the marine terrace deposits in vicinity of TW 07 is approximately 420 ft^2/day and 0.0082, respectively. The 72-hour specific capacity and well efficiency of TW 07 at a 6-gpm pumping rate is 0.33 gpm/ft and 18%, respectively.

Previously established well source capacities for MSUD wells (GHD 2021) with the addition of TW 07 are shown in Table 7. The combined source capacities with the highest capacity offline is 18 gpm which meets the required 17.7 gpm requirement by DDW.

Table 7 MUSD Dry Season Source Well Capacities

Well ID	Source Capacity (gpm)
Well 01	10
Well 02	7
Well 06	5
TW 07	6

Background trends indicate that the local aquifer(s) groundwater level depletes at approximately 2.6 inches per week on average during the summer through seeps and springs. There were no observed pumping effects in monitored domestic wells despite theoretical drawdown calculations indicating that a visible effect would present.

The projected 3-day pumping effects from TW 07 are estimated to be negligible with 4 percent or less theoretical drawdown of the available water column in the monitored wells. Projected 90- and 180-day drought pumping scenarios estimate up to 1.05 and 1.25 ft, respectively, of potential drawdown effects in the nearest domestic well, which is a bedrock well located 297 feet from TW 07.

Cumulative impacts from a theoretical 3-day MDD pumping event spread across all wells (Well 01, Well 02, Well 06, and TW 07) estimate a maximum theoretical drawdown of 1.47-feet in the nearest domestic well. Cumulative impacts to neighbouring domestic wells are minimal.

The findings provided in this study show that TW 07 doesn't negatively impact onsite or offsite wells and that it is intended to be a redundant and/or back-up well with no new increase in water use proposed by MUSD. Therefore, it is concluded that test well TW 07:

- Should be permitted as a new supply well for MUSD by both the County of Mendocino and the State Division Drinking Water (DDW).
- Has a firm pumping capacity of 6 gpm in the dry season.
- Could be used in combination with MUSD's other existing permitted wells.
- Could be used during the wet season conditions to fill the fire and water supply storage tanks.

7. References

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Appendices

Appendix A

Well Completion Reports and Boring Logs

TW-07

State of California

Well Completion Report

Form DWR 188 Submitted 10/01/2025

WCR2025-009670

Owner's Well Number: **Date Work Began:** 08/07/2025 **Date Work Ended:** 08/08/2025

Local Permit Agency: Environmental Health Division - Fort Bragg Office **County:** Mendocino

Secondary Permit Agency: **Permit Number:** 6551 **Permit Date:** 08/06/2025

Well Owner (must remain confidential pursuant to Water Code 13752)

Name: Mendocino Unified School District

Address: P.O. Box 1154

City: Mendocino **State:** California **Zip:** 95460

Planned Use and Activity

Activity: New Production or Monitoring Well

Planned Use: Monitoring

Well Location

Address: 44020 LITTLE LAKE RD

City: MENDOCINO **Zip:** 95460

APN: 11910023

Township: 17N **Range:** 17W

Section: 29 **BM:** Mount Diablo

Ground Surface Elevation:

Elevation Accuracy:

Elevation Determination Method:

Latitude: 39 Deg. 18 Min. 45.918 Sec. N

Dec. Lat. : 39.312755

Vertical Datum:

Location Accuracy:

Longitude: -123 Deg. 46 Min. 54.0012 Sec. W

Dec. Long. : -123.781667

Horizontal Datum:

Location Determination Method:

Borehole Information

Orientation: Vertical **# of casings (Specify):** 1

Drilling Method: Auger **Drilling Fluid:** None

Total Depth of Boring: 40 Feet

Total Depth of Completed Well: 40 Feet

Water Level and Yield of Completed Well

Depth to first water: 20 (Feet below surface)

Depth to Static Water Level: 6 (Feet)

Date Measured: 08/08/2025

Estimated Yield*: 6 (GPM) **Test Type:** Pump

Test Length*: 1 (Hours) **Total Drawdown:** (Feet)

***May not be representative of a well's long term yield.**

Geologic Log - Free Form

Depth from Surface (Feet to Feet)		Description
0	5	Stiff sandy clay light gray
5	12	Soft sandy clay white to gray
12	26	Soft to stiff transitions of light brown sandy clay fine coarse sand mix. Free water at 20' to 21'
26	35	Orange clay sand (wet) weathered franciscan bedrock - fine coarse sands
35	40	Orange fransiscan bedrock soil sample refusal

Casings

Casing #	Depth from Surface (Feet to Feet)		Casing Type	Material	Casings Specifications	Wall Thickness (inches)	Outside Diameter (inches)	Screen Type	Slot Size if any (inches)	Description
1	0	20	Blank	PVC	Other	0.26	6.5			
1	20	40	Screen	PVC	Other	0.26	6.5	Milled Slots	0.4	

Annular Material

Depth from Surface (Feet to Feet)		Fill	Fill Type Details	Filter Pack Size	Description
0	18	Cement	Portland Cement/Neat Cement		
18	20	Bentonite	Other Bentonite		TR pellets
20	40	Filter Pack	Other Gravel Pack		#6

Other Observations:

Borehole Specifications

Depth from Surface (Feet to Feet)		Borehole Diameter (inches)
0	20	10.5
20	40	10.5

Certification Statement

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

Name: CLEAR HEART DRILLING INC
Person, Firm or Corporation

555 B W COLLEGE AVENUE (Address) | SANTA ROSA (City) | California (State) | 95401 (Zip)

Signed: electronic signature received (C-57 Licensed Water Well Contractor) | 10/01/2025 (Date Signed) | 780357 (License Number)

DWR Use Only

CSG #	State Well Number	Site Code	Local Well Number

N — Latitude Deg/Min/Sec

W — Longitude Deg/Min/Sec

TRS:

APN:

Attachments

No Attachments

HYDROLOGIC BORING LOG

Project Name:	MUSD Test Wells	Project No.:	11136611	Boring No:	BH-2
Drilling Method:	Hollow Stem	Date Started:	8/7/2025	Time:	9:00 AM
Drilling Company:	Clear Heart	Date Completed:	8/8/2025	Time:	12:00 PM
C57 Number:	780357	Total Depth:	40.5'	Corresponds	
Logged By:	WM/CG	Water Level (bgs) first / last:	20'	to Well No.:	TW-7
Latitude/Longitude:	39.31234, -123.78207	Ground Surface Elevation (ft msl):	412'		
Hammer Type:	Auto Hammer	Surface Conditions:	Cleared vegitation, dirt covered		

DEPTH	SPT Blow Counts / 6"	SAMPLE NUMBER	USCS SYMBOL	SOIL DESCRIPTION [Soil type, Color, Percentage Estimate (0,0,0) fines, sand, gravel, Grain Size, Plasticity, Roundness, Other]	COLOR	MOISTURE	CONSISTENCY	GRAPHIC SYMBOL	WELL CONSTRUCTION DETAILS	WELL CONSTRUCTION DESCRIPTION (well and annular space materials, and depth intervals)
0			CL	0-5' Sandy Lean Clay (60,40,0)	light gray	dry to moist	stiff			
2										
4										0-18' Sanitary Seal Neat Cement
6			CL	5-12' Sandy Lean Clay fine sand, (75,25,0)	white to gray	moist to wet	soft			
8										0-20' 6" Sch. 40 PVC Blank
10	4-5	1								
12	-9		CL	12-26' Sandy Lean Clay fine-coarse rounded sand mottled brown (60,40,0)	light brown	moist to wet	soft-m. stiff			
14										
16										
18										18-20' Sanitary Seal Bentonite
20	1-2	2		Free Water at 20-21'		wet	soft			
22	-5									20-40.5' Sandpack 8x16 Graded Clean Sand
24										
26	8-11	3								20-40' 6" Sch. 40 PVC 0.040" slot Screen
	-17		SC	26-35' Clayey Sand weathered fransiscan bedrock fine to coarse sand (30,70,0)	orange	wet	m. dense			
28										
30	10-12	4		decreasing weathering						
32	-20									
34										
36	25-50	5		35-40.5' Fransiscan Bedrock Sampler refusal at 35.5'	orange	dry to moist	v. dense			
38				Sampler refusal at 40'						
40	50	6		40.5' End of Drilling			v. dense			

TW-08

State of California

Well Completion Report

Form DWR 188 Submitted 10/01/2025

WCR2025-009674

Owner's Well Number: **Date Work Began:** 08/08/2025 **Date Work Ended:** 08/09/2025

Local Permit Agency: Environmental Health Division - Fort Bragg Office **County:** Mendocino

Secondary Permit Agency: **Permit Number:** 6552 **Permit Date:** 08/08/2025

Well Owner (must remain confidential pursuant to Water Code 13752)

Name: Mendocino Unified School District

Address: P.O. Box 1154

City: Mendocino **State:** California **Zip:** 95460

Planned Use and Activity

Activity: New Production or Monitoring Well

Planned Use: Monitoring

Well Location

Address: 44020 LITTLE LAKE RD

City: MENDOCINO **Zip:** 95460

APN: 11910004

Township: 17N **Range:** 17W

Section: 29 **BM:** Mount Diablo

Ground Surface Elevation:

Elevation Accuracy:

Elevation Determination Method:

Latitude: 39 Deg. 18 Min. 45.918 Sec. N

Dec. Lat. : 39.312755

Vertical Datum:

Location Accuracy:

Longitude: -123 Deg. 46 Min. 54.0012 Sec. W

Dec. Long. : -123.781667

Horizontal Datum:

Location Determination Method:

Borehole Information

Orientation: Vertical **# of casings (Specify):** 1

Drilling Method: Auger **Drilling Fluid:** None

Total Depth of Boring: 30 Feet

Total Depth of Completed Well: 30 Feet

Water Level and Yield of Completed Well

Depth to first water: 15 (Feet below surface)

Depth to Static Water Level: 20 (Feet)

Date Measured: 08/08/2025

Estimated Yield*: 1.25 (GPM) **Test Type:** Pump

Test Length*: 2 (Hours) **Total Drawdown:** 8 (Feet)

***May not be representative of a well's long term yield.**

Geologic Log - Free Form

Depth from Surface (Feet to Feet)		Description
0	6	Dark gray clay - stiff
6	8.5	Light brown moist to wet soft clay (fine sands)
8.5	15	Clay sand fine-coarse sand (brown) wet (water)
15	27	Clay sand weathered franscican rock - sand mix (orange) moist to wet
27	30	Orange fransican bedrock dense and dry to moist

Casings

Casing #	Depth from Surface (Feet to Feet)		Casing Type	Material	Casings Specifications	Wall Thickness (inches)	Outside Diameter (inches)	Screen Type	Slot Size if any (inches)	Description
1	0	20	Blank	PVC	Other	0.26	6.5			
1	20	30	Screen	PVC	Other	0.26	6.5	Milled Slots	0.4	Milled slotted

Annular Material

Depth from Surface (Feet to Feet)		Fill	Fill Type Details	Filter Pack Size	Description
0	18	Cement	Portland Cement/Neat Cement		
18	20	Bentonite	Other Bentonite		TR Pellets
20	30	Filter Pack	Other Gravel Pack		#6

Other Observations:

Borehole Specifications

Depth from Surface (Feet to Feet)		Borehole Diameter (inches)
0	20	10.5
20	30	10.5

Certification Statement

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

Name: CLEAR HEART DRILLING INC
Person, Firm or Corporation

555 B W COLLEGE AVENUE (Address) | SANTA ROSA (City) | California (State) | 95401 (Zip)

Signed: electronic signature received (C-57 Licensed Water Well Contractor) | 10/01/2025 (Date Signed) | 780357 (License Number)

DWR Use Only

CSG #	State Well Number	Site Code	Local Well Number

N — Latitude Deg/Min/Sec

W — Longitude Deg/Min/Sec

TRS:

APN:

Attachments

No Attachments

HYDROLOGIC BORING LOG

Project Name:	MUSD Test Wells	Project No.:	11136611	Boring No:	BH-1
Drilling Method:	Hollow Stem	Date Started:	8/5/2025	Time:	1:00 PM
Drilling Company:	Clear Heart	Date Completed:	8/6/2025	Time:	12:00 PM
C57 Number:	780357	Total Depth:	30.5'	Corresponds	
Logged By:	CRG	Water Level (bgs) first / last:	20'	to Well No.:	TW-8
Latitude/Longitude:	39.31244, -123.78279	Ground Surface Elevation (ft msl):	395'		
Hammer Type:	Auto Hammer	Surface Conditions:	Cleared vegitation, dirt covered		

DEPTH	SPT Blow Counts / 6"	SAMPLE NUMBER	USCS SYMBOL	SOIL DESCRIPTION [Soil type, Color, Percentage Estimate (0,0,0) fines, sand, gravel, Grain Size, Plasticity, Roundness, Other]	COLOR	MOISTURE	CONSISTENCY	GRAPHIC SYMBOL	WELL CONSTRUCTION DETAILS	WELL CONSTRUCTION DESCRIPTION (well and annular space materials, and depth intervals)
0			CL	0-6' Lean Clay (90,10,0)	dark gray	dry to moist	stiff			
2										
4										0-18' Sanitary Seal Neat Cement
6			CL	6-8.5' Sandy Lean Clay fine sand, (70,30,0)	white to gray	moist to wet	soft to m. stiff			
8										0-20' 6" Sch. 40 PVC Blank
10			SC	8.5-15' Clayey Sand	light brown	moist to wet	m. dense			
	9-12	1		fine-coarse rounded sand						
12	-14			mottled brown (30,70,0)						
14										
16			SC	15-27' Clayey Sand	orange	moist to wet	m. dense			
				weathered fransiscan bedrock						
18				fine to coarse sand (30,70,0)						18-20' Sanitary Seal Bentonite
20										
	11-12	2		Free Water at 20-21'						
22	-16			decreasing weathering						20-30.5' Sandpack 8x16 Graded Clean Sand
24										
26	11-13	3								20-30' 6" Sch. 40 PVC 0.040" slot Screen
	-18									
28				27-30.5' Fransiscan Bedrock	orange	dry to moist	v. dense			
				drilling rate slows significantly						
30				Sampler refusal at 30'						
	50	4		30.5' End of Drilling						
32										
34										
36										
38										
40										

TW-09

State of California

Well Completion Report

Form DWR 188 Submitted 10/01/2025

WCR2025-009682

WCR Number of Original Well:

Owner's Well Number: **Date Work Began:** 08/06/2025 **Date Work Ended:** 08/06/2025

Local Permit Agency: Environmental Health Division - Fort Bragg Office **County:** Mendocino

Secondary Permit Agency: **Permit Number:** 6553 **Permit Date:** 07/31/2025

Well Owner (must remain confidential pursuant to Water Code 13752)

Name: Mendocino Unified School District

Address: P.O. Box 1154

City: Mendocino **State:** California **Zip:** 95460

Planned Use and Activity

Activity: Well Destruction (of existing well)

Former Use: Monitoring

Well Location

Address: 44100 LITTLE LAKE RD

City: MENDOCINO **Zip:** 95460

Latitude: 39 Deg. 18 Min. 47.3256 Sec. N

Dec. Lat. : 39.313146

Vertical Datum:

Location Accuracy:

Longitude: -123 Deg. 46 Min. 57.5292 Sec. W

Dec. Long. : -123.782647

Horizontal Datum:

Location Determination Method:

APN: 11910003

Township: 17N **Range:** 17W

Section: 29 **BM:** Mount Diablo

Ground Surface Elevation:

Elevation Accuracy:

Elevation Determination Method:

Borehole Information

Orientation: Vertical **# of casings (Specify):** 1

Drilling Method: **Drilling Fluid:**

Total Depth of Boring: Feet

Total Depth of Completed Well: Feet

Water Level and Yield of Completed Well

Depth to first water: (Feet below surface)

Depth to Static Water Level: (Feet)

Date Measured:

Estimated Yield*: (GPM) **Test Type:**

Test Length*: (Hours) **Total Drawdown:** (Feet)

***May not be representative of a well's long term yield.**

Destruction Details: Backfilled with a cement grout slurry and topped with native soil.

Other Observations:

Borehole Specifications

Depth from Surface (Feet to Feet)	Borehole Diameter (inches)

Certification Statement

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

Name: CLEAR HEART DRILLING INC
Person, Firm or Corporation

555 B W COLLEGE AVENUE	SANTA ROSA	California	95401
Address	City	State	Zip

Signed: electronic signature received | 10/01/2025 | 780357
C-57 Licensed Water Well Contractor | Date Signed | License Number

DWR Use Only

CSG #	State Well Number	Site Code	Local Well Number

					N
					W

Latitude Deg/Min/Sec

Longitude Deg/Min/Sec

TRS:

APN:

Attachments

No Attachments

HYDROLOGIC BORING LOG

Project Name:	MUSD Test Wells	Project No.:	11136611	Boring No:	BH-3
Drilling Method:	Hollow Stem	Date Started:	8/12/2025	Time:	
Drilling Company:	Clear Heart	Date Completed:	8/13/2025	Time:	
C57 Number:	780357	Total Depth:	25.5'	Corresponds	
Logged By:	WM/CG	Water Level (bgs) first / last:	NA	to Well No.:	TW-9
Latitude/Longitude:	39.31252, -123.78335	Ground Surface Elevation (ft msl):	395'		
Hammer Type:	Auto Hammer	Surface Conditions:	Grass Covered		

DEPTH	SPT Blow Counts / 6"	SAMPLE NUMBER	USCS SYMBOL	SOIL DESCRIPTION [Soil type, Color, Percentage Estimate (0,0,0) fines, sand, gravel, Grain Size, Plasticity, Roundness, Other]	COLOR	MOISTURE	CONSISTENCY	GRAPHIC SYMBOL	WELL CONSTRUCTION DETAILS	WELL CONSTRUCTION DESCRIPTION (well and annular space materials, and depth intervals)
0			CL	0-4' Lean Clay	dark	dry to	stiff			
2				(90,10,0)	brown	moist				
4										Backfilled with
6			CL-SC	4-20' Sandy Lean Clay fine sand (60,40,0)	reddish brown	dry to mosit				Cement Grout
8										
10						moist to wet				
12	4-5 11	1								
14										
16										
18						wet				
20	50	2		20-25' Fransiscan Bedrock (shale)	dark gray	dry	v. dense			
22				drilling rate slows significantly						
24				Sampler refusal at 20' and 25'						
26	50	3		Boring Terminated at 25.5'						
28										
30										
32										
34										
36										
38										
40										

MUSD Well 01

17N/17W - 29

CONFIDENTIAL LOG Water Code Sec. 13752

ORIGINAL
File with DWR

STATE OF CALIFORNIA
THE RESOURCES AGENCY
DEPARTMENT OF WATER RESOURCES

WATER WELL DRILLERS REPORT

Do Not Fill In

No 141427

State Well No.
Other Well No.

CONFIDENTIAL LOG Water Code Sec. 13752

(1) OWNER:
Name
Addre

(2) LOCATION OF WELL:
County Mendocino Owner's number, if any
Township, Range, and Section
Distance from cities, roads, railroads, etc. MUSD Watershed on north side of Little Lake Road, Mendocino

(3) TYPE OF WORK *(check)*:
New Well [X] Deepening [ ] Reconditioning [ ] Destroying [ ]
If destruction, describe material and procedure in Item 11.

(4) PROPOSED USE *(check)*:
Domestic [ ] Industrial [ ] Municipal [ ]
Irrigation [ ] Test Well [ ] Other [X]

(5) EQUIPMENT:
Rotary [ ]
Cable [ ]
Other Bucket [X]

(6) CASING INSTALLED:
STEEL: (OTHER:)
SINGLE [ ] DOUBLE [ ] Plastic

From ft.	To ft.	Diam.	Gage or Wall	Diameter of Bore	If gravel packed: From ft.	If gravel packed: To ft.
0	36	8	160 PSI	30"		

Size of shoe or well ring: none
Size of gravel: pea
Describe joint Bell & glue joint

(7) PERFORATIONS OR SCREEN:
Type of perforation or name of screen sawn

From ft.	To ft.	Perf. per row	Rows per ft.	Size in. x in.
21	36	5	2	1/8 x 4

(8) CONSTRUCTION:
Was a surface sanitary seal provided? Yes [X] No [ ] To what depth 20 ft.
Were any strata sealed against pollution? Yes [ ] No [X] If yes, note depth of strata
From ft. to ft.
From ft. to ft.
Method of sealing cement on gravel pack

(9) WATER LEVELS:
Depth at which water was first found, if known ft.
Standing level before perforating, if known ft.
Standing level after perforating and developing 9 ft.

(10) WELL TESTS:
Was pump test made? Yes [ ] No [X] If yes, by whom? bail
Yield: 30 gal./min. with 22 ft. drawdown after hrs.
Temperature of water cold Was a chemical analysis made? Yes [ ] No [X]
Was electric log made of well? Yes [ ] No [X] If yes, attach copy

(11) WELL LOG:
Total depth 35 ft. Depth of completed well 35 ft.
Formation: *Describe by color, character, size of material, and structure*

ft. to	ft.	
0	- 1	Brown top soil
1	- 8	Brown sandy clay
8	- 15	Gray sand
15	- 20	Brown and gray sandy clay
20	- 25	Birds eye gravel making water
25	- 35	Brown clay and shale

Work started 3/23/76 19 , Completed 3/23/76 19

WELL DRILLER'S STATEMENT:
This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME Weeks Drilling and Pump Co.
(Person, firm, or corporation) (Typed or printed)
Address Sebastopol Road
Sebastopol, California 95470
[SIGNED] Gerald Thompson
By: Mary E. Thompson (Well Driller) Mary E. Thompson
License No. 177681 Dated March 24, 19 76

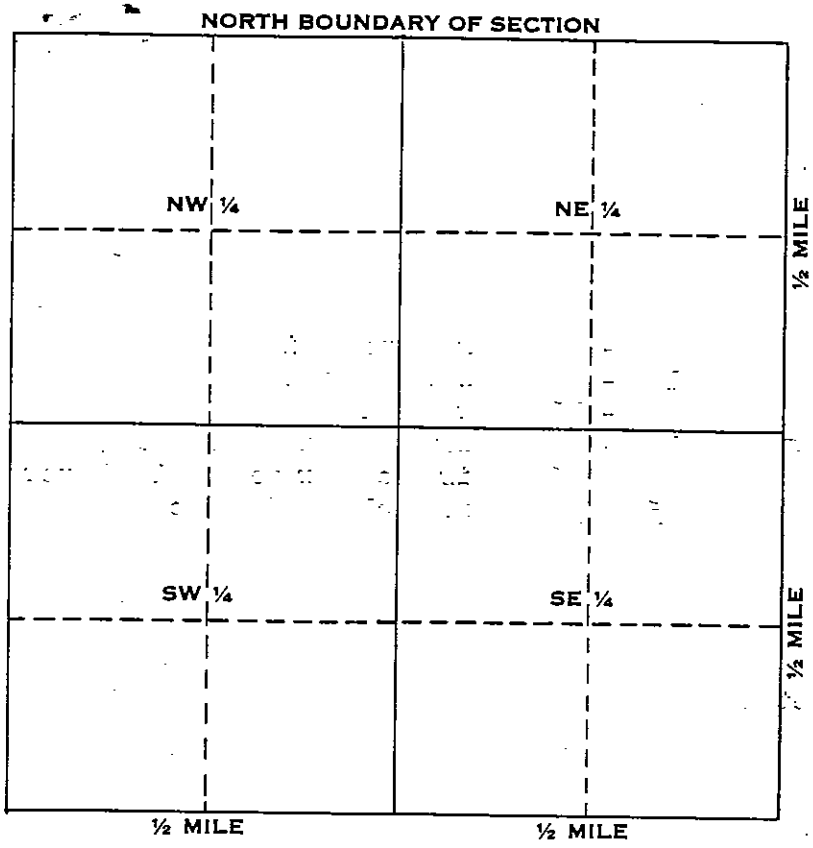
SKETCH LOCATION OF WELL ON REVERSE SIDE

DWR 188 (REV. 9-68)

8-72 30M TRIP OT OSP

WELL LOCATION SKETCH

141427

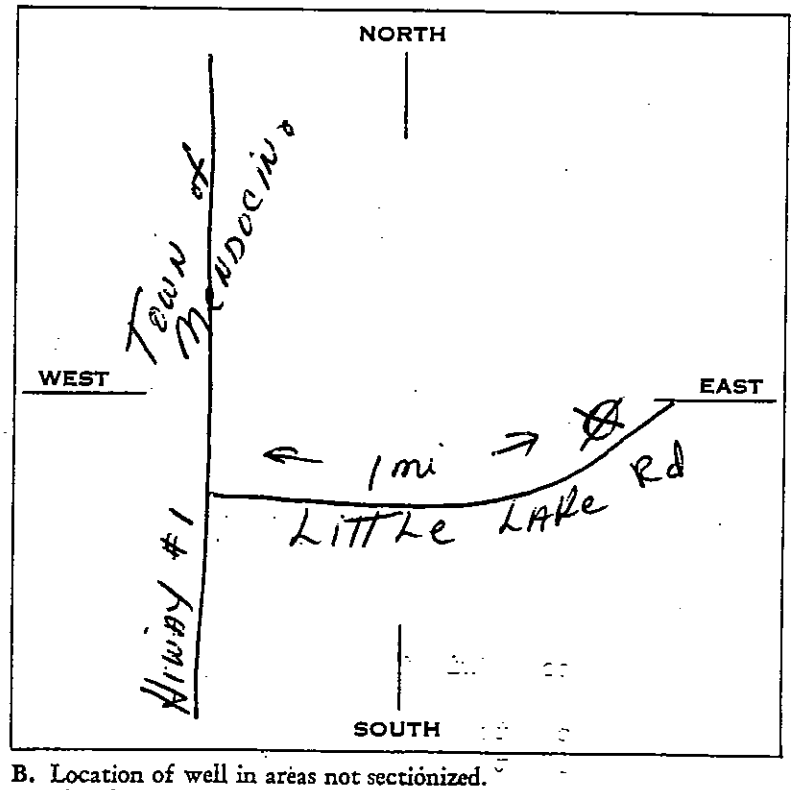


Township 17 N/S

Range 17 E/W

Section No. 29C

A. Location of well in sectionized areas.
Sketch roads, railroads, streams, or other features as necessary.



B. Location of well in areas not sectionized.
Sketch roads, railroads, streams, or other features as necessary.
Indicate distances.

1976 APR 1 AM 11 15

DEPT. OF WATER RESOURCES

State of California

Well Completion Report

Form DWR 188 Auto-Completed 4/19/2021

WCR2021-001445

MUSD Well 06

Owner's Well Number: WW-2 | Date Work Began: 12/10/2020 | Date Work Ended: 12/11/2020

Local Permit Agency: Environmental Health Division - Fort Bragg Office

Secondary Permit Agency: | Permit Number: WW23932 | Permit Date: 12/02/2020

Well Owner (must remain confidential pursuant to Water Code 13752)

Name: XXXXXXXXXXXXXXXXXXX

Mailing Address: XXXXXXXXXXXXXXXXXXX

XXXXXXXXXXXXXXXXXXX

City: XXXXXXXXXXXXXXXXXXX | State: XX | Zip: XXXXX

Planned Use and Activity

Activity: New Well

Planned Use: Water Supply Domestic

Well Location

Address: 44020 Little Lake RD

City: Mendodcino | Zip: 95460 | County: Mendocino

Latitude: 39 Deg. 18 Min. 45.9035 Sec. N | Longitude: -123 Deg. 46 Min. 54.1397 Sec. W

Dec. Lat.: 39.312751 | Dec. Long.: -123.7817055

Vertical Datum: | Horizontal Datum: WGS84

Location Accuracy: Unknown | Location Determination Method: Unknown

APN: 119-100-23

Township: 17 N

Range: 17 W

Section: 29

Baseline Meridian: Mount Diablo

Ground Surface Elevation:

Elevation Accuracy:

Elevation Determination Method:

Borehole Information

Orientation: Vertical | Specify:

Drilling Method: Auger | Drilling Fluid: None

Total Depth of Boring: 45 Feet

Total Depth of Completed Well: 45 Feet

Water Level and Yield of Completed Well

Depth to first water: 16 (Feet below surface)

Depth to Static Water Level: 26.5 (Feet) | Date Measured: 12/11/2020

Estimated Yield*: 6 (GPM) | Test Type: Pump

Test Length: 8 (Hours) | Total Drawdown: 10.5 (feet)

*May not be representative of a well's long term yield.

Geologic Log - Free Form

Depth from Surface Feet to Feet		Description
0	5	Silty clay with sand (dry-soft)
5	10	Silty sand yellowish (dry-loose)
10	15	Poorly graded sand, fine sand mix
15	20	Graded sand light gray, fine sand
20	25	Well graded sand, yellowish (wet) fine-coarse sand
25	30	Yellowish silty sand
30	35	Poorly graded sand, coarse sand (wet)
35	40	Dark brown wethered bed rock
40	45	Solid bed rock

Casings

Casing #	Depth from Surface Feet to Feet		Casing Type	Material	Casings Specificatons	Wall Thickness (inches)	Outside Diameter (inches)	Screen Type	Slot Size if any (inches)	Description
1	0	25	Blank	PVC	OD: 5.563 in. | SDR: 21 | Thickness: 0.265 in.	0.265	5.563			Sch 40 Blank
2	25	40	Screen	PVC	OD: 5.563 in. | SDR: 21 | Thickness: 0.265 in.	0.265	5.563	Milled Slots	0.04	SCH 80 SCREEN
3	40	45	Blank	PVC	OD: 5.563 in. | SDR: 21 | Thickness: 0.265 in.	0.265	5.563			Sch 40 Blank

Annular Material

Depth from Surface Feet to Feet		Fill	Fill Type Details	Filter Pack Size	Description
0	18	Cement	Portland Cement/Neat Cement		Grout
18	20	Bentonite	Non Hydrated Bentonite		Pellets/Time Release
20	45	Filter Pack	Other Gravel Pack	#8	Sand

Other Observations:

Borehole Specifications

Depth from Surface Feet to Feet		Borehole Diameter (inches)
0	45	13

Certification Statement

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief

Name: CLEAR HEART DRILLING INC (Person, Firm or Corporation)

555 B W COLLEGE AVENUE (Address) | SANTA ROSA (City) | CA (State) | 95401 (Zip)

Signed: *electronic signature received* (C-57 Licensed Water Well Contractor) | 02/04/2021 (Date Signed) | 780357 (C-57 License Number)

DWR Use Only

CSG #	State Well Number	Site Code	Local Well Number

					N	

Latitude Deg/Min/Sec

						W

Longitude Deg/Min/Sec

TRS:

APN:

North Caison

ORIGINAL
File Original, Duplicate and Triplicate with the REGIONAL WATER POLLUTION CONTROL BOARD No. 1
(Insert appropriate number)

WATER WELL DRILLERS REPORT
(Sections 7076, 7077, 7078, Water Code)

THE RESOURCES AGENCY OF CALIFORNIA

430

Do Not Fill In
No 112963

State Well No.
Other Well No. 17N/17W29F

(1) OWNER:
Name
Address

(2) LOCATION OF WELL:
County Mendocino Owner's number, if any—
R. F. D. or Street No. map attached

(3) TYPE OF WORK (check):
New well ☒ Deepening ☐ Reconditioning ☐ Abandon ☐
If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):
Domestic ☒ Industrial ☐ Municipal ☐
Irrigation ☐ Test Well ☐ Other ☐

(5) EQUIPMENT:
Rotary ☒
Cable ☐
Dug Well ☐

(6) CASING INSTALLED:
SINGLE ☐ DOUBLE ☐

From ft.	to ft.	Diam.	Gage or Wall
36"	concrete	casing	"
"	"	"	"
"	"	"	"
"	"	"	"
"	"	"	"

Type and size of shoe or well ring none
Describe joint slip

If gravel packed

Diameter of Bore	from ft.	to ft.
60"	0 "	30'
"	"	"
"	"	"
"	"	"
"	"	"

Size of gravel: 1½ inch

(7) PERFORATIONS:
Type of perforator used round ½ x ½ inch
Size of perforations in., length, by in.

From ft.	to ft.	Perf. per row	Rows per ft.
bottom 6'	"	" " "	" " "
"	"	" " "	" " "
"	"	" " "	" " "
"	"	" " "	" " "

(8) CONSTRUCTION:
Was a surface sanitary seal provided? ☒ Yes ☐ No To what depth 12 ft.
Were any strata sealed against pollution? ☐ Yes ☒ No If yes, note depth of strata

From ft.	to ft.
"	"

Method of Sealing

(9) WATER LEVELS:
Depth at which water was first found 12 ft.
Standing level before perforating 12 ft.
Standing level after perforating 12 ft.

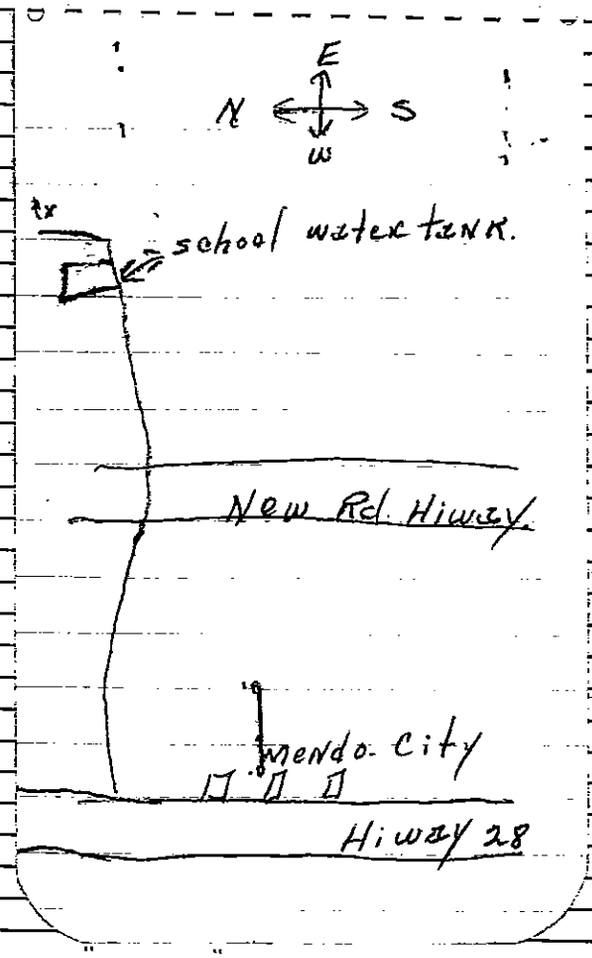
(10) WELL TESTS:
Was a pump test made? ☐ Yes ☒ No If yes, by whom?
Yield: gal./min. with ft. draw down after hrs.
Temperature of water Was a chemical analysis made? ☐ Yes ☒ No
Was electric log made of well? ☐ Yes ☒ No

(11) WELL LOG:
CONFIDENTIAL LOG
Water Code Sec. 13752

Total depth 29 ft. Depth of completed well 29 ft.
Formation: *Describe by color, character, size of material, and structure.*

ft. to	ft.	
0	12	spongey clay
12	13	gravel
13	22	yellow clay
22	29	shale and rock

Two identical wells side by side



FOR OFFICIAL USE ONLY

Work started 10/14/63 19 , Completed 10/18/63 19

WELL DRILLER'S STATEMENT:
This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME R & B Drilling (Person, firm, or corporation) (Typed or printed)
Address RT. 1 Box 617-H
Ukiah, California

[SIGNED] Ralph Braun (Well Driller)

License No. 197854 Dated 11/12/63, 19

ORIGINAL
File with DWR

Page 1 of 1

RECEIVED
MAR 03 1993

STATE OF CALIFORNIA
WELL COMPLETION REPORT
Refer to Instruction Pamphlet

No. 407185

DWR USE ONLY — DO NOT FILL IN
17N17W29L01M
STATE WELL NO./STATION NO.
LATITUDE LONGITUDE
APN/TRS/OTHER

Owner's Well No. ____
Date Work Began 11-30-92 Ended 12-3-92
Local Permit Agency CO Health Dept
Permit No. 10442 Permit Date 10-30-92

GEOLOGIC LOG

ORIENTATION (✓) ✓ VERTICAL ___ HORIZONTAL ___ ANGLE ___ (SPECIFY)
DEPTH TO FIRST WATER ___ (Ft.) BELOW SURFACE

DEPTH FROM SURFACE Ft. to Ft.	DESCRIPTION *Describe material, grain size, color, etc.*
0 4	Light Brown Clay
4 11	Orange Sandy Clay
11 22	Tan Sandy Clay
22 38	orange Sandy Clay
38 47	Gravel 1/16 To 1/2"
47 150	Franciscan

TOTAL DEPTH OF BORING 150 (Feet)
TOTAL DEPTH OF COMPLETED WELL 150 (Feet)

WELL LOCATION

Address 44000 Little Lake Rd
City Mendocino
County Mendo.
APN Book 119 Page 10 Parcel 05
or Township 17N Range 17W Section 29 L
or Latitude ___ DEG. ___ MIN. ___ SEC. NORTH Longitude ___ DEG. ___ MIN. ___ SEC. WEST

LOCATION SKETCH

NORTH / WEST / EAST / SOUTH

Illustrate or Describe Distance of Well from Landmarks such as Roads, Buildings, Fences, Rivers, etc. PLEASE BE ACCURATE & COMPLETE.

ACTIVITY (✓)

✓ NEW WELL
MODIFICATION/REPAIR
___ Deepen
___ Other (Specify)
___ DESTROY *(Describe Procedures and Materials Under "GEOLOGIC LOG")*

PLANNED USE(S) (✓)

___ MONITORING
WATER SUPPLY
✓ Domestic
___ Public
___ Irrigation
___ Industrial
___ "TEST WELL"
___ CATHODIC PROTECTION
___ OTHER (Specify)

DRILLING METHOD Air Rotary FLUID ___

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH OF STATIC WATER LEVEL ___ (Ft.) & DATE MEASURED ___
ESTIMATED YIELD 6+ (GPM) & TEST TYPE Air Lift
TEST LENGTH 1 (Hrs.) TOTAL DRAWDOWN ___ (Ft.)
* *May not be representative of a well's long-term yield.*

CASING(S)

DEPTH FROM SURFACE Ft. to Ft.	BORE-HOLE DIA. (Inches)	TYPE (✓) BLANK	SCREEN	CONDUCTOR	FILL PIPE	MATERIAL/GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)
0 50	9	✓				PVC	5	Cl 200	
50 150	7		✓			11	11	11	.032

ANNULAR MATERIAL

DEPTH FROM SURFACE Ft. to Ft.	TYPE CEMENT (✓)	BENTONITE (✓)	FILL (✓)	FILTER PACK (TYPE/SIZE)
0 33	✓			
33 150				Gravel 8X16

ATTACHMENTS (✓)

___ Geologic Log
___ Well Construction Diagram
___ Geophysical Log(s)
___ Soil/Water Chemical Analyses
___ Other ___

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME THRA Drilling INC (PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)
ADDRESS 12251 Redwood 3Parks Dr CITY Fort Bragg STATE Ca ZIP 95437
Signed Todd (WELL DRILLER/AUTHORIZED REPRESENTATIVE)
DATE SIGNED 12-5-92
C-57 LICENSE NUMBER 583316

DWR 188 REV. 7-90

IF ADDITIONAL SPACE IS NEEDED, USE NEXT CONSECUTIVELY NUMBERED FORM

1676

ORIGINAL

File with DWR

STATE OF CALIFORNIA
THE RESOURCES AGENCY
DEPARTMENT OF WATER RESOURCES

WATER WELL DRILLERS REPORT

Do not fill in

No. 140367

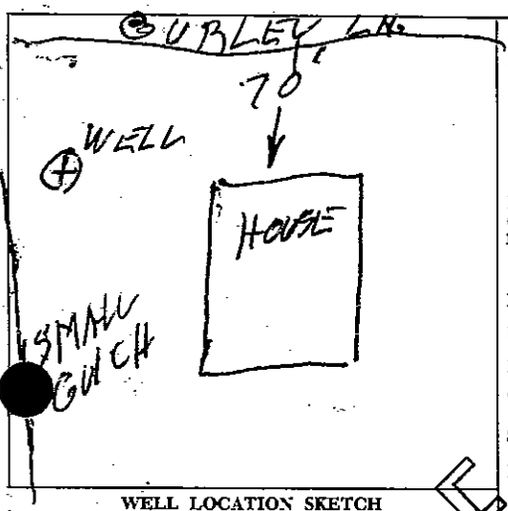
[redacted] of Intent No.
Local Permit No. or Date 8002 replaces #7721

119-090-004

State Well No.
Other Well No. 17N17W29D

(1)
Addre
City

(2) LOCATION OF WELL (See instructions):
County Mendocino Owner's Well Number AP 119-090-04
Well address if different from above 10650 Gurley Lane
Township Mendocino, CA 95460 Range Section
Distance from cities, roads, railroads, fences, etc.



WELL LOCATION SKETCH

(3) TYPE OF WORK:
New Well [X] Deepening [ ]
Reconstruction [ ]
Reconditioning [ ]
Horizontal Well [ ]
Destruction [ ] (Describe destruction materials and procedures in Item 12)

(4) PROPOSED USE:
Domestic [X]
Irrigation [ ]
Industrial [ ]
Test Well [ ]
Stock [ ]
Municipal [ ]
Other [ ]

(5) EQUIPMENT:
Rotary [ ] Reverse [ ]
Cable [X] Air [ ]
Other [ ] Bucket [X]

(6) GRAVEL PACK:
Yes [X] No [ ] Size 1/4"
Diameter of bore 26 and 10
Packed from 20 to 59 ft.

(7) CASING INSTALLED:
Steel [ ] Plastic [X] Concrete [ ]

From ft.	To ft.	Dia. in.	Gage or Wall
1 ft.	above grd.		
	59	5	1/4"

(8) PERFORATIONS:
Type of perforation or size of screen

From ft.	To ft.	Slot size
20	59	1/8"

(9) WELL SEAL:
Was surface sanitary seal provided? Yes [X] No [ ] If yes, to depth 17 ft.
Were strata sealed against pollution? Yes [ ] No [X] Interval ft.
Method of sealing Concrete

(10) WATER LEVELS:
Depth of first water, if known 20 ft.
Standing level after well completion ft.

(11) WELL TESTS:
Was well test made? Yes [X] No [ ] If yes, by whom? Driller
Type of test Pump [ ] Bailer [X] Air lift [ ]
Depth to water at start of test ft. At end of test ft
Charge 4 1/2 gal/min after 3 hours Water temperature
Chemical analysis made? Yes [ ] No [X] If yes, by whom?
Was electric log made? Yes [ ] No [X] If yes, attach copy to this report

(12) WELL LOG: Total depth 59 ft. Depth of completed well 60 ft.

from ft.	to	ft. Formation (Describe by color, character, size or material)
0	-	12 Brown Clay
12	-	15 White sandy clay
15	-	20 Blue rock
20	-	29 Black rock
29	-	59 Blue and black rock

Work started May 16, 1988 Completed May 25, 1988

WELL DRILLER'S STATEMENT:
This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief

SIGNED John W Murray (Well Driller)
NAME Murray Well Drilling (Person, firm, or corporation) (Typed or printed)
Address 30520 Sherwood Rd.
City Fort Bragg, Ca. Zip 95437
License No. 268792 Date of this report June 25, 1988

CONFIDENTIAL
NOT FOR PUBLIC USE
WATER CODE SEC. 13752

DWR 188 (REV. 7-76) IF ADDITIONAL SPACE IS NEEDED, USE NEXT CONSECUTIVELY NUMBERED FORM

STATE OF CALIFORNIA

WELL COMPLETION REPORT

No. 0924893

DWR USE ONLY — DO NOT FILL IN

17N12W29

STATE WELL NO. STATION NO.

LATITUDE LONGITUDE

APN / TRS / OTHER

OWNER'S WELL No. 5578

Date Work Began 9/9/05 Ended 9/9/05

Local Permit Agency MENDOCINO

Permit No. WW20432 Permit Date 8-16-2005

GEOLOGIC LOG

ORIENTATION Vertical Degree of Angle .....

DEPTH TO FIRST WATER .....(ft.) BELOW SURFACE

DEPTH FROM SURFACE Ft.	Ft.	DESCRIPTION
0	2	topsoil
2	20	brown clay
20	25	weathered greenstone
25	140	greenstone w/ shale

Address 10651 GURLEY LANE

City MENDOCINO County MENDOCINO

Apn Book 119 Page 100 Parcel 01

or

Township ..... Range ..... Section .... 1/4 ..... 1/4

or

Latitude .... NORTH Longitude .... WEST

Deg. Min. Sec. Deg. Min. Sec.

LOCATION SKETCH

ACTIVITY NEW WELL PLANNED USE(S) Domestic Water

DRILLING METHOD ROTARY AIR FLUID Bentonite

DEPTH OF STATIC WATER LEVEL 20 (Ft.) & DATE MEASURED Sep 9, 2005

ESTIMATED YIELD * 1.5 (G.P.M.) & TEST TYPE Airlift

TEST LENGTH. 2 (Hrs.) TOTAL DRAWDOWN 135 (FT.)

*May not be representative of a well's long-term yield.

TOTAL DEPTH OF BORING 140 (Feet)

TOTAL DEPTH OF COMPLETED WELL 140 (Feet)

CASING

DEPTH FROM SURFACE Ft.	To Ft.	BORE-HOLE DIA.	TYPE	Material / Grade	Dia.	Gauge	Slot size
0	20	10 5/8	Blank	F480 PVC	5	160	
20	40	8 3/4	Blank	F480 PVC	5	160	
40	140	7 1/2	Perfs	F480 PVC	5	200	Factor

ANNULAR MATERIAL

DEPTH FROM SURFACE Ft.	To Ft.	Seal Material	Filter Pack (Type / Size)
0	20	Bentonite	
20	140		Pea Gravel

Attachments

no Geologic Log

no Well Construction Diagram

no Geophysical Logs

no Soil Water Chemical Analyses

no Other

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME FISCH BROS. DRILLING, INC.

(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

5001 Gravenstein Hwy No. Sebastopol CA 9547

Signed Dale Theiss 09/30/05 399226

WELL DRILLER / AUTHORIZED REPRESENTATIVE DATE SIGNED C-57 LICENSE NUMBER

Appendix B

Public Outreach Materials

Mendocino Unified School District
Jason Morse, Superintendent
44141 Little Lake Road ▪▪ PO Box 1154 ▪▪ Mendocino, CA 95460
Phone: 707.937.5868 Fax: 707.937.0714 http://www.mendocinousd.org

NOTICE OF AQUIFER TEST

Property Owner	Mendocino Unified School District
Site Address	44100 Little Lake Road, Mendocino
Assessor Parcel	119-100-03
Contact Person	Ryan Crawford: Ryan.Crawford@ghd.com, (707) 236-1541
Mailing Address	2235 Mercury Way, Suite 150, Santa Rosa, CA 95407
Purpose of Test	To evaluate capacity and drawdown effects of new wells at the property for the MUSD school's existing water use as apart of the MCCSD Drought Tolerance Emergency Water Supply and Storage Improvements project.

NOTICE IS HEREBY GIVEN THAT AN AQUIFER TEST (one of up to six) WILL BE CONDUCTED

ON TUESDAY, AUGUST 20, 2024 BEGINNING AT 9:00 AM

For the purpose of testing water quantity and observing any impacts resulting from groundwater extraction during the test. This test shall continue for a period of 72-hours from the time the test is begun. If you notice any change in your well level or any other condition that indicates that your well is being affected by this test, you should immediately notify:

GHD - Ryan.Crawford@ghd.com

Tel. # (707) 236-1541

Each additional test will be performed beginning each Wednesday until all tests are completed, estimated by September 26th.

Mendocino Unified School District
Jason Morse, Superintendent
44141 Little Lake Road ▪▪ PO Box 1154 ▪▪ Mendocino, CA 95460
Phone: 707.937.5868 Fax: 707.937.0714 http://www.mendocinousd.org

May 30, 2025

Mendocino Resident/Neighbor
California Postal Code 95460

State Water Resources Control Board
Agreement No.: D2202005
Project No.: 2300584-001C
State Department of Water Resources:
Agreement No.: 4600014624

SUBJECT: Pump Testing for New Test Wells

Dear Resident:

The Mendocino Unified School District (MUSD) is constructing new test wells at their water storage and well site located northeast of the Mendocino K-8 School, neighboring your property. Following the installation of these test wells, a 72-hour pump test will be conducted for each. Pump tests are anticipated to be performed beginning August 20th and span approximately 4 to 5 weeks .

Your water well is anticipated to be beyond the influence of the proposed pump tests; however, if you feel that your well may be hydrologically connected and influenced by the test wells please contact GHD or MUSD to request that your well be included in the monitoring well program. Request to opt into monitoring must be made to GHD or MUSD a minimum of 72 hours prior to the beginning of the pump tests (August 17th). Should you opt into our monitoring program you agree to the following:

- You will not operate your well 24 hours prior to and during the pump testing period. Testing is anticipated to span 4-5 weeks beginning August 20th.
- You will provide access to your wellhead to allow for either: (1) installation of a digital pressure logger (transducer) to monitor groundwater levels within your well during the testing period or (2) periodic manual water level measurements during the pump testing period.
- You will allow a surveyor to access your well to survey the elevation of your well, if needed.
- You will provide GHD with records (or estimates if no records are available) of: (1) previous hydrological studies associated with your well(s), (2) well construction information including: total depth, pump setting, well screen zones, surface seal depth and material, and geologic log (if available), and (3) pumping volumes and schedule (daily, monthly, and yearly if available).

GHD and MUSD shall not be held liable for any damages to private property except to the extent caused by its own gross negligence. By opting into the well testing, you agree to release MUSD and GHD from any claims arising out of or related to the monitoring activities. To the extent permitted by law, you further agree to

indemnify and hold harmless MUSD and GHD from any such claims, except to the extent caused by MUSD's or GHD's own gross negligence.

During the testing period, if you feel that the water level in your well has been influenced, please contact MUSD or GHD as soon as possible so that we may add such information to our pump test evaluation and potentially collect groundwater level measurements from your well. Please include the following information:

- Static water level (depth from the surface to water level when pump is not operating, if your measurement is from the top of the well casing, please note the height of the well casing from the ground surface);
- Frequency of pump operation (day and hours of operation, if possible); and,
- How was your well influenced?

Attached is a location map showing the location of the property on which the pump tests will be performed in relation to your property.

Please email the requested information and any other pertinent information to MUSD's appointed contractor representative with GHD Inc. - Ryan Crawford at (707) 496-8070 or email at ryan.crawford@ghd.com or send to Ryan Crawford at our office:

GHD
P.O. Box 7967
Santa Rosa CA, 95407, USA.

Thank you for your time and willingness to assist us with this monitoring program.

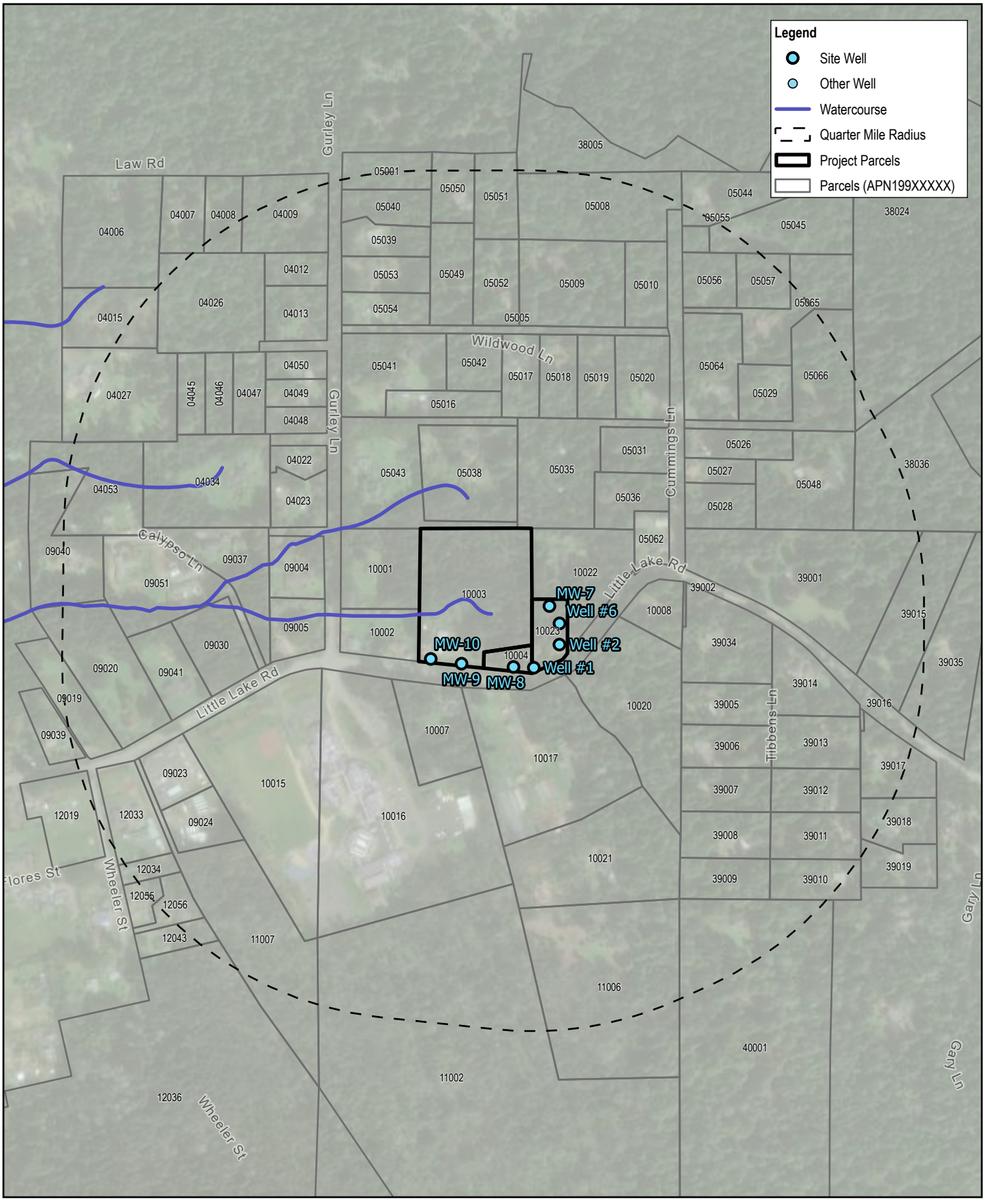
Best Regards,



Jason Morse
MUSD Superintendent

cc. GHD Inc. (Ryan Crawford)

Attachments:
Figure 1 – Identified Properties within 1/4 Mile of Pump Test



Paper Size ANSI A

0 100 200 300 400 500

Feet

Map Projection: Mercator Auxiliary Sphere
Horizontal Datum: WGS 1984
Grid: WGS 1984 Web Mercator Auxiliary Sphere

N

GHD

Mendocino City CSD
PW Drought Tolerance Supply and Storage Improvements

Identified Properties within 1/4 Mile of Pump Test

Project No. **12584992**
Revision No. **-**
Date **May 2025**

FIGURE 1

\\ghdnet\ghd\US\Azure\EastUS\12584992\GIS\Maps\Deliverables\12584992_Parcels_2025.aprx
Print date: 12 May 2025 - 13:52

Data source: Reference - Full: Esri Community Maps Contributors, California State Parks, © OpenStreetMap, Microsoft, Esri, TomTom, Garmin, SafeGraph, GeoTechnologies, Inc, METI/NASA, USGS, Bureau of Land Management, EPA, NPS, US Census Bureau, USDA, USFWS
World Imagery: Maxar. Created by: ethompson3

Mendocino Unified School District
Jason Morse, Superintendent
44141 Little Lake Road ▪▪ PO Box 1154 ▪▪ Mendocino, CA 95460
Phone: 707.937.5868 Fax: 707.937.0714 http://www.mendocinousd.org

May 30, 2025

Mendocino Resident/Neighbor
California Postal Code 95460

State Water Resources Control Board
Agreement No.: D2202005
Project No.: 2300584-001C
State Department of Water Resources:
Agreement No.: 4600014624

SUBJECT: Pump Testing for New Test Wells

Dear Resident:

The Mendocino Unified School District (MUSD) is constructing new test wells at their water storage and well site located northeast of the Mendocino K-8 School, neighboring your property. Following the installation of these test wells, a 72-hour pump test will be conducted for each. Pump tests are anticipated to be performed beginning August 20th and span approximately 4 to 5 weeks.

Your water well is potentially within the influence of the proposed pump tests and MUSD is offering to monitor your well during the pumping tests. You are not required to participate in this monitoring program, but your inclusion would assist in the understanding of the local aquifer characteristics and help make sure that your well is not adversely effected by any new wells. Requirements for opting into the monitoring well program are attached.

Pre-pump test well monitoring is scheduled to begin in June and we would like to install digital pressure loggers (transducers) into participant wells as early as possible to collect background data prior to testing. If you want your well(s) to be monitored, please respond to this notice as soon as possible.

Attached is a location map showing the wells which may be sampled as part of this monitoring program. Please contact MUSD's appointed contractor representative with GHD Inc. - Ryan Crawford at (707) 496-8070 or email at ryan.crawford@ghd.com if you are willing to participate in this program or have any questions. Thank you for your time and willingness to assist us with this monitoring program.

Best Regards,



Jason Morse
MUSD Superintendent
cc. GHD Inc. (Ryan Crawford)

Attachments:

Monitoring Program Requirements

Figure 1 – Identified Properties within 1/4 Mile of Pump Test

Figure 2 – Target Public Monitoring Well Locations

Monitoring Program Requirements

Requests to opt into the monitoring program must be made to MUSD or MUSD's appointed contractor GHD, a minimum of 72 hours prior to the beginning of the pump tests (August 17th). By opting in to the monitoring program you agree to the following:

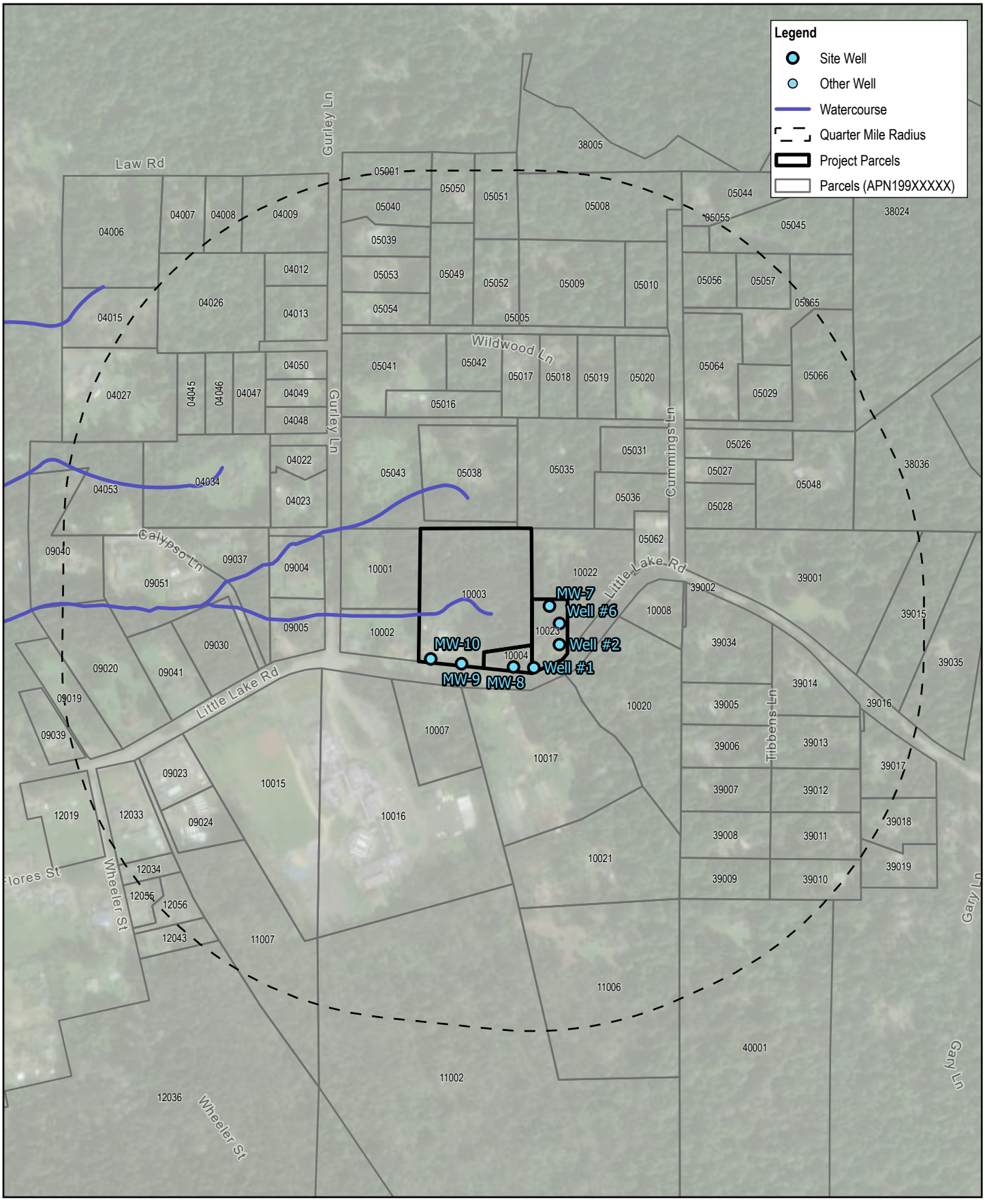
- You will not operate your well 24 hours prior to and during the pump testing period. Testing is anticipated to span 4-5 weeks beginning August 20th.
- You will provide access to your well for inspection and remove your wellhead to allow for either: (1) installation of a digital pressure logger (transducer) to monitor groundwater levels within your well during the testing period or (2) periodic manual water level measurements during the pump testing period.
- You will allow a surveyor to access your well to survey the elevation of your well, if needed.

Additionally, you agree to provide/estimate the following information, if available:

- Provide previous hydrological studies associated with your well(s).
- Provide well construction information including: total depth, pump setting, well screen zones, surface seal depth and material, and geologic log (if available).
- Estimated pumping volumes and schedule (daily, monthly, and yearly if available).

A transducer would monitor groundwater levels prior to and during the pump testing period to obtain groundwater conditions and you would use your well as normal until 24 hours prior to the pump test. If manual water level measurements are taken GHD personnel will require access to your well daily beginning 24 hours prior to the pump testing period until its conclusion.

GHD and MUSD shall not be held liable for any damages to private property except to the extent caused by its own gross negligence. By opting into the well testing, you agree to release MUSD and GHD from any claims arising out of or related to the monitoring activities. To the extent permitted by law, you further agree to indemnify and hold harmless MUSD and GHD from any such claims, except to the extent caused by MUSD's or GHD's own gross negligence.



Paper Size ANSI A

0 100 200 300 400 500

Feet

Map Projection: Mercator Auxiliary Sphere
Horizontal Datum: WGS 1984
Grid: WGS 1984 Web Mercator Auxiliary Sphere

N

GHD

Mendocino City CSD
PW Drought Tolerance Supply and Storage Improvements

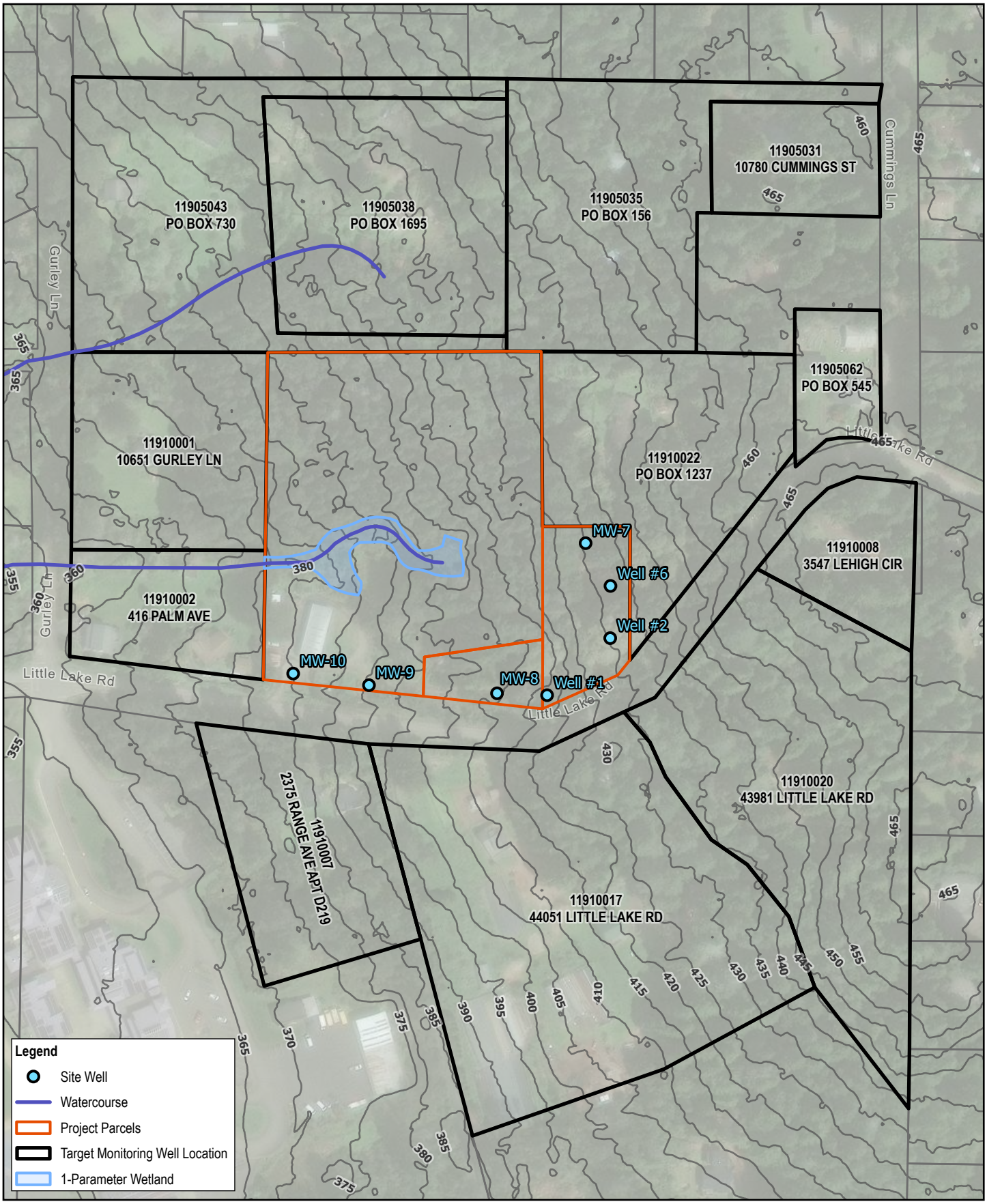
Identified Properties within 1/4 Mile of Pump Test

Project No. **12584992**
Revision No. **-**
Date **May 2025**

FIGURE 1

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Print date: 12 May 2025 - 13:52

Data source: Reference - Full: Esri Community Maps Contributors, California State Parks, © OpenStreetMap, Microsoft, Esri, TomTom, Garmin, SafeGraph, GeoTechnologies, Inc, METI/NASA, USGS, Bureau of Land Management, EPA, NPS, US Census Bureau, USDA, USFWS
World Imagery: Maxar. Created by: ethompson3



Paper Size ANSI A

0 100 200 300

Feet

Map Projection: Mercator Auxiliary Sphere
Horizontal Datum: WGS 1984
Grid: WGS 1984 Web Mercator Auxiliary Sphere

N

GHD

Mendocino City CSD
PW Drought Tolerance Supply and Storage Improvements

Target Private Monitoring Well Locations

Project No. **12584992**
Revision No. **-**
Date **May 2025**

FIGURE 2

\\ghdnet\ghd\US\Azure\EastUS\12584992\GIS\Maps\Deliverables\12584992_Parcels_2025.aprx
Print date: 12 May 2025 - 14:29

Data source: World Imagery: Maxar, Microsoft
Reference - Full: Esri Community Maps Contributors, California State Parks, © OpenStreetMap, Microsoft, Esri, TomTom, Garmin, SafeGraph, GeoTechnologies, Inc, METI/NASA, USGS, Bureau of Land Management, EPA, NPS, US Census Bureau, USDA, USFWS. Created by: ethompson3

Advertising Order Confirmation

Fort Bragg Advocate-News

The Mendocino Beacon

Ad Order Number	Customer	Payor Customer	PO Number
0006912588	GHD	GHD	
Sales Representative	**Customer Account**	**Payor Account**	**Ordered By**
Audrey Taylor	3874734	3874734	
Order Taker	**Customer Address**	**Payor Address**	**Customer Fax**
Audrey Taylor	PO BOX 7967 SANTA ROSA, CA 95407	PO BOX 7967 SANTA ROSA, CA 95407	
Order Source	**Customer Phone**	**Payor Phone**	**Customer EMail**
Select Source	707-236-1547	707-236-1547	Coleton.Golden@ghd.com

Current Queue	Invoice Text
Ready	Notice of Aquifer Test

Tear Sheets	Affidavits	Blind Box	Materials	Promo Type	Special Pricing
0	0				

Advertising Order Confirmation

Fort Bragg Advocate-News

The Mendocino Beacon

Ad Number	Color	Production Color	Ad Attributes	Production Method	Production Notes
0006912588-01				AdBooker	

External Ad Number	Pick Up	Ad Type	Released for Publication
		Legal Liner	

NOTICE OF AQUIFER TEST

Property Owner: Mendocino Unified School District Site Address: 44100 Little Lake Road, Mendocino, CA 95460
Assessor Parcel Number: 119-100-03
Contact person: Ryan Crawford
Mailing Address: 2235 Mercury Way, Santa Rosa, CA 95407
Telephone: 707-236-1541
Purpose of test: To evaluate capacity and drawdown effects of new wells at the property for the MUSD school's existing water use as apart of the MCCSD Drought Tolerance Emergency Water Supply and Storage Improvements project.
NOTICE IS HEREBY GIVEN THAT AN AQUIFER TEST (one of up to six) WILL BE CONDUCTED ON WEDNESDAY **AUGUST 20, 2024**, BEGINNING AT 9:00 AM for the purpose of testing water quantity and observing any impacts resulting from groundwater extraction during the test. This test shall continue for a period of 72-hours from the time the test is begun. If you notice any change in your well level or any other condition that indicates that your well is being affected by this test, you should immediately notify: GHD - Ryan.Crawford@ghd.com Tel. # (707) 236-1541. Each additional test will be performed beginning each Wednesday until all tests are completed.
Publish: August 14, 2025

Product	Requested Placement	Requested Position	Run Dates	# Inserts
Fort Bragg Advocate	Legals CLS NC	General Legal NC - 1076~	08/14/25	1

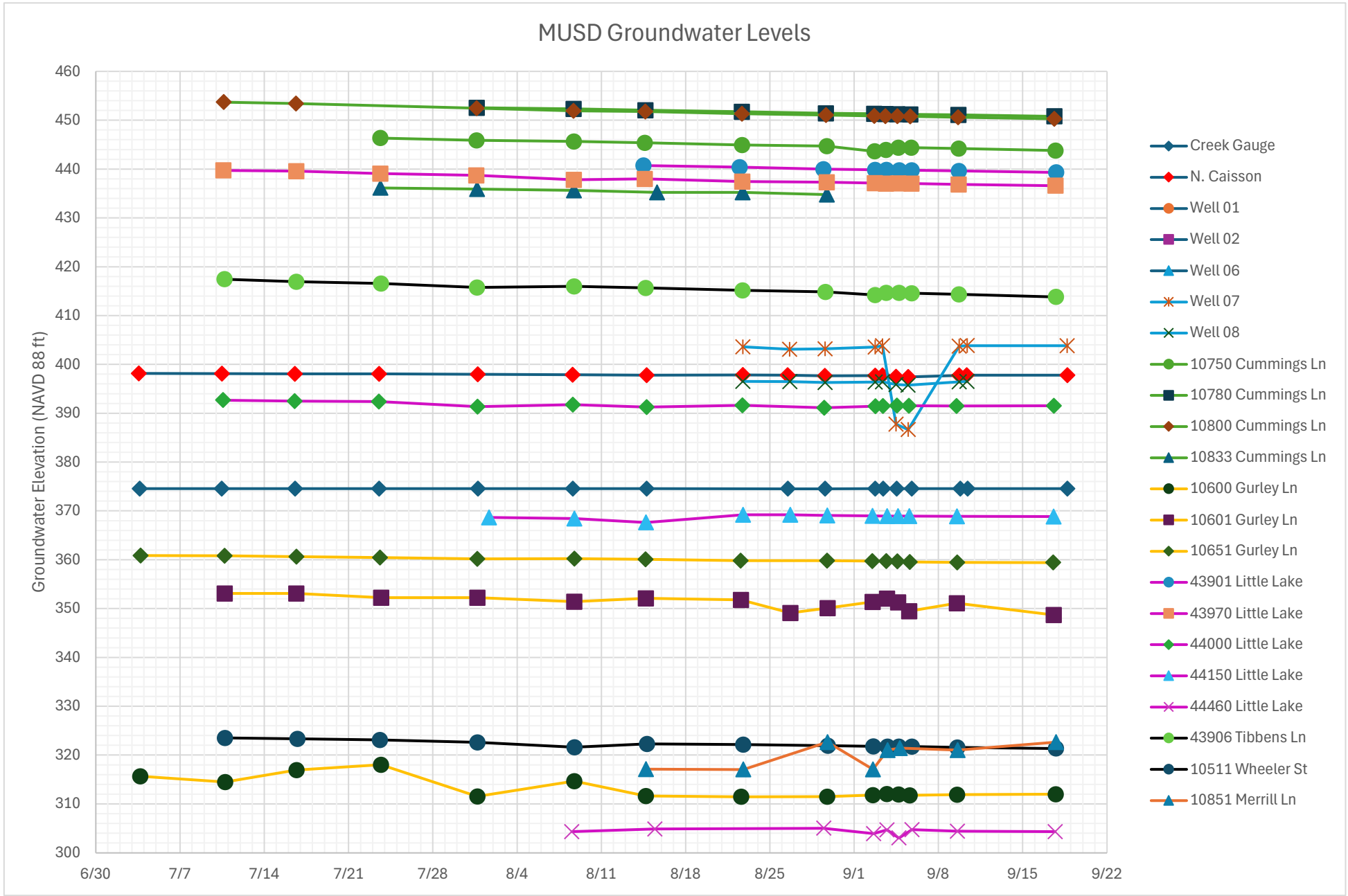
Order Charges:

Net Amount	Tax Amount	Total Amount	Payment Amount	Amount Due
105.24	0.00	105.24	0.00	**$105.24**

Please note: If you pay by bank card, your card statement will show "CAL NEWSPAPER ADV" or "CALIFORNIA NEWSPAPER ADVERTISING SERVICES", depending on the type of card used.

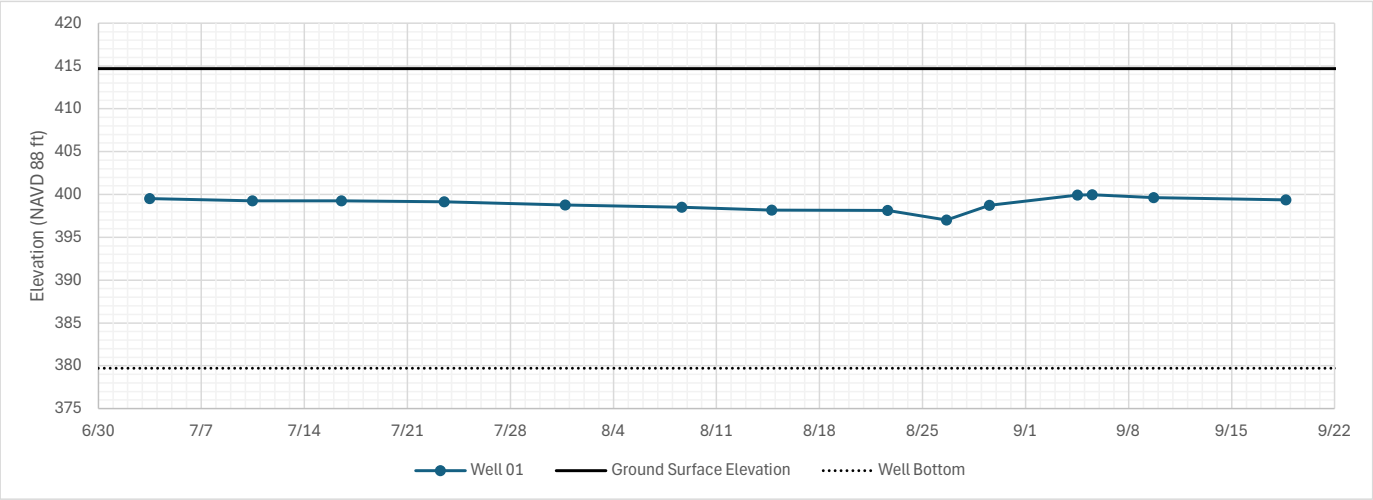
Appendix C

Depth-to-Water Measurements


MUSD Groundwater Levels
Groundwater Elevation (NAVD 88 ft)
460
450
440
430
420
410
400
390
380
370
360
350
340
330
320
310
300
6/30
7/7
7/14
7/21
7/28
8/4
8/11
8/18
8/25
9/1
9/8
9/15
9/22
Creek Gauge
N. Caisson
Well 01
Well 02
Well 06
Well 07
Well 08
10750 Cummings Ln
10780 Cummings Ln
10800 Cummings Ln
10833 Cummings Ln
10600 Gurley Ln
10601 Gurley Ln
10651 Gurley Ln
43901 Little Lake
43970 Little Lake
44000 Little Lake
44150 Little Lake
44460 Little Lake
43906 Tibbens Ln
10511 Wheeler St
10851 Merrill Ln

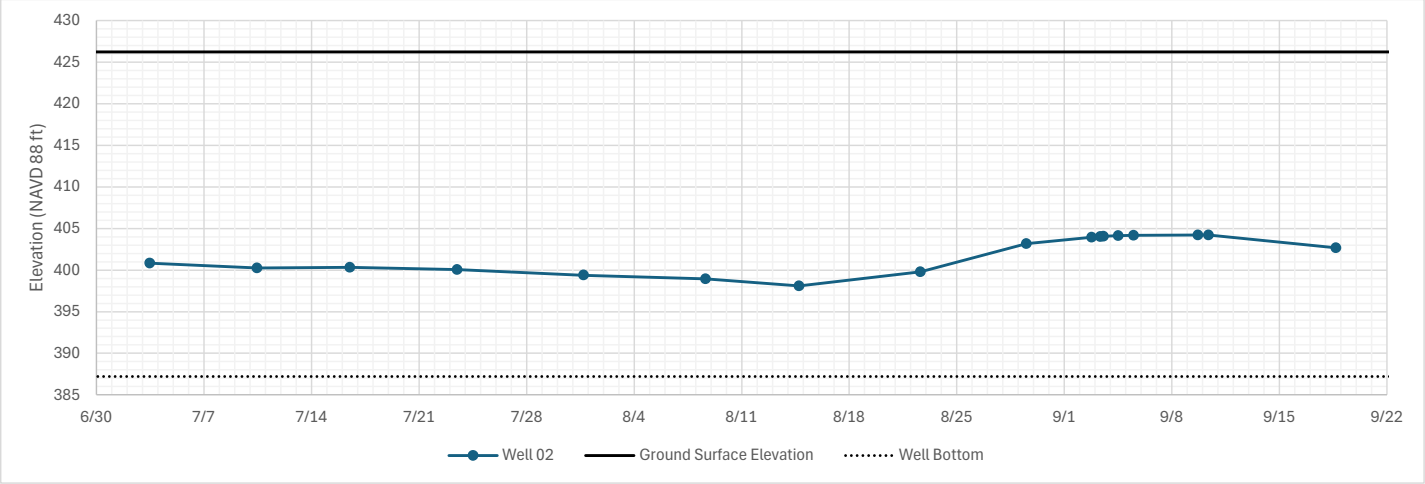
	Ground Elevation	Well Total Depth	Casing Height
Well 01	414.70	35' + Casing Height	

Date-Time	GWE	Casing Height Measured	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/3/2025 11:35	399.51	0.875	Well 01	7/3/2025	11:35	16.07	Programed at 14:40 - 1hr interval, installed at 14:45 @ 33' pumping at 6.5 gpm
7/10/2025 11:15	399.26	0.875	Well 01	7/10/2025	11:15	16.32	6.5 gpm Pumping
7/16/2025 12:35	399.27	0.875	Well 01	7/16/2025	12:35	16.31	Pumping ~6.4 GPM
7/23/2025 11:58	399.13	0.875	Well 01	7/23/2025	11:58	16.45	Pumping
7/31/2025 17:33	398.78	0.875	Well 01	7/31/2025	17:33	16.80	6 gpm
8/8/2025 15:35	398.52	0.875	Well 01	8/8/2025	15:35	17.06	Pumping at 5.75 gpm
8/14/2025 18:01	398.16	0.875	Well 01	8/14/2025	18:01	17.42	Pumping at 5.5 gpm, Weeks Drilling performed pump test around 10:30AM at Well 06
8/22/2025 15:10	398.12	0.875	Well 01	8/22/2025	15:10	17.46	Pumping 8 gpm
8/26/2025 15:18	397.00	0.875	Well 01	8/26/2025	15:18	18.58	Pumping at 8 gpm
8/29/2025 12:58	398.73	0.875	Well 01	8/29/2025	12:58	16.85	Not pumping, storage tanks are full per Travis (MUSD staff)
9/2/2025 19:05		0.250	Well 01	9/2/2025	19:05	15.60	Difficult to measure, casing height changed (casing broken), Weeks Drilling redeveloped
9/3/2025 8:30		0.250	Well 01	9/3/2025	8:30	14.90	Difficult to measure, casing still broken, indicator activates when casing is touched
9/4/2025 12:32	399.93	1.083	Well 01	9/4/2025	12:32	15.85	Casing height changed (new casing), reduced sensitivity of indicator to measure, still difficult
9/5/2025 12:34	399.95	1.083	Well 01	9/5/2025	12:34	15.83	Approximate measurement
9/9/2025 17:10	399.61	1.083	Well 01	9/9/2025	17:10	16.17	0
9/18/2025 16:43	399.37	1.083	Well 01	9/18/2025	16:43	16.41	36 feet deep from TOC



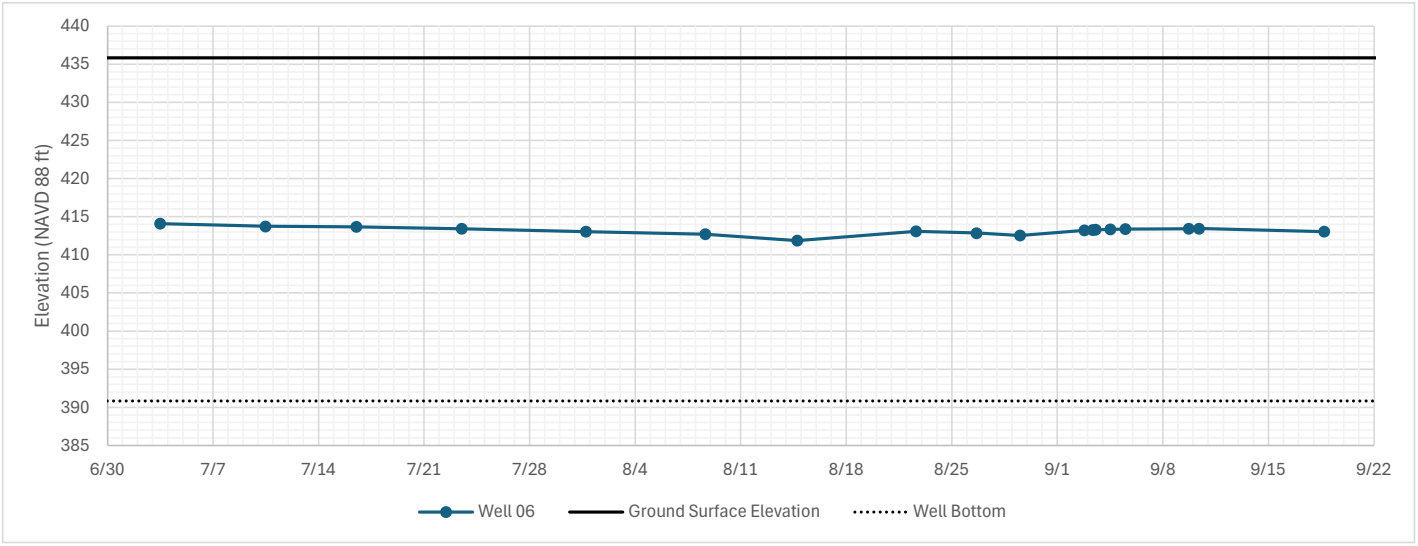
Well 02	Ground Elevation	Well Total Depth	Casing Height
	426.21	40' + Casing Height	

Date-Time	GWE	Casing Height Measured	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/3/2025 11:40	400.84	1	Well 02	7/3/2025	11:40	26.37	Apparently Pumping, Totalizer not working
7/10/2025 11:20	400.24	1	Well 02	7/10/2025	11:20	26.97	Not Pumping, totalizer out
7/16/2025 12:13	400.35	1	Well 02	7/16/2025	12:13	26.86	Not Pumping
7/23/2025 11:49	400.06	1	Well 02	7/23/2025	11:49	27.15	0
7/31/2025 17:28	399.39	1	Well 02	7/31/2025	17:28	27.82	0
8/8/2025 15:32	398.96	1	Well 02	8/8/2025	15:32	28.25	0
8/14/2025 17:57	398.09	1	Well 02	8/14/2025	17:57	29.12	Weeks Drilling performed pump test around 10:30AM at Well 06
8/22/2025 15:05	399.81	1	Well 02	8/22/2025	15:05	27.40	0
8/29/2025 12:49	403.17	0.92	Well 02	8/29/2025	12:49	23.95	Weeks Drilling replaced well head around 8/27, casing height has changed
9/2/2025 18:51	403.96	0.92	Well 02	9/2/2025	18:51	23.16	Weeks Drilling redeveloped Well 1 today
9/3/2025 8:22	404.02	0.92	Well 02	9/3/2025	8:22	23.10	0
9/3/2025 13:04	404.04	0.92	Well 02	9/3/2025	13:04	23.08	0
9/4/2025 12:16	404.15	0.92	Well 02	9/4/2025	12:16	22.97	Measured twice
9/5/2025 12:17	404.19	0.92	Well 02	9/5/2025	12:17	22.93	0
9/9/2025 17:04	404.20	0.92	Well 02	9/9/2025	17:04	22.92	0
9/10/2025 9:20	404.20	0.92	Well 02	9/10/2025	9:20	22.92	0
9/18/2025 16:17	402.67	0.92	Well 02	9/18/2025	16:17	24.45	Well recovering, 40 feet deep from TOC



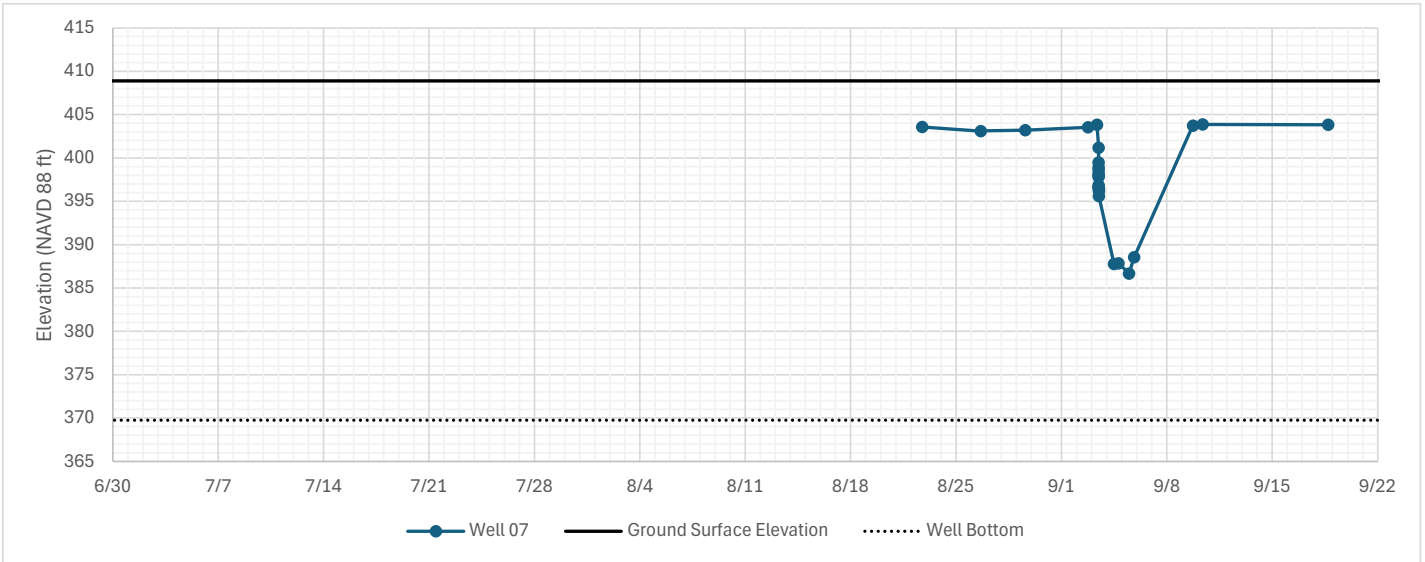
	Ground Elevation	Well Total Depth	Casing Height
Well 06	435.85	45' + Casign Height	

Date-Time	GWE	Casing Height	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/3/2025 11:45	414.08	0.83	Well 06	7/3/2025	11:45	22.60	Programed at 13:10 - 1hr interval, installed at 13:15 @ 42.5'
7/10/2025 11:25	413.73	0.83	Well 06	7/10/2025	11:25	22.95	0
7/16/2025 12:02	413.68	0.83	Well 06	7/16/2025	12:02	23.00	0
7/23/2025 11:37	413.42	0.83	Well 06	7/23/2025	11:37	23.26	0
7/31/2025 17:23	413.03	0.83	Well 06	7/31/2025	17:23	23.65	0
8/8/2025 15:27	412.70	0.83	Well 06	8/8/2025	15:27	23.98	0
8/14/2025 17:50	411.87	1.50	Well 06	8/14/2025	17:50	25.48	New 8 inch tall access port installed, Weeks Drilling performed pump test around 10:30AM
8/22/2025 15:00	413.09	1.50	Well 06	8/22/2025	15:00	24.26	Gray access port
8/26/2025 15:09	412.85	1.50	Well 06	8/26/2025	15:09	24.50	Gray access port
8/29/2025 12:38	412.53	1.50	Well 06	8/29/2025	12:38	24.82	Gray access port
9/2/2025 18:41	413.20	1.50	Well 06	9/2/2025	18:41	24.15	Gray access port, Weeks Drilling redeveloped Well 1 today
9/3/2025 8:18	413.27	1.50	Well 06	9/3/2025	8:18	24.08	Gray access port
9/3/2025 13:00	413.29	1.50	Well 06	9/3/2025	13:00	24.06	Gray access port
9/4/2025 12:06	413.35	1.50	Well 06	9/4/2025	12:06	24.00	Gray access port, measured twice
9/5/2025 12:10	413.39	1.50	Well 06	9/5/2025	12:10	23.96	Gray access port
9/9/2025 16:57	413.42	1.50	Well 06	9/9/2025	16:57	23.93	Gray access port
9/10/2025 9:28	413.44	1.50	Well 06	9/10/2025	9:28	23.91	Gray access port
9/18/2025 16:28	413.03	1.50	Well 06	9/18/2025	16:28	24.32	Gray access port, 45 feet deep from TOC



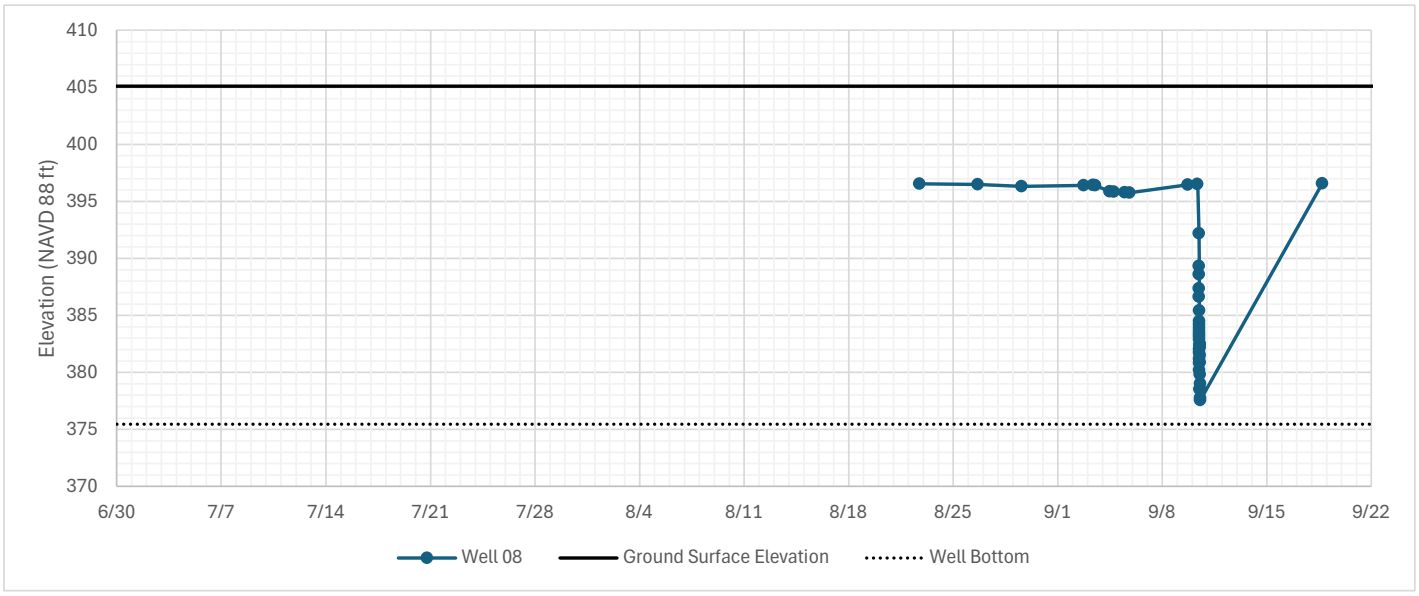
	Ground Elevation	Well Total Depth	Casing Height
Well 07	408.88	41.16	2.04

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
8/22/2025 18:03	403.58	Well 07	8/22/2025	18:03	7.34	0
8/26/2025 15:35	403.11	Well 07	8/26/2025	15:35	7.81	0
8/29/2025 14:08	403.19	Well 07	8/29/2025	14:08	7.73	0
9/2/2025 18:11	403.54	Well 07	9/2/2025	18:11	7.38	Measured twice, Weeks Drilling redeveloped Well 1 today
9/3/2025 8:38	403.82	Well 07	9/3/2025	8:38	7.10	0
9/3/2025 11:00	401.18	Well 07	9/3/2025	11:00	9.74	Pump test at 6gpm, pump started before this measurement taken
9/3/2025 11:01	399.49	Well 07	9/3/2025	11:01	11.43	Pump test
9/3/2025 11:02	398.92	Well 07	9/3/2025	11:02	12.00	Pump test
9/3/2025 11:03	398.62	Well 07	9/3/2025	11:03	12.30	Pump test
9/3/2025 11:04	398.18	Well 07	9/3/2025	11:04	12.74	Pump test
9/3/2025 11:05	398.00	Well 07	9/3/2025	11:05	12.92	Pump test
9/3/2025 11:06	397.80	Well 07	9/3/2025	11:06	13.12	Pump test
9/3/2025 11:10	396.58	Well 07	9/3/2025	11:10	14.34	Pump test
9/3/2025 11:15	396.87	Well 07	9/3/2025	11:15	14.05	Pump test
9/3/2025 11:20	396.66	Well 07	9/3/2025	11:20	14.26	Pump test
9/3/2025 11:25	396.44	Well 07	9/3/2025	11:25	14.48	Pump test
9/3/2025 11:30	396.19	Well 07	9/3/2025	11:30	14.73	Pump test
9/3/2025 11:45	395.60	Well 07	9/3/2025	11:45	15.32	Pump test
9/4/2025 11:42	387.76	Well 07	9/4/2025	11:42	23.16	0
9/4/2025 18:38	387.86	Well 07	9/4/2025	18:38	23.06	0
9/5/2025 11:40	386.65	Well 07	9/5/2025	11:40	24.27	0
9/5/2025 19:56	388.53	Well 07	9/5/2025	19:56	22.39	Switched to backup generator before measurement, well drawing down
9/9/2025 17:27	403.72	Well 07	9/9/2025	17:27	7.20	0
9/10/2025 9:13	403.86	Well 07	9/10/2025	9:13	7.06	0
9/18/2025 16:55	403.84	Well 07	9/18/2025	16:55	7.08	0



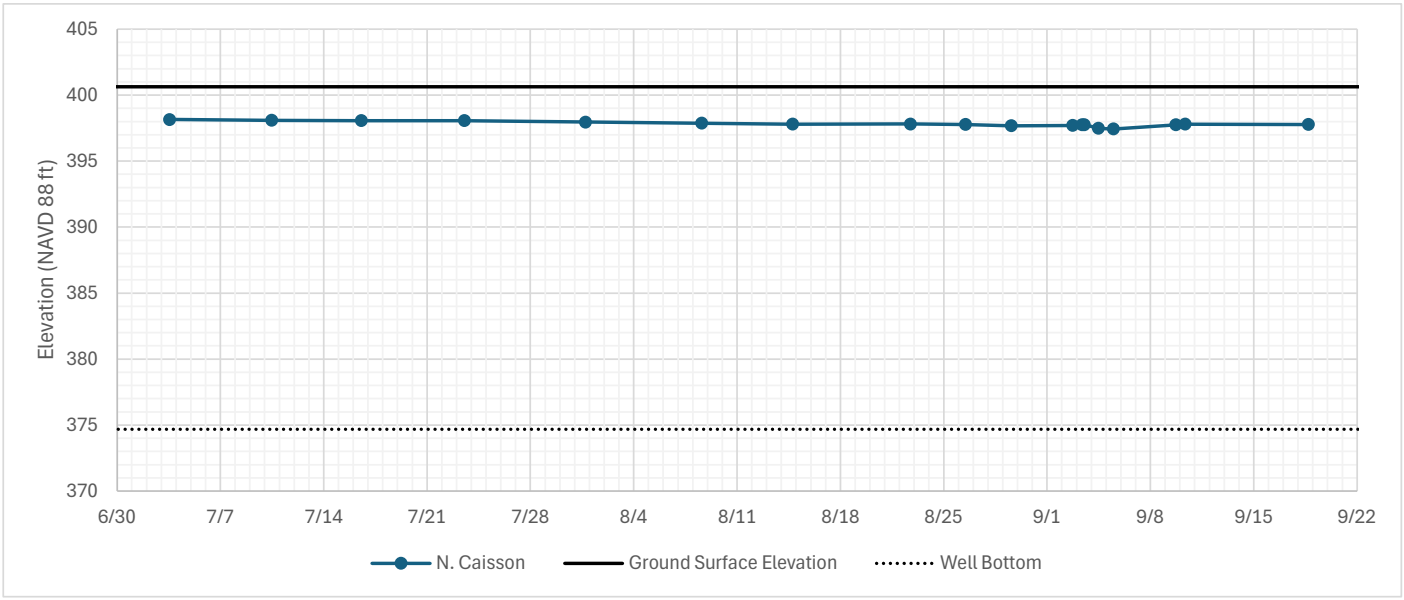
	Ground Elevation	Well Total Depth	Casing Height
Well 08	405.10	31.83	2.17

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
8/22/2025 18:00	396.54	Well 08	8/22/2025	18:00	10.73	0
8/26/2025 15:55	396.47	Well 08	8/26/2025	15:55	10.80	0
8/29/2025 14:01	396.31	Well 08	8/29/2025	14:01	10.96	0
9/2/2025 18:06	396.39	Well 08	9/2/2025	18:06	10.88	Measured twice, Weeks Drilling redeveloped Well 1 today
9/3/2025 8:42	396.41	Well 08	9/3/2025	8:42	10.86	0
9/3/2025 12:26	396.40	Well 08	9/3/2025	12:26	10.87	0
9/4/2025 11:26	395.87	Well 08	9/4/2025	11:26	11.40	0
9/4/2025 18:34	395.82	Well 08	9/4/2025	18:34	11.45	0
9/5/2025 11:35	395.77	Well 08	9/5/2025	11:35	11.50	0
9/5/2025 19:40	395.74	Well 08	9/5/2025	19:40	11.53	Switched to backup generator at Well 7 before measurement
9/9/2025 17:24	396.44	Well 08	9/9/2025	17:24	10.83	0
9/10/2025 8:45	396.51	Well 08	9/10/2025	8:45	10.76	0
9/10/2025 10:56	392.17	Well 08	9/10/2025	10:56	15.10	well recovering from pump flow rate calibration
9/10/2025 11:21	389.31	Well 08	9/10/2025	11:21	17.96	Pump test start at 11:15 at 1.5gpm
9/10/2025 11:22	388.58	Well 08	9/10/2025	11:22	18.69	0
9/10/2025 11:24	387.35	Well 08	9/10/2025	11:24	19.92	0
9/10/2025 11:25	386.63	Well 08	9/10/2025	11:25	20.64	0
9/10/2025 11:26	385.43	Well 08	9/10/2025	11:26	21.84	0
9/10/2025 11:27	384.50	Well 08	9/10/2025	11:27	22.77	0
9/10/2025 11:28	384.19	Well 08	9/10/2025	11:28	23.08	0
9/10/2025 11:29	383.87	Well 08	9/10/2025	11:29	23.40	0
9/10/2025 11:30	383.59	Well 08	9/10/2025	11:30	23.68	0
9/10/2025 11:31	383.34	Well 08	9/10/2025	11:31	23.93	0
9/10/2025 11:32	383.14	Well 08	9/10/2025	11:32	24.13	0
9/10/2025 11:33	382.89	Well 08	9/10/2025	11:33	24.38	0
9/10/2025 11:38	382.03	Well 08	9/10/2025	11:38	25.24	0
9/10/2025 11:40	381.74	Well 08	9/10/2025	11:40	25.53	0
9/10/2025 11:45	381.17	Well 08	9/10/2025	11:45	26.10	0
9/10/2025 11:50	380.80	Well 08	9/10/2025	11:50	26.47	0
9/10/2025 11:55	380.21	Well 08	9/10/2025	11:55	27.06	0
9/10/2025 12:00	378.52	Well 08	9/10/2025	12:00	28.75	Pump stopped around 12:03
9/10/2025 12:35	382.47	Well 08	9/10/2025	12:35	24.80	Pump test start at 12:35 at 1gpm
9/10/2025 12:36	382.46	Well 08	9/10/2025	12:36	24.81	0
9/10/2025 12:37	382.40	Well 08	9/10/2025	12:37	24.87	0
9/10/2025 12:38	382.35	Well 08	9/10/2025	12:38	24.92	0
9/10/2025 12:39	382.27	Well 08	9/10/2025	12:39	25.00	0
9/10/2025 12:40	382.22	Well 08	9/10/2025	12:40	25.05	0
9/10/2025 12:45	381.49	Well 08	9/10/2025	12:45	25.78	0
9/10/2025 12:50	380.87	Well 08	9/10/2025	12:50	26.40	0
9/10/2025 12:55	379.80	Well 08	9/10/2025	12:55	27.47	0
9/10/2025 13:00	379.03	Well 08	9/10/2025	13:00	28.24	0
9/10/2025 13:05	378.54	Well 08	9/10/2025	13:05	28.73	0
9/10/2025 13:10	377.74	Well 08	9/10/2025	13:10	29.53	0
9/10/2025 13:15	377.57	Well 08	9/10/2025	13:15	29.70	Pump stopped shortly after
9/18/2025 17:01	396.55	Well 08	9/18/2025	17:01	10.72	0

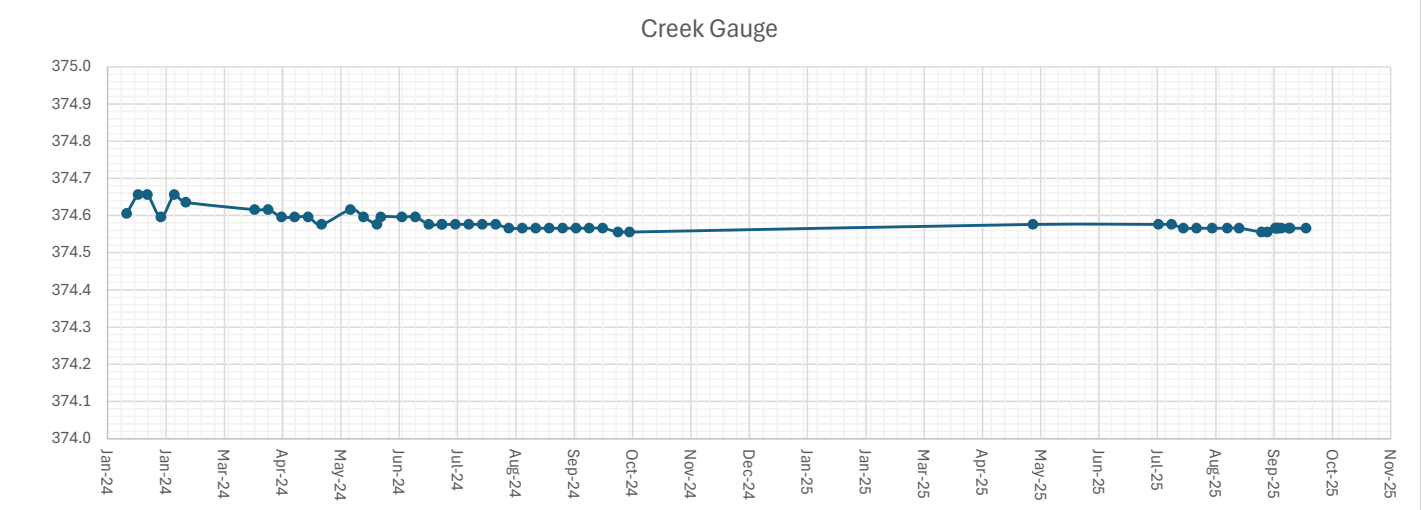

410
405
400
395
390
385
380
375
370
Elevation (NAVD 88 ft)
6/30
7/7
7/14
7/21
7/28
8/4
8/11
8/18
8/25
9/1
9/8
9/15
9/22
Well 08
Ground Surface Elevation
Well Bottom

	Ground Elevation	Well Total Depth	Casing Height
N. Caisson	400.64	29.00	3.04

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/3/2025 13:40	398.16	N. Caisson	7/3/2025	13:40	5.52	Programed at 13:50 - 1hr interval, installed at 14.57'
7/10/2025 11:35	398.11	N. Caisson	7/10/2025	11:35	5.57	TOC to ground is 2.92
7/16/2025 13:07	398.08	N. Caisson	7/16/2025	13:07	5.60	0
7/23/2025 12:40	398.07	N. Caisson	7/23/2025	12:40	5.61	0
7/31/2025 17:44	397.96	N. Caisson	7/31/2025	17:44	5.72	0
8/8/2025 14:47	397.88	N. Caisson	8/8/2025	14:47	5.80	0
8/14/2025 18:25	397.80	N. Caisson	8/14/2025	18:25	5.88	0
8/22/2025 18:09	397.82	N. Caisson	8/22/2025	18:09	5.86	0
8/26/2025 11:32	397.78	N. Caisson	8/26/2025	11:32	5.90	0
8/29/2025 13:51	397.68	N. Caisson	8/29/2025	13:51	6.00	0
9/2/2025 17:55	397.70	N. Caisson	9/2/2025	17:55	5.98	Weeks Drilling redeveloped Well 1 today
9/3/2025 8:47	397.75	N. Caisson	9/3/2025	8:47	5.93	0
9/3/2025 12:30	397.77	N. Caisson	9/3/2025	12:30	5.91	0
9/4/2025 11:33	397.49	N. Caisson	9/4/2025	11:33	6.19	0
9/5/2025 11:56	397.44	N. Caisson	9/5/2025	11:56	6.24	0
9/9/2025 17:33	397.76	N. Caisson	9/9/2025	17:33	5.92	Rain yesterday
9/10/2025 8:32	397.80	N. Caisson	9/10/2025	8:32	5.88	0
9/18/2025 17:05	397.78	N. Caisson	9/18/2025	17:05	5.90	0

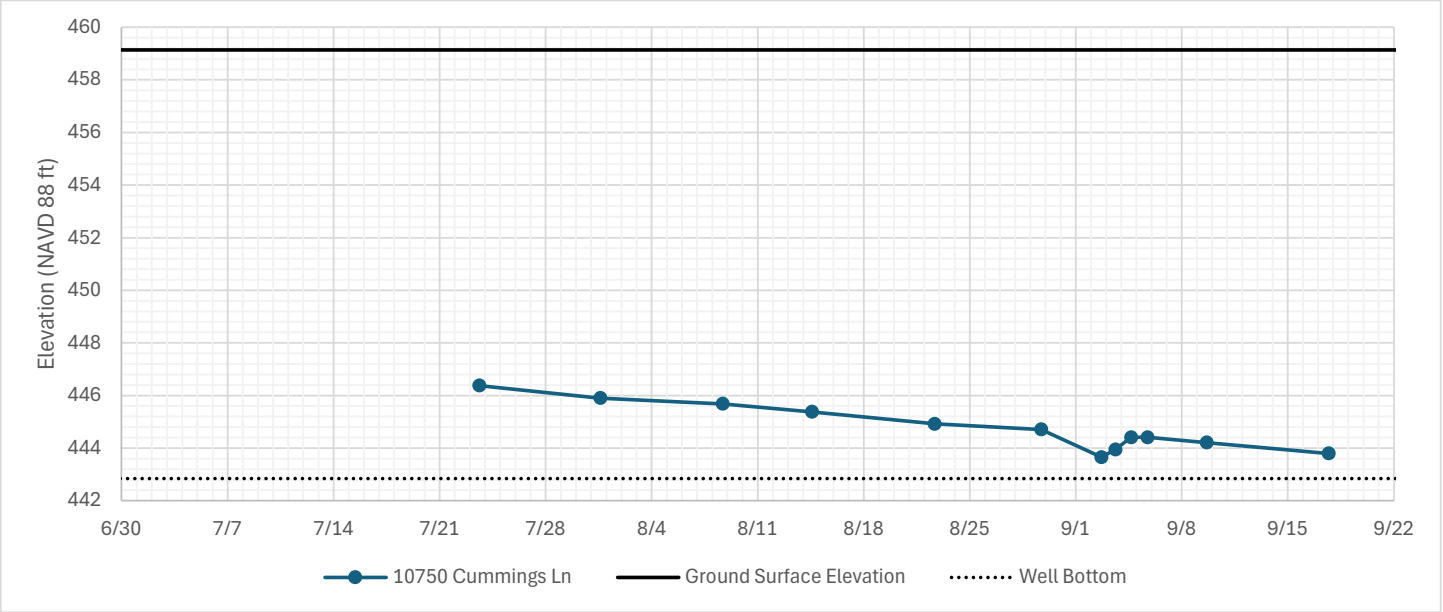


Creek Gauge		Ground Elevation	Well Total Depth	Casing Height			
		374.36					
Date-Time	Stage	Well ID	Date	Time		Depth of Water (ft)	Comments
1/11/2024 0:00	374.61	Creek Gauge	1/11/2024		0:00	0.25	Raining
1/17/2024 0:00	374.66	Creek Gauge	1/17/2024		0:00	0.30	Raining
1/22/2024 0:00	374.66	Creek Gauge	1/22/2024		0:00	0.30	0
1/29/2024 0:00	374.60	Creek Gauge	1/29/2024		0:00	0.24	0
2/5/2024 0:00	374.66	Creek Gauge	2/5/2024		0:00	0.30	0
2/11/2024 0:00	374.64	Creek Gauge	2/11/2024		0:00	0.28	0
3/18/2024 0:00	374.62	Creek Gauge	3/18/2024		0:00	0.26	0
3/25/2024 0:00	374.62	Creek Gauge	3/25/2024		0:00	0.26	0
4/1/2024 0:00	374.60	Creek Gauge	4/1/2024		0:00	0.24	0
4/8/2024 0:00	374.60	Creek Gauge	4/8/2024		0:00	0.24	0
4/15/2024 0:00	374.60	Creek Gauge	4/15/2024		0:00	0.24	0
4/22/2024 0:00	374.58	Creek Gauge	4/22/2024		0:00	0.22	0
5/7/2024 0:00	374.62	Creek Gauge	5/7/2024		0:00	0.26	0
5/14/2024 0:00	374.60	Creek Gauge	5/14/2024		0:00	0.24	0
5/21/2024 0:00	374.58	Creek Gauge	5/21/2024		0:00	0.22	0
5/23/2024 0:00	374.60	Creek Gauge	5/23/2024		0:00	0.24	0
6/3/2024 0:00	374.60	Creek Gauge	6/3/2024		0:00	0.24	0
6/10/2024 0:00	374.60	Creek Gauge	6/10/2024		0:00	0.24	0
6/17/2024 0:00	374.58	Creek Gauge	6/17/2024		0:00	0.22	0
6/24/2024 0:00	374.58	Creek Gauge	6/24/2024		0:00	0.22	0
6/24/2024 0:00	374.58	Creek Gauge	6/24/2024		0:00	0.22	0
7/1/2024 0:00	374.58	Creek Gauge	7/1/2024		0:00	0.22	0
7/8/2024 0:00	374.58	Creek Gauge	7/8/2024		0:00	0.22	0
7/15/2024 0:00	374.58	Creek Gauge	7/15/2024		0:00	0.22	0
7/22/2024 0:00	374.58	Creek Gauge	7/22/2024		0:00	0.22	0
7/29/2024 0:00	374.57	Creek Gauge	7/29/2024		0:00	0.21	0
8/5/2024 0:00	374.57	Creek Gauge	8/5/2024		0:00	0.21	0
8/12/2024 0:00	374.57	Creek Gauge	8/12/2024		0:00	0.21	0
8/19/2024 0:00	374.57	Creek Gauge	8/19/2024		0:00	0.21	0
8/26/2024 0:00	374.57	Creek Gauge	8/26/2024		0:00	0.21	0
9/2/2024 0:00	374.57	Creek Gauge	9/2/2024		0:00	0.21	0
9/9/2024 0:00	374.57	Creek Gauge	9/9/2024		0:00	0.21	0
9/16/2024 0:00	374.57	Creek Gauge	9/16/2024		0:00	0.21	0
9/24/2024 0:00	374.56	Creek Gauge	9/24/2024		0:00	0.20	0
9/30/2024 0:00	374.56	Creek Gauge	9/30/2024		0:00	0.20	0
4/29/2025 0:00	374.58	Creek Gauge	4/29/2025		0:00	0.22	0
7/3/2025 15:20	374.58	Creek Gauge	7/3/2025		15:20	0.22	Gauge at West Boundary in Creek
7/10/2025 11:05	374.58	Creek Gauge	7/10/2025		11:05	0.22	0
7/16/2025 13:30	374.57	Creek Gauge	7/16/2025		13:30	0.21	0
7/23/2025 12:50	374.57	Creek Gauge	7/23/2025		12:50	0.21	0
7/31/2025 17:52	374.57	Creek Gauge	7/31/2025		17:52	0.21	0
8/8/2025 15:03	374.57	Creek Gauge	8/8/2025		15:03	0.21	0
8/14/2025 18:30	374.57	Creek Gauge	8/14/2025		18:30	0.21	0
8/26/2025 11:41	374.56	Creek Gauge	8/26/2025		11:41	0.20	0
8/29/2025 13:56	374.56	Creek Gauge	8/29/2025		13:56	0.20	0
9/2/2025 18:00	374.57	Creek Gauge	9/2/2025		18:00	0.21	Difficult to read
9/3/2025 9:43	374.57	Creek Gauge	9/3/2025		9:43	0.21	Difficult to read
9/3/2025 12:42	374.57	Creek Gauge	9/3/2025		12:42	0.21	Difficult to read, seems unchanged from yesterday
9/4/2025 12:53	374.57	Creek Gauge	9/4/2025		12:53	0.21	Difficult to read
9/5/2025 18:50	374.57	Creek Gauge	9/5/2025		18:50	0.21	0
9/9/2025 19:30	374.57	Creek Gauge	9/9/2025		19:30	0.21	Rain yesterday
9/10/2025 10:12	374.57	Creek Gauge	9/10/2025		10:12	0.21	0
9/18/2025 17:17	374.57	Creek Gauge	9/18/2025		17:17	0.21	0



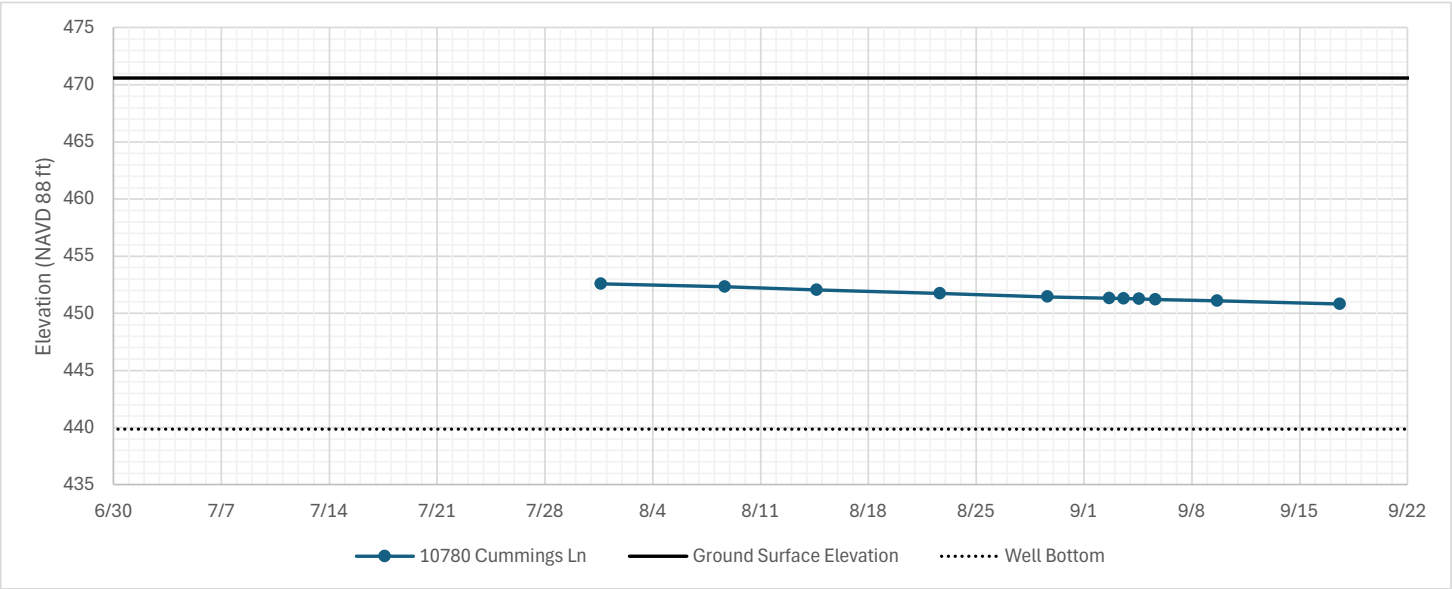
	Ground Elevation	Well Total Depth	Casing Height
10750 Cummings Ln	459.14	18.00	1.71

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/23/2025 15:15	446.37	10750 Cummings Ln	7/23/2025	15:15	14.48	0
7/31/2025 14:57	445.90	10750 Cummings Ln	7/31/2025	14:57	14.95	0
8/8/2025 16:53	445.68	10750 Cummings Ln	8/8/2025	16:53	15.17	0
8/14/2025 14:28	445.38	10750 Cummings Ln	8/14/2025	14:28	15.47	0
8/22/2025 16:31	444.92	10750 Cummings Ln	8/22/2025	16:31	15.93	0
8/29/2025 17:17	444.71	10750 Cummings Ln	8/29/2025	17:17	16.14	0
9/2/2025 16:47	443.66	10750 Cummings Ln	9/2/2025	16:47	17.19	0
9/3/2025 15:05	443.95	10750 Cummings Ln	9/3/2025	15:05	16.90	0
9/4/2025 15:52	444.41	10750 Cummings Ln	9/4/2025	15:52	16.44	0
9/5/2025 17:43	444.41	10750 Cummings Ln	9/5/2025	17:43	16.44	Measured twice
9/9/2025 15:58	444.21	10750 Cummings Ln	9/9/2025	15:58	16.64	0
9/17/2025 17:11	443.80	10750 Cummings Ln	9/17/2025	17:11	17.05	0



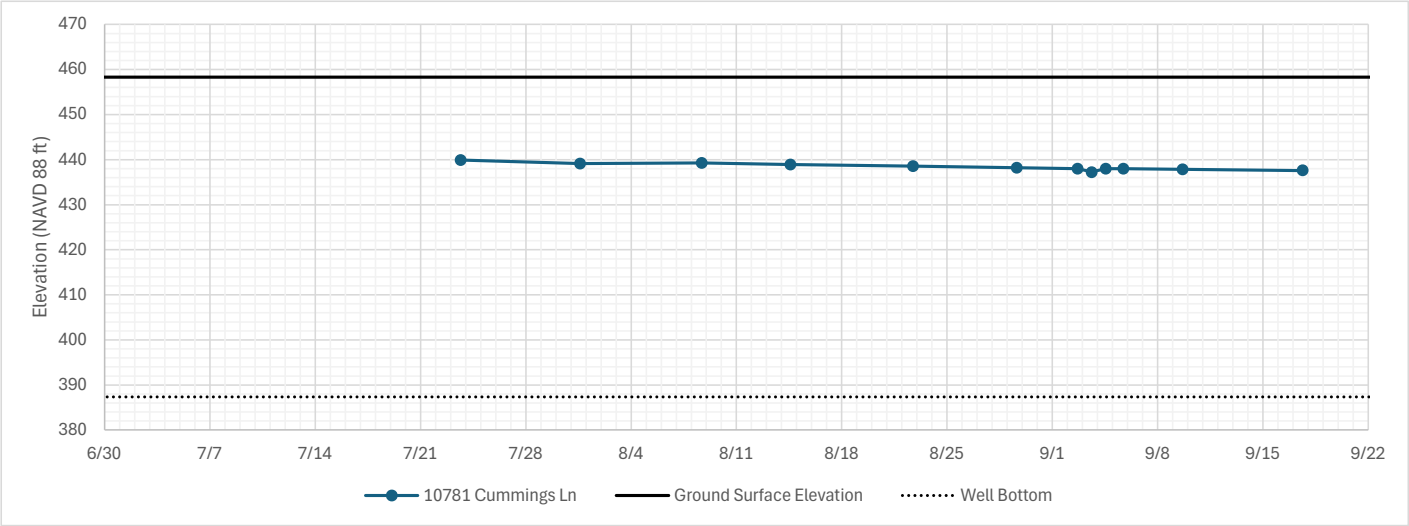
		Ground Elevation	Well Total Depth	Casing Height		
10780 Cummings Ln		470.59	32.00	1.25		

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/31/2025 15:24	452.57	10780 Cummings Ln	7/31/2025	15:24	19.27	Measured to top of concrete well deck, slide top open
8/8/2025 16:29	452.32	10780 Cummings Ln	8/8/2025	16:29	19.52	Measured to top of concrete well deck, slide top open
8/14/2025 15:40	452.04	10780 Cummings Ln	8/14/2025	15:40	19.80	0
8/22/2025 15:46	451.74	10780 Cummings Ln	8/22/2025	15:46	20.10	0
8/29/2025 15:32	451.44	10780 Cummings Ln	8/29/2025	15:32	20.40	0
9/2/2025 15:48	451.32	10780 Cummings Ln	9/2/2025	15:48	20.52	0
9/3/2025 14:11	451.28	10780 Cummings Ln	9/3/2025	14:11	20.56	0
9/4/2025 13:45	451.25	10780 Cummings Ln	9/4/2025	13:45	20.59	0
9/5/2025 15:39	451.20	10780 Cummings Ln	9/5/2025	15:39	20.64	0
9/9/2025 15:31	451.09	10780 Cummings Ln	9/9/2025	15:31	20.75	0
9/17/2025 14:54	450.81	10780 Cummings Ln	9/17/2025	14:54	21.03	32 feet deep from TOC



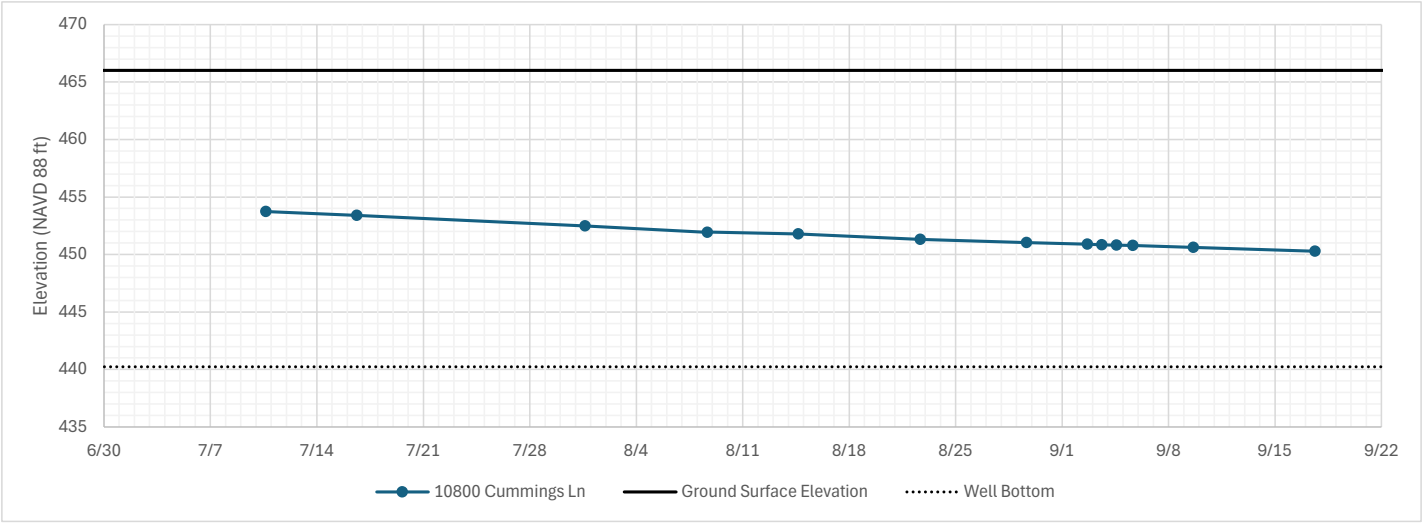
	Ground Elevation	Well Total Depth	Casing Height
10781 Cummings Ln	458.28	72.00	1.04

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/23/2025 16:00	439.88	10781 Cummings Ln	7/23/2025	16:00	19.44	0
7/31/2025 14:36	439.07	10781 Cummings Ln	7/31/2025	14:36	20.25	0
8/8/2025 16:43	439.21	10781 Cummings Ln	8/8/2025	16:43	20.11	0
8/14/2025 14:14	438.90	10781 Cummings Ln	8/14/2025	14:14	20.42	0
8/22/2025 17:39	438.53	10781 Cummings Ln	8/22/2025	17:39	20.79	0
8/29/2025 15:09	438.20	10781 Cummings Ln	8/29/2025	15:09	21.12	0
9/2/2025 16:31	437.98	10781 Cummings Ln	9/2/2025	16:31	21.34	0
9/3/2025 14:48	437.22	10781 Cummings Ln	9/3/2025	14:48	22.10	Pumping before measurement, well was still recovering, leak at well head
9/4/2025 13:25	437.96	10781 Cummings Ln	9/4/2025	13:25	21.36	0
9/5/2025 17:23	437.96	10781 Cummings Ln	9/5/2025	17:23	21.36	Measured twice
9/9/2025 15:45	437.84	10781 Cummings Ln	9/9/2025	15:45	21.48	0
9/17/2025 15:40	437.59	10781 Cummings Ln	9/17/2025	15:40	21.73	0



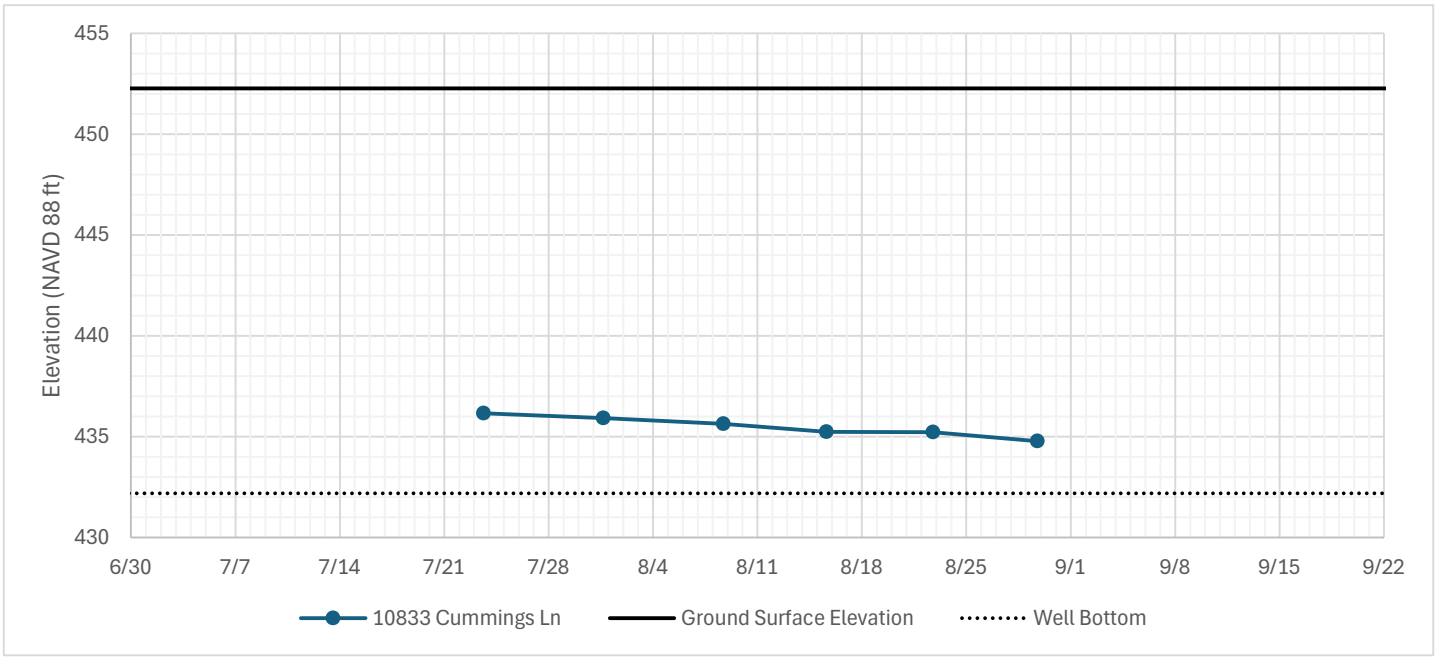
	Ground Elevation	Well Total Depth	Casing Height
10800 Cummings Ln	466.03	27	1.21

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/10/2025 15:15	453.73	10800 Cummings Ln	7/10/2025	15:15	13.51	M30 set at bottom @ 3:30, 5min interval, Total Depth 27', not pumping
7/16/2025 15:05	453.41	10800 Cummings Ln	7/16/2025	15:05	13.83	Not Pumping
7/31/2025 15:10	452.48	10800 Cummings Ln	7/31/2025	15:10	14.76	14.82 - 0.06, measured to upper wood trim which is 0.75 inch above well deck
8/8/2025 16:15	451.94	10800 Cummings Ln	8/8/2025	16:15	15.30	Measured to top of well deck
8/14/2025 15:30	451.79	10800 Cummings Ln	8/14/2025	15:30	15.45	Measured to top of well deck
8/22/2025 16:10	451.32	10800 Cummings Ln	8/22/2025	16:10	15.92	0
8/29/2025 16:02	451.04	10800 Cummings Ln	8/29/2025	16:02	16.20	0
9/2/2025 16:13	450.89	10800 Cummings Ln	9/2/2025	16:13	16.35	0
9/3/2025 14:32	450.85	10800 Cummings Ln	9/3/2025	14:32	16.39	0
9/4/2025 14:05	450.82	10800 Cummings Ln	9/4/2025	14:05	16.42	0
9/5/2025 15:58	450.78	10800 Cummings Ln	9/5/2025	15:58	16.46	0
9/9/2025 15:13	450.62	10800 Cummings Ln	9/9/2025	15:13	16.62	0
9/17/2025 15:19	450.29	10800 Cummings Ln	9/17/2025	15:19	16.95	0



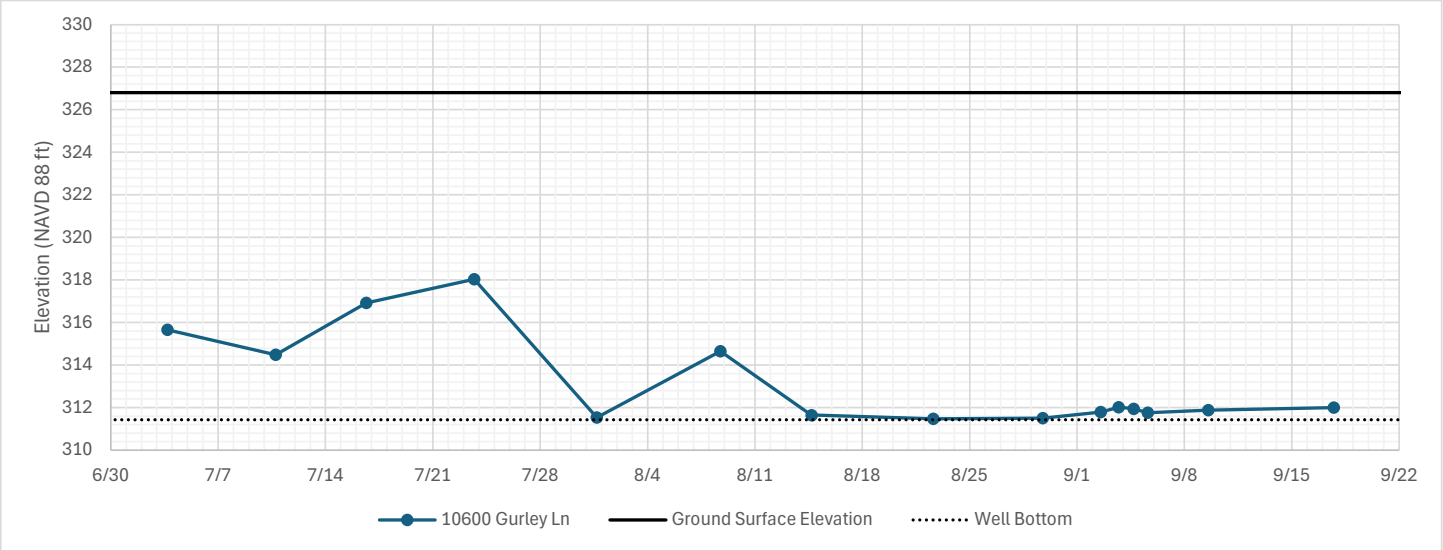
	Ground Elevation	Well Total Depth	Casing Height
10833 Cummings Ln	452.28	21.00	0.92

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/23/2025 15:35	436.16	10833 Cummings Ln	7/23/2025	15:35	17.03	0
7/31/2025 16:03	435.92	10833 Cummings Ln	7/31/2025	16:03	17.27	0
8/8/2025 17:13	435.63	10833 Cummings Ln	8/8/2025	17:13	17.56	0
8/15/2025 15:00	435.23	10833 Cummings Ln	8/15/2025	15:00	17.96	0
8/22/2025 17:51	435.22	10833 Cummings Ln	8/22/2025	17:51	17.97	0
8/29/2025 17:48	434.78	10833 Cummings Ln	8/29/2025	17:48	18.41	0



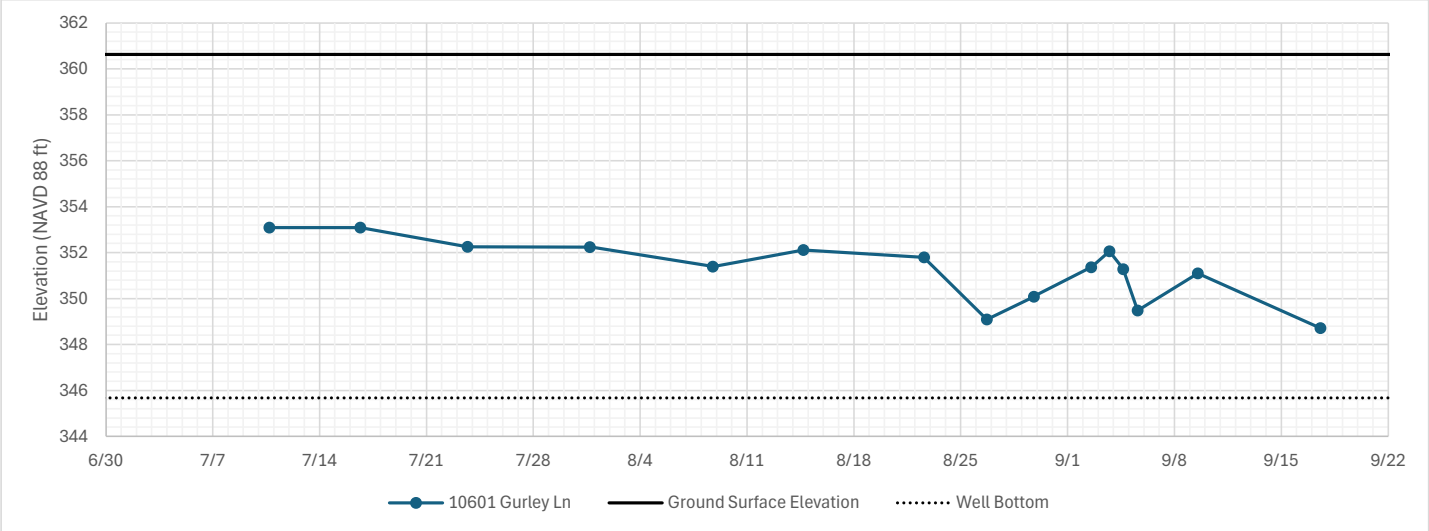
	Ground Elevation	Well Total Depth	Casing Height
10600 Gurley Ln	326.80	18	2.83

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/3/2025 16:20	315.66	10600 Gurley Ln	7/3/2025	16:20	13.98	Total Depth 18', Transducer set at 18'
7/10/2025 17:45	314.49	10600 Gurley Ln	7/10/2025	17:45	15.15	4' Caisson
7/16/2025 15:55	316.92	10600 Gurley Ln	7/16/2025	15:55	12.72	Not Pumping
7/23/2025 16:34	318.04	10600 Gurley Ln	7/23/2025	16:34	11.60	0
7/31/2025 16:37	311.54	10600 Gurley Ln	7/31/2025	16:37	18.10	0
8/8/2025 17:48	314.66	10600 Gurley Ln	8/8/2025	17:48	14.98	0
8/14/2025 16:28	311.65	10600 Gurley Ln	8/14/2025	16:28	17.99	0
8/22/2025 14:45	311.48	10600 Gurley Ln	8/22/2025	14:45	18.16	Pumping
8/29/2025 18:16	311.51	10600 Gurley Ln	8/29/2025	18:16	18.13	0
9/2/2025 13:02	311.79	10600 Gurley Ln	9/2/2025	13:02	17.85	Pumping after measurement
9/3/2025 17:00	312.02	10600 Gurley Ln	9/3/2025	17:00	17.62	0
9/4/2025 16:25	311.95	10600 Gurley Ln	9/4/2025	16:25	17.69	0
9/5/2025 14:27	311.76	10600 Gurley Ln	9/5/2025	14:27	17.88	Pumping after measurement
9/9/2025 13:13	311.88	10600 Gurley Ln	9/9/2025	13:13	17.76	0
9/17/2025 17:44	312.01	10600 Gurley Ln	9/17/2025	17:44	17.63	0



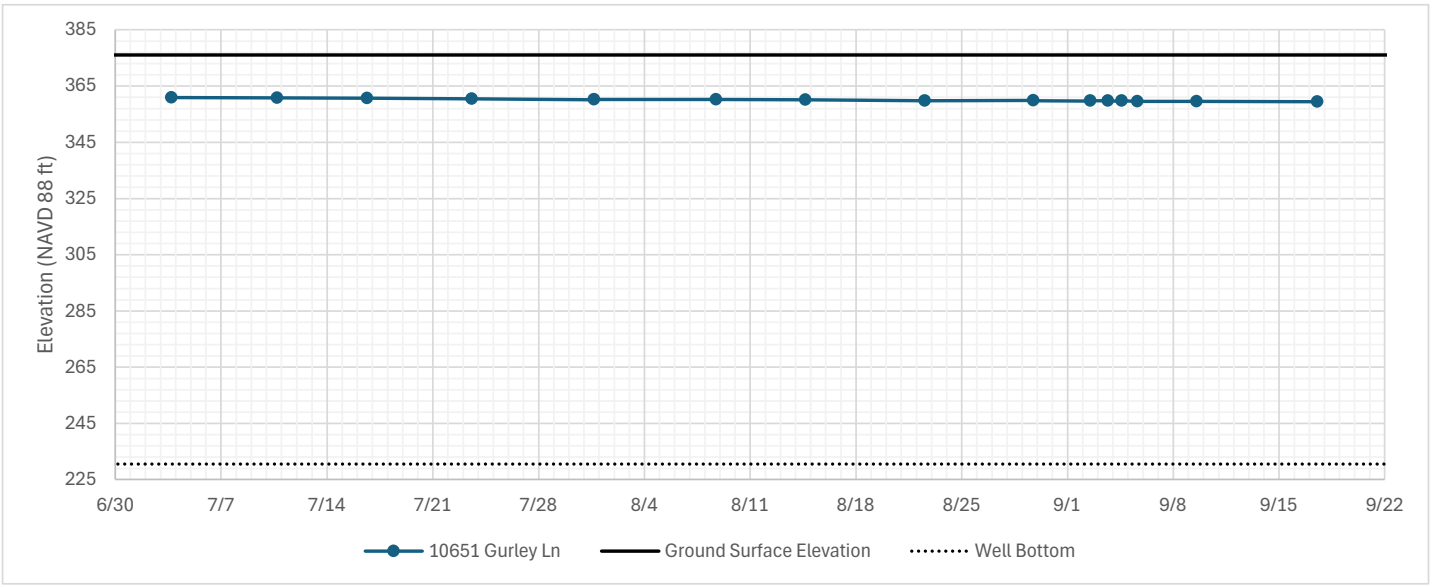
	Ground Elevation	Well Total Depth	Casing Height
10601 Gurley Ln	360.63	15.83	0.88

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/10/2025 16:45	353.10	10601 Gurley Ln	7/10/2025	16:45	8.41	15.5' Total Depth, 4' Caisson
7/16/2025 15:45	353.10	10601 Gurley Ln	7/16/2025	15:45	8.41	Not Pumping
7/23/2025 16:40	352.26	10601 Gurley Ln	7/23/2025	16:40	9.25	0
7/31/2025 16:42	352.25	10601 Gurley Ln	7/31/2025	16:42	9.26	0
8/8/2025 17:56	351.40	10601 Gurley Ln	8/8/2025	17:56	10.11	0
8/14/2025 16:22	352.12	10601 Gurley Ln	8/14/2025	16:22	9.39	0
8/22/2025 14:00	351.80	10601 Gurley Ln	8/22/2025	14:00	9.71	0
8/26/2025 16:50	349.09	10601 Gurley Ln	8/26/2025	16:50	12.42	Pumping before measurement
8/29/2025 18:46	350.09	10601 Gurley Ln	8/29/2025	18:46	11.42	Leak in pump house above well head
9/2/2025 12:46	351.37	10601 Gurley Ln	9/2/2025	12:46	10.14	Superior Pump working on well, well off for several hours
9/3/2025 17:35	352.06	10601 Gurley Ln	9/3/2025	17:35	9.45	0
9/4/2025 15:20	351.29	10601 Gurley Ln	9/4/2025	15:20	10.22	Pumping after measurement
9/5/2025 13:48	349.48	10601 Gurley Ln	9/5/2025	13:48	12.03	0
9/9/2025 12:40	351.10	10601 Gurley Ln	9/9/2025	12:40	10.41	0
9/17/2025 13:34	348.72	10601 Gurley Ln	9/17/2025	13:34	12.79	0

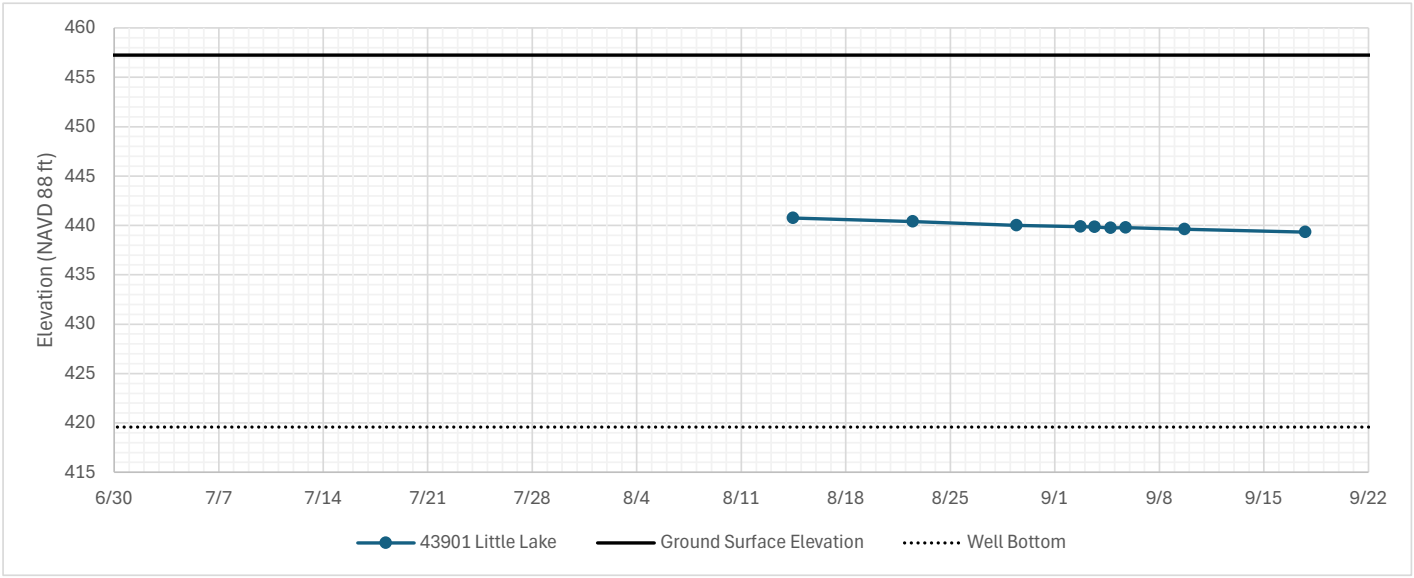


	Ground Elevation	Well Total Depth	Casing Height
10651 Gurley Ln	376.30	147.00	1.54

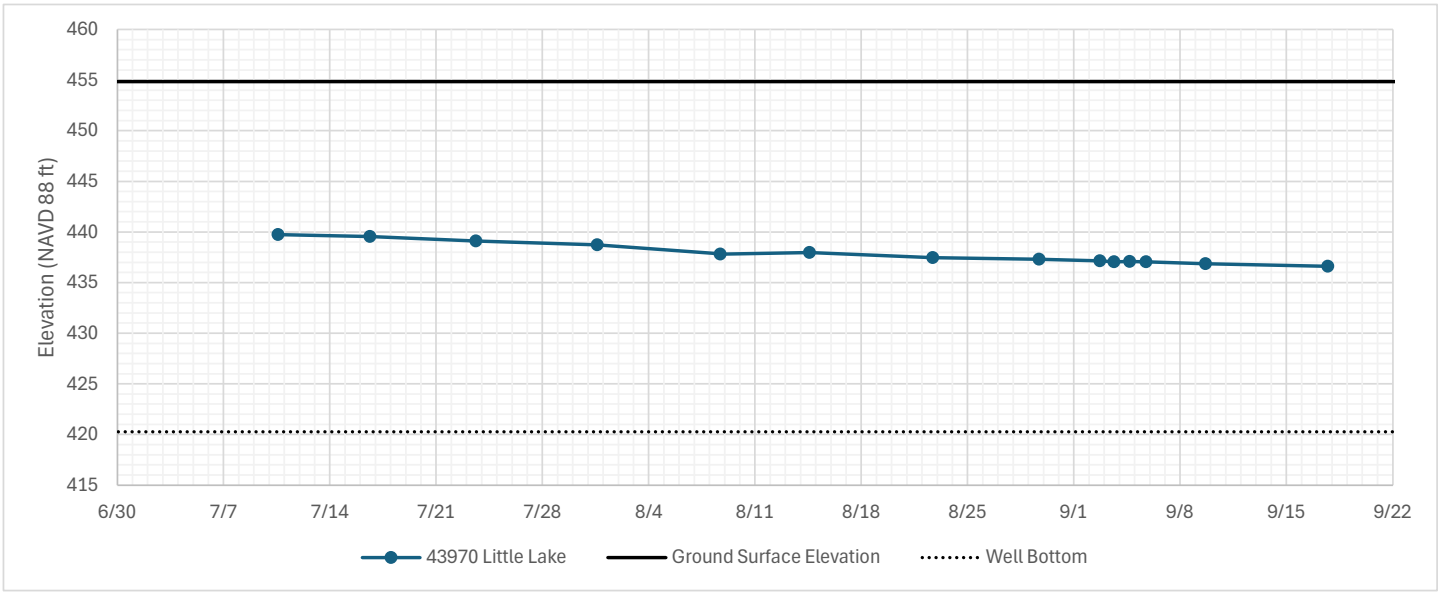
Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/3/2025 17:25	360.87	10651 Gurley Ln	7/3/2025	17:25	16.97	Transducer set at 37' TOC
7/10/2025 17:00	360.81	10651 Gurley Ln	7/10/2025	17:00	17.03	5" BR Well
7/16/2025 16:10	360.62	10651 Gurley Ln	7/16/2025	16:10	17.22	Not Pumping
7/23/2025 14:25	360.44	10651 Gurley Ln	7/23/2025	14:25	17.40	0
7/31/2025 16:27	360.19	10651 Gurley Ln	7/31/2025	16:27	17.65	0
8/8/2025 18:03	360.21	10651 Gurley Ln	8/8/2025	18:03	17.63	0
8/14/2025 16:13	360.10	10651 Gurley Ln	8/14/2025	16:13	17.74	0
8/22/2025 13:45	359.79	10651 Gurley Ln	8/22/2025	13:45	18.05	0
8/29/2025 17:59	359.80	10651 Gurley Ln	8/29/2025	17:59	18.04	0
9/2/2025 12:18	359.71	10651 Gurley Ln	9/2/2025	12:18	18.13	0
9/3/2025 16:13	359.70	10651 Gurley Ln	9/3/2025	16:13	18.14	0
9/4/2025 14:17	359.69	10651 Gurley Ln	9/4/2025	14:17	18.15	0
9/5/2025 15:04	359.54	10651 Gurley Ln	9/5/2025	15:04	18.30	0
9/9/2025 13:24	359.46	10651 Gurley Ln	9/9/2025	13:24	18.38	0
9/17/2025 12:56	359.44	10651 Gurley Ln	9/17/2025	12:56	18.40	147 feet deep from TOC



		Ground Elevation	Well Total Depth	Casing Height		
43901 Little Lake		457.24	38	0.33		
Date-Time	**GWE**	**Well ID**	**Date**	**Time**	**Depth to Water (ft bgs)**	**Comments**
						38 feet deep, measured to inner
8/14/2025 11:35	440.76	43901 Little Lake	8/14/2025	11:35	16.82	PVC sleeve below well cover
8/22/2025 11:35	440.40	43901 Little Lake	8/22/2025	11:35	17.18	0
8/29/2025 10:41	440.01	43901 Little Lake	8/29/2025	10:41	17.57	Pumping after measurement
9/2/2025 17:35	439.87	43901 Little Lake	9/2/2025	17:35	17.71	0
9/3/2025 15:56	439.84	43901 Little Lake	9/3/2025	15:56	17.74	0
9/4/2025 17:45	439.76	43901 Little Lake	9/4/2025	17:45	17.82	0
9/5/2025 18:17	439.77	43901 Little Lake	9/5/2025	18:17	17.81	0
9/9/2025 16:41	439.61	43901 Little Lake	9/9/2025	16:41	17.97	0
9/17/2025 18:33	439.34	43901 Little Lake	9/17/2025	18:33	18.24	0

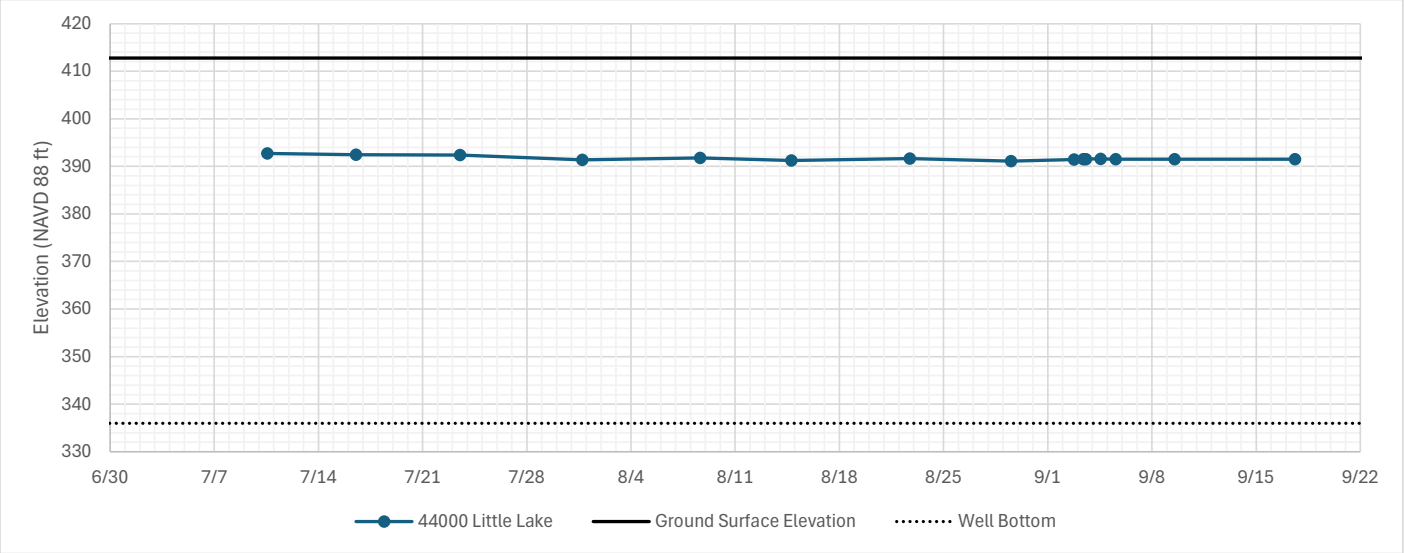


		Ground Elevation	Well Total Depth	Casing Height		
43970 Little Lake		454.85	35.00	0.42		
Date-Time	**GWE**	**Well ID**	**Date**	**Time**	**Depth to Water (ft bgs)**	**Comments**
7/10/2025 14:20	439.75	43970 Little Lake	7/10/2025	14:20	15.52	Richard Jung 35' Total Depth, 4' Caisson wasn't pumping
7/16/2025 15:25	439.57	43970 Little Lake	7/16/2025	15:25	15.70	Not Pumping
7/23/2025 15:05	439.10	43970 Little Lake	7/23/2025	15:05	16.17	0
7/31/2025 14:25	438.72	43970 Little Lake	7/31/2025	14:25	16.55	0
8/8/2025 17:00	437.83	43970 Little Lake	8/8/2025	17:00	17.44	0
8/14/2025 14:09	437.98	43970 Little Lake	8/14/2025	14:09	17.29	0
8/22/2025 16:46	437.46	43970 Little Lake	8/22/2025	16:46	17.81	0
8/29/2025 17:05	437.31	43970 Little Lake	8/29/2025	17:05	17.96	0
9/2/2025 17:06	437.15	43970 Little Lake	9/2/2025	17:06	18.12	0
9/3/2025 15:20	437.05	43970 Little Lake	9/3/2025	15:20	18.22	0
9/4/2025 16:09	437.08	43970 Little Lake	9/4/2025	16:09	18.19	0
9/5/2025 18:03	437.05	43970 Little Lake	9/5/2025	18:03	18.22	0
9/9/2025 16:11	436.87	43970 Little Lake	9/9/2025	16:11	18.40	0
9/17/2025 17:25	436.62	43970 Little Lake	9/17/2025	17:25	18.65	0



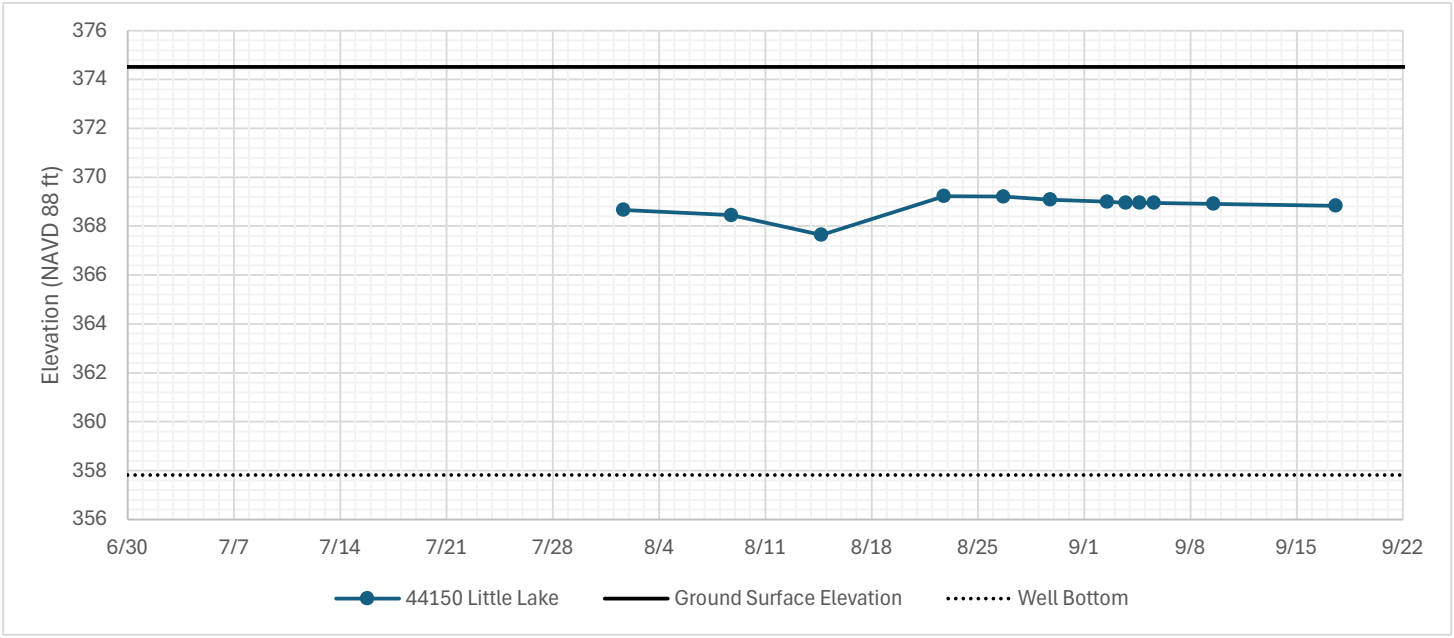
	Ground Elevation	Well Total Depth	Casing Height
44000 Little Lake	412.80	78.00	1.17

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/10/2025 13:30	392.70	44000 Little Lake	7/10/2025	13:30	21.27	Static ~10min Recharge - drawdown to 28.97 with pump on
7/16/2025 12:22	392.47	44000 Little Lake	7/16/2025	12:22	21.50	Not Pumping
7/23/2025 12:12	392.39	44000 Little Lake	7/23/2025	12:12	21.58	Not Pumping, 10022 Mooney Lane
7/31/2025 17:17	391.37	44000 Little Lake	7/31/2025	17:17	22.60	0
8/8/2025 15:14	391.77	44000 Little Lake	8/8/2025	15:14	22.20	0
8/14/2025 18:17	391.26	44000 Little Lake	8/14/2025	18:17	22.71	Weeks Drilling performed pump test around 10:30AM at Well 06
8/22/2025 17:21	391.63	44000 Little Lake	8/22/2025	17:21	22.34	0
8/29/2025 12:30	391.14	44000 Little Lake	8/29/2025	12:30	22.83	0
9/2/2025 18:33	391.44	44000 Little Lake	9/2/2025	18:33	22.53	Weeks Drilling redeveloped Well 1 today
9/3/2025 9:30	391.49	44000 Little Lake	9/3/2025	9:30	22.48	0
9/3/2025 13:19	391.53	44000 Little Lake	9/3/2025	13:19	22.44	0
9/4/2025 13:05	391.56	44000 Little Lake	9/4/2025	13:05	22.41	0
9/5/2025 13:13	391.53	44000 Little Lake	9/5/2025	13:13	22.44	0
9/9/2025 12:22	391.49	44000 Little Lake	9/9/2025	12:22	22.48	0
9/17/2025 14:21	391.53	44000 Little Lake	9/17/2025	14:21	22.44	78 feet deep from TOC



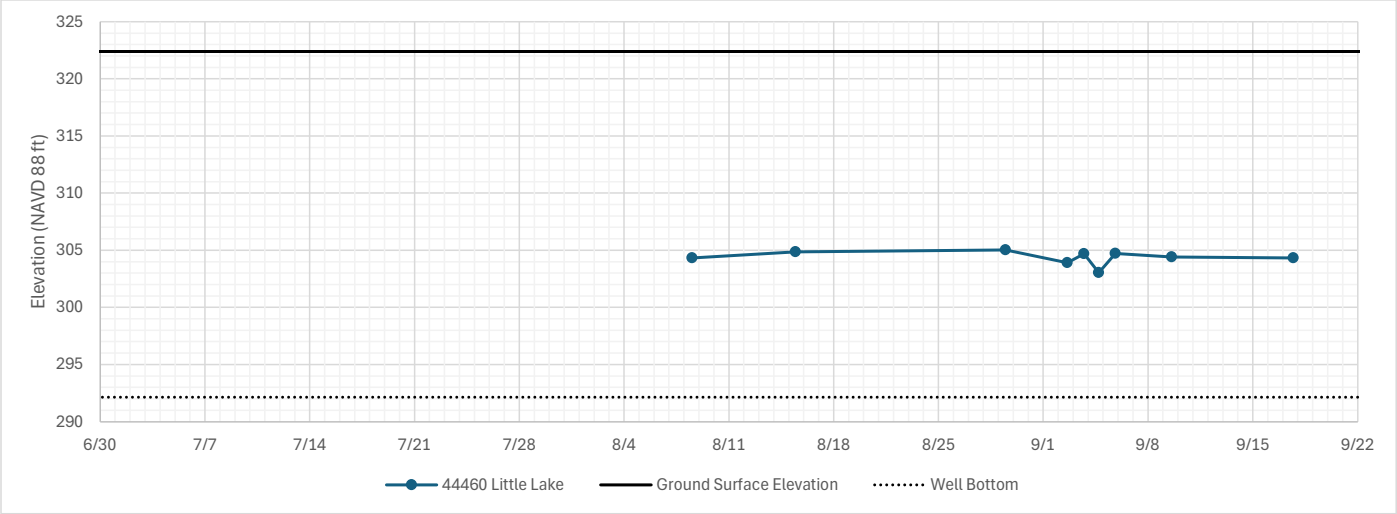
	Ground Elevation	Well Total Depth	Casing Height
44150 Little Lake	374.51	18.33	1.63

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
8/1/2025 15:57	368.66	44150 Little Lake	8/1/2025	15:57	7.48	0
8/8/2025 18:13	368.45	44150 Little Lake	8/8/2025	18:13	7.69	0
8/14/2025 16:48	367.65	44150 Little Lake	8/14/2025	16:48	8.49	0
8/22/2025 18:26	369.23	44150 Little Lake	8/22/2025	18:26	6.91	0
8/26/2025 16:35	369.21	44150 Little Lake	8/26/2025	16:35	6.93	0
8/29/2025 18:31	369.08	44150 Little Lake	8/29/2025	18:31	7.06	0
9/2/2025 12:32	369.00	44150 Little Lake	9/2/2025	12:32	7.14	0
9/3/2025 17:48	368.96	44150 Little Lake	9/3/2025	17:48	7.18	0
9/4/2025 15:34	368.96	44150 Little Lake	9/4/2025	15:34	7.18	Measured twice
9/5/2025 14:04	368.96	44150 Little Lake	9/5/2025	14:04	7.18	0
9/9/2025 12:54	368.91	44150 Little Lake	9/9/2025	12:54	7.23	0
9/17/2025 13:51	368.84	44150 Little Lake	9/17/2025	13:51	7.30	0



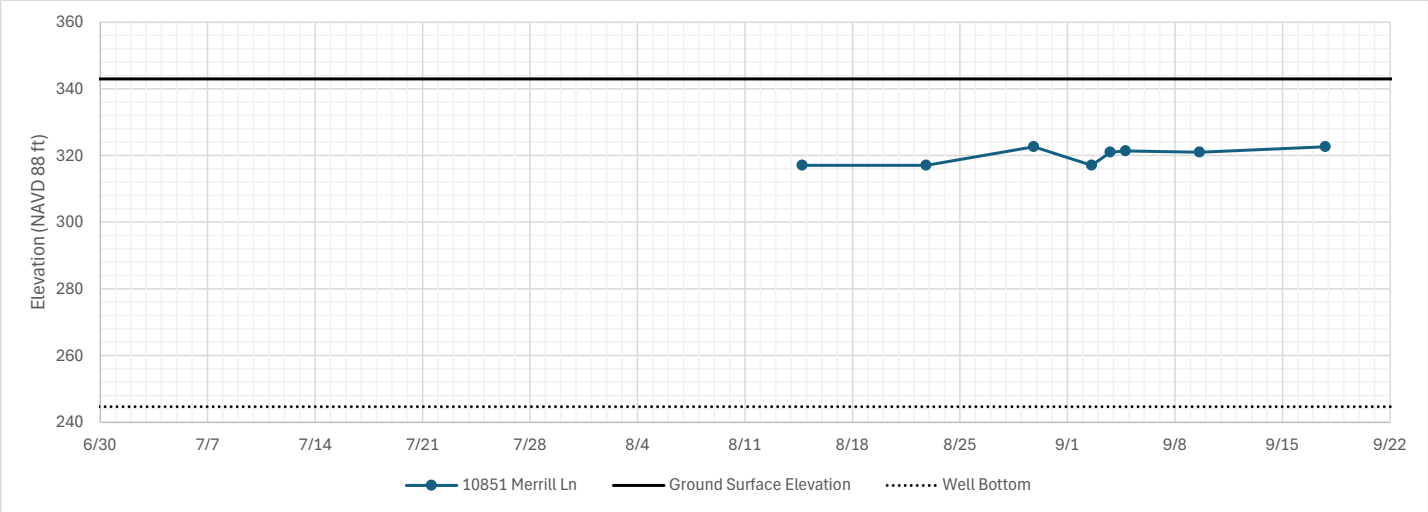
	Ground Elevation	Well Total Depth	Casing Height
44460 Little Lake	322.41	32.00	1.75

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
8/8/2025 13:00	304.33	44460 Little Lake	8/8/2025	13:00	19.83	Measured to bottom of board across well, probe was within concrete pipe at well bottom, pump cycled on and off
8/15/2025 10:43	304.88	44460 Little Lake	8/15/2025	10:43	19.28	Measured to bottom of board across well, probe was within concrete pipe at well bottom
8/29/2025 11:32	305.04	44460 Little Lake	8/29/2025	11:32	19.12	Pumping after measurement
9/2/2025 14:45	303.92	44460 Little Lake	9/2/2025	14:45	20.24	0
9/3/2025 17:22	304.70	44460 Little Lake	9/3/2025	17:22	19.46	0
9/4/2025 17:05	303.04	44460 Little Lake	9/4/2025	17:05	21.12	Pump in well is still on per Mary, no pumping during measurement
9/5/2025 19:25	304.74	44460 Little Lake	9/5/2025	19:25	19.42	0
9/9/2025 13:57	304.42	44460 Little Lake	9/9/2025	13:57	19.74	0
9/17/2025 16:43	304.33	44460 Little Lake	9/17/2025	16:43	19.83	32 feet deep from TOC



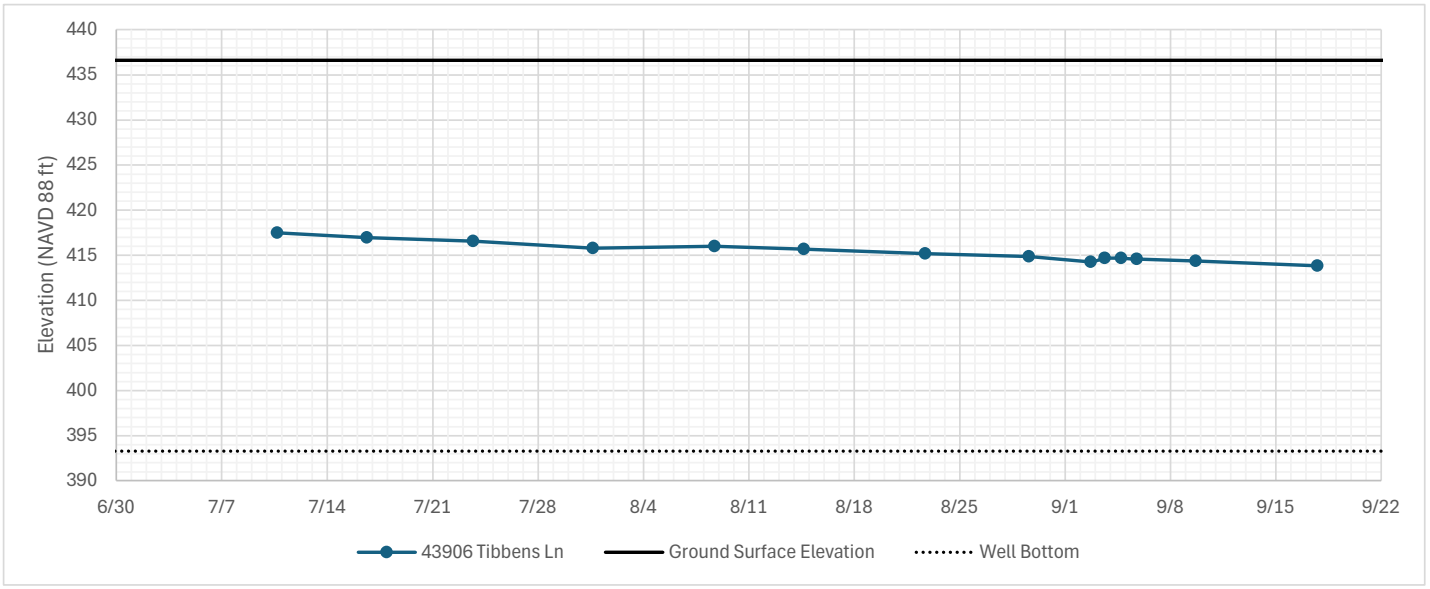
	Ground Elevation	Well Total Depth	Casing Height
10851 Merrill Ln	343.01	100.00	1.67

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
8/14/2025 17:10	317.10	10851 Merrill Ln	8/14/2025	17:10	27.58	Iron bacteria present, Not in tab due to bact in well (only one measurement). - Will try again.
8/22/2025 18:51	317.05	10851 Merrill Ln	8/22/2025	18:51	27.63	0
8/29/2025 19:05	322.67	10851 Merrill Ln	8/29/2025	19:05	22.01	Measurement taken twice, floor was wet
9/2/2025 13:34	317.06	10851 Merrill Ln	9/2/2025	13:34	27.62	0
9/3/2025 18:41	321.02	10851 Merrill Ln	9/3/2025	18:41	23.66	0
9/4/2025 18:54	321.43	10851 Merrill Ln	9/4/2025	18:54	23.25	0
9/9/2025 14:16	321.00	10851 Merrill Ln	9/9/2025	14:16	23.68	0
9/17/2025 18:51	322.66	10851 Merrill Ln	9/17/2025	18:51	22.02	100 feet deep from TOC



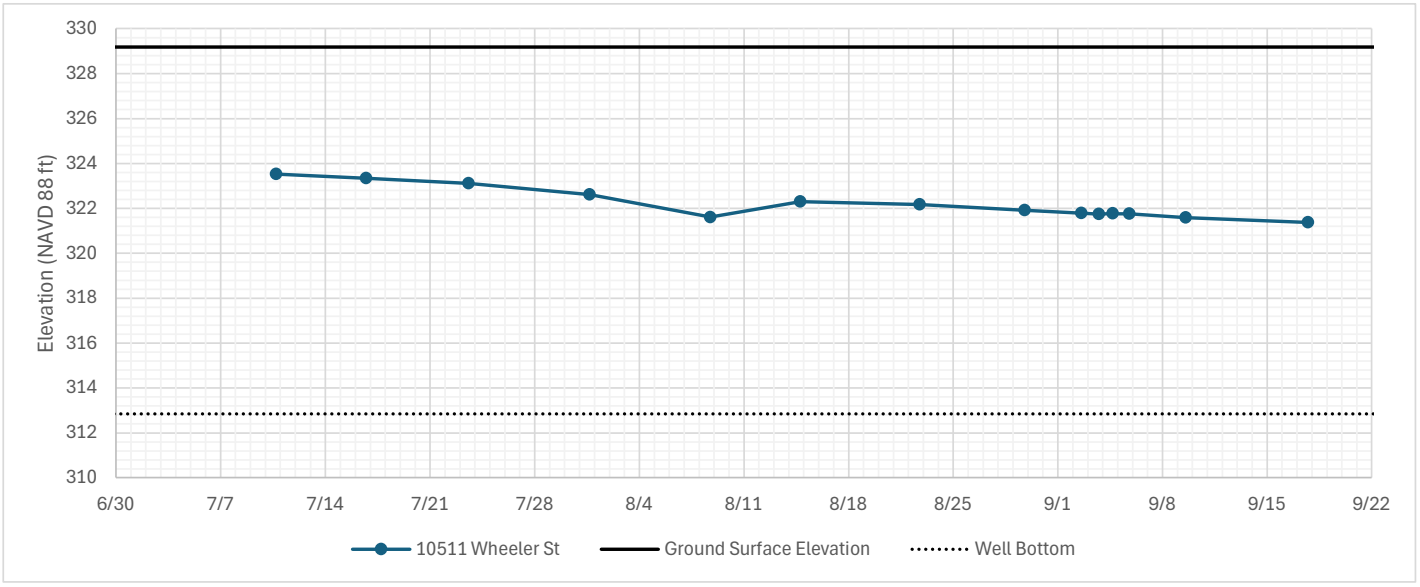
	Ground Elevation	Well Total Depth	Casing Height
43906 Tibbens Ln	436.60	45.00	1.67

Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/10/2025 16:15	417.46	43906 Tibbens Ln	7/10/2025	16:15	20.80	45' Total Depth, 4' Caisson
7/16/2025 15:35	416.95	43906 Tibbens Ln	7/16/2025	15:35	21.31	Not Pumping
7/23/2025 16:35	416.56	43906 Tibbens Ln	7/23/2025	16:35	21.70	Obstruction at 72', Not Pumping
7/31/2025 15:48	415.76	43906 Tibbens Ln	7/31/2025	15:48	22.50	0
8/8/2025 17:26	415.99	43906 Tibbens Ln	8/8/2025	17:26	22.27	0
8/14/2025 15:59	415.65	43906 Tibbens Ln	8/14/2025	15:59	22.61	0
8/22/2025 17:05	415.18	43906 Tibbens Ln	8/22/2025	17:05	23.08	0
8/29/2025 14:44	414.84	43906 Tibbens Ln	8/29/2025	14:44	23.42	0
9/2/2025 17:20	414.23	43906 Tibbens Ln	9/2/2025	17:20	24.03	0
9/3/2025 15:37	414.67	43906 Tibbens Ln	9/3/2025	15:37	23.59	0
9/4/2025 17:26	414.68	43906 Tibbens Ln	9/4/2025	17:26	23.58	Measured twice
9/5/2025 18:39	414.56	43906 Tibbens Ln	9/5/2025	18:39	23.70	0
9/9/2025 16:24	414.34	43906 Tibbens Ln	9/9/2025	16:24	23.92	0
9/17/2025 18:20	413.83	43906 Tibbens Ln	9/17/2025	18:20	24.43	0



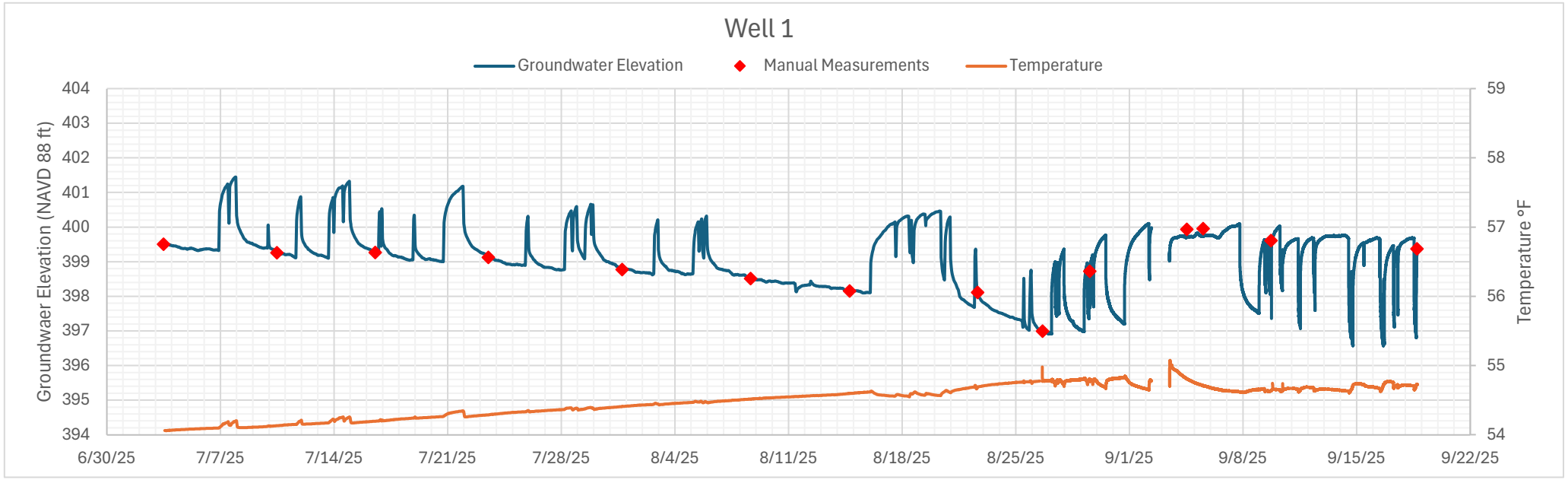
	Ground Elevation	Well Total Depth	Casing Height
10511 Wheeler St	329.18	18.00	1.67

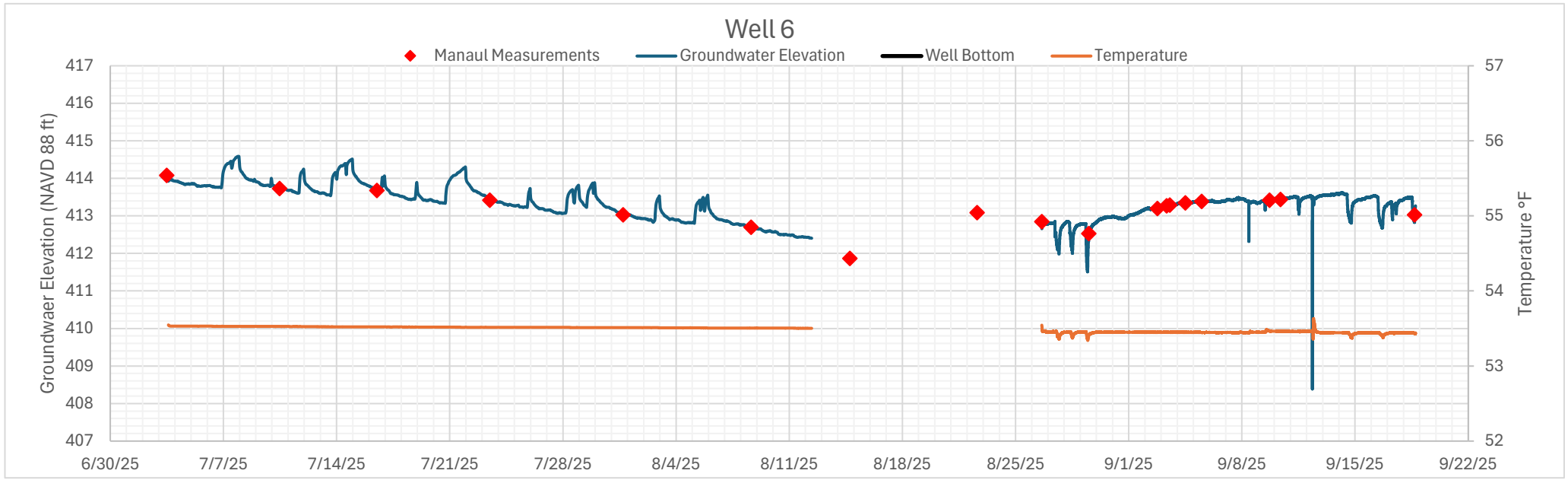
Date-Time	GWE	Well ID	Date	Time	Depth to Water (ft bgs)	Comments
7/10/2025 17:15	323.52	10511 Wheeler St	7/10/2025	17:15	7.32	4' Caisson
7/16/2025 17:45	323.33	10511 Wheeler St	7/16/2025	17:45	7.51	Not Pumping
7/23/2025 14:15	323.11	10511 Wheeler St	7/23/2025	14:15	7.73	Not Pumping
7/31/2025 16:50	322.60	10511 Wheeler St	7/31/2025	16:50	8.24	0
8/8/2025 18:22	321.60	10511 Wheeler St	8/8/2025	18:22	9.24	0
8/14/2025 18:36	322.29	10511 Wheeler St	8/14/2025	18:36	8.55	0
8/22/2025 18:37	322.16	10511 Wheeler St	8/22/2025	18:37	8.68	0
8/29/2025 19:20	321.91	10511 Wheeler St	8/29/2025	19:20	8.93	0
9/2/2025 14:05	321.78	10511 Wheeler St	9/2/2025	14:05	9.06	0
9/3/2025 18:26	321.74	10511 Wheeler St	9/3/2025	18:26	9.10	0
9/4/2025 16:43	321.76	10511 Wheeler St	9/4/2025	16:43	9.08	0
9/5/2025 19:03	321.75	10511 Wheeler St	9/5/2025	19:03	9.09	0
9/9/2025 13:40	321.58	10511 Wheeler St	9/9/2025	13:40	9.26	0
9/17/2025 18:02	321.37	10511 Wheeler St	9/17/2025	18:02	9.47	18 feet deep from TOC

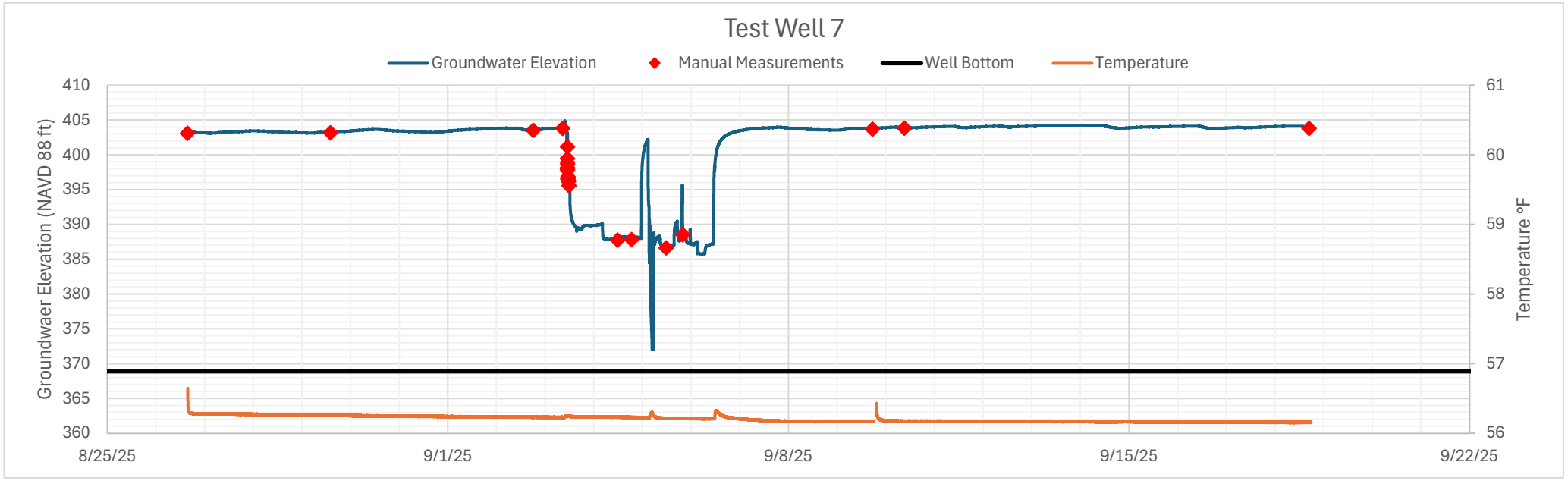


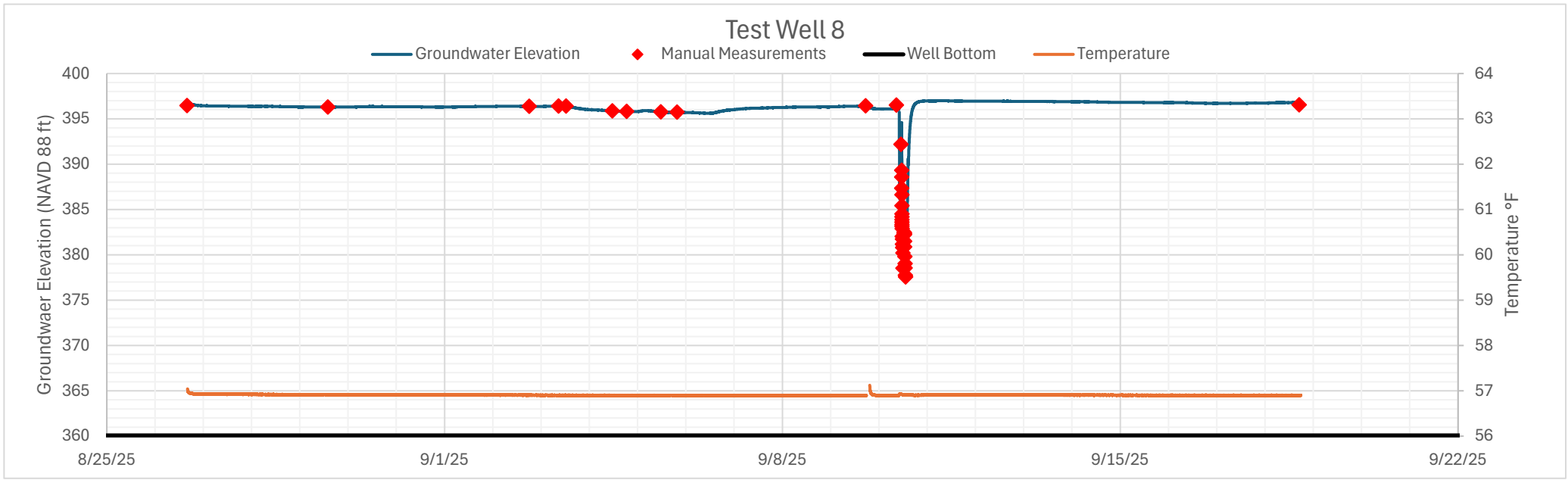
Appendix D

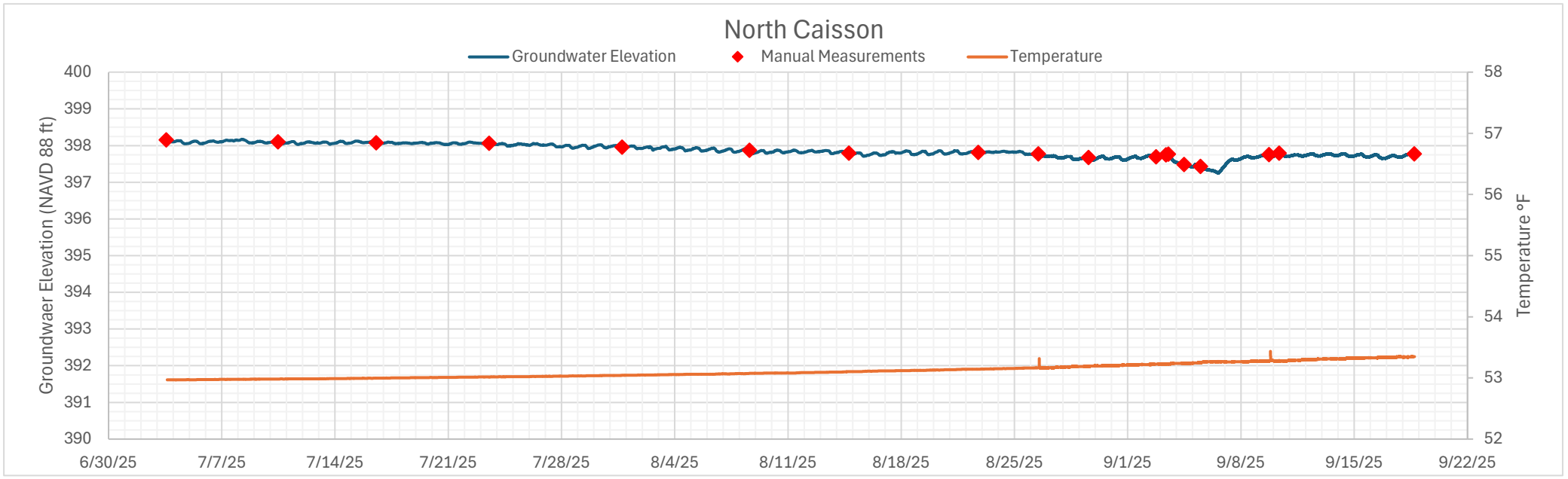
Transducer Hydrographs

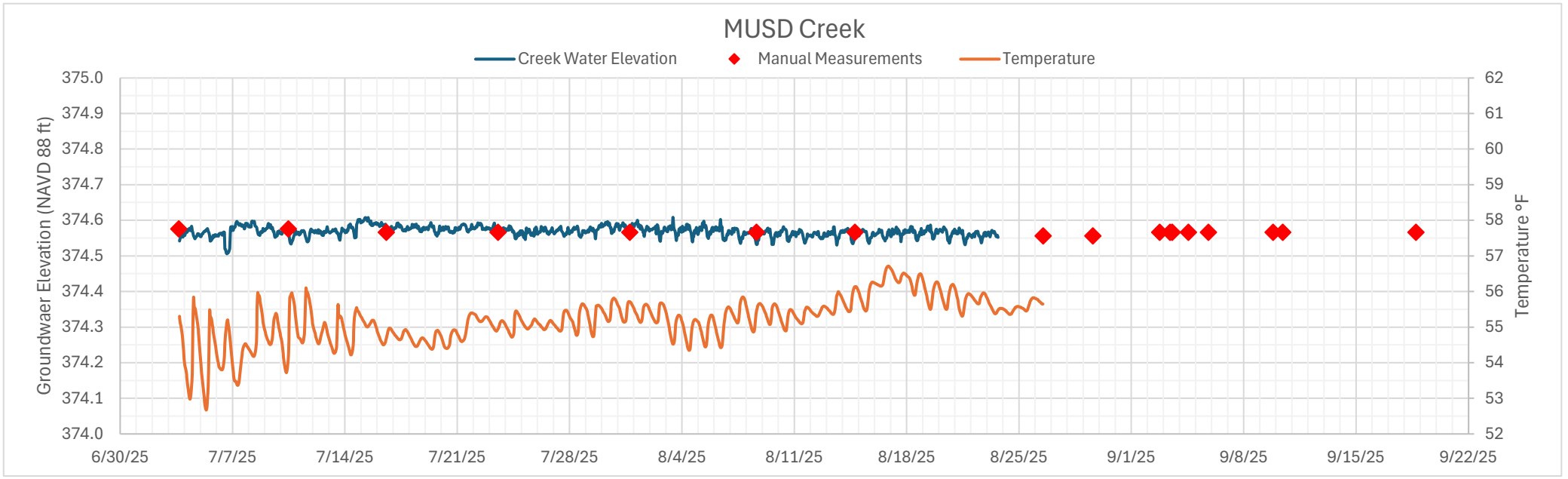

Well 1
Groundwater Elevation
Manual Measurements
Temperature
Groundwaer Elevation (NAVD 88 ft)
Temperature °F
404
403
402
401
400
399
398
397
396
395
394
59
58
57
56
55
54
6/30/25
7/7/25
7/14/25
7/21/25
7/28/25
8/4/25
8/11/25
8/18/25
8/25/25
9/1/25
9/8/25
9/15/25
9/22/25

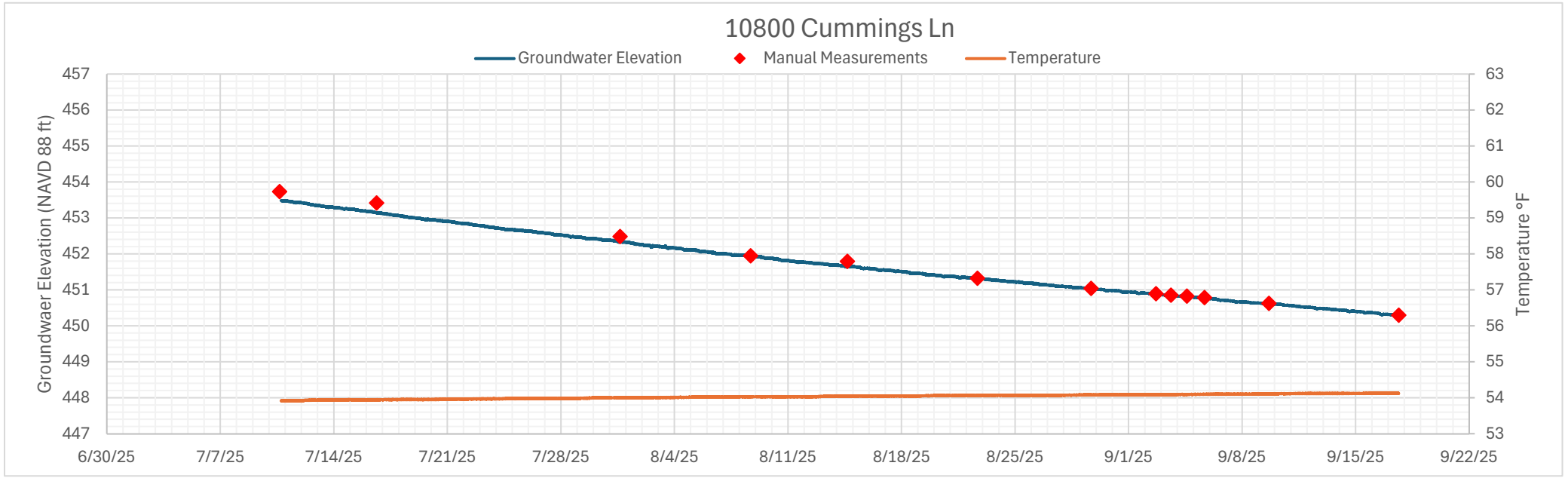

Well 6
Manaul Measurements
Groundwater Elevation
Well Bottom
Temperature
Groundwaer Elevation (NAVD 88 ft)
Temperature °F
417
416
415
414
413
412
411
410
409
408
407
57
56
55
54
53
52
6/30/25
7/7/25
7/14/25
7/21/25
7/28/25
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9/15/25
9/22/25

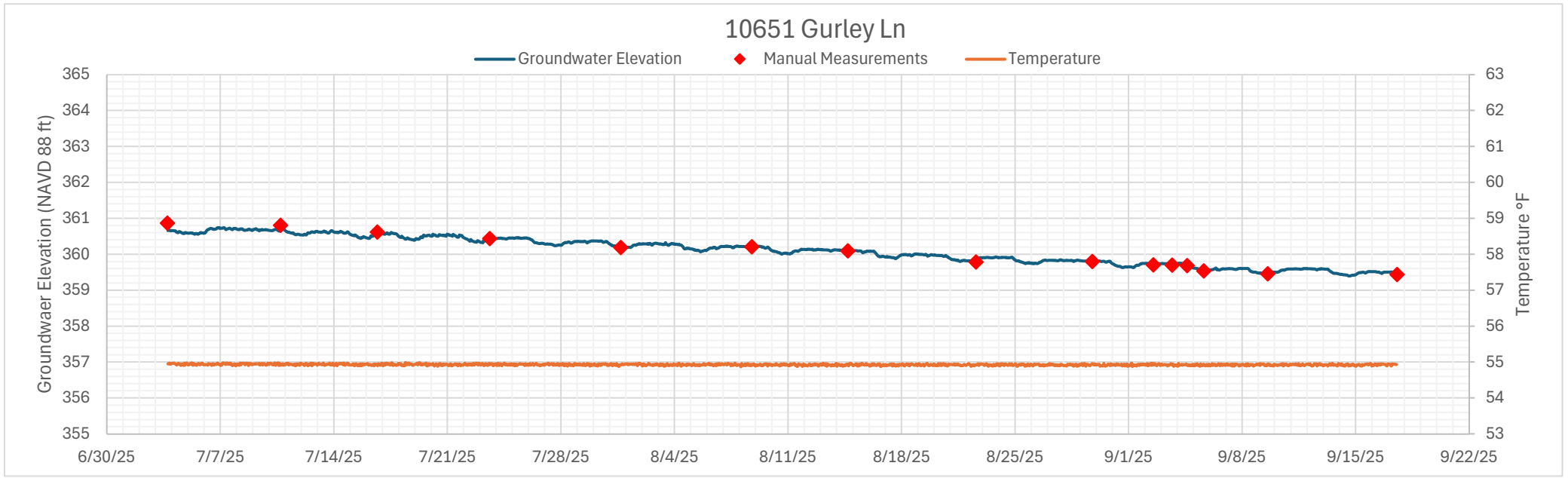

Test Well 7
Groundwater Elevation
Manual Measurements
Well Bottom
Temperature
Groundwaer Elevation (NAVD 88 ft)
Temperature °F
410
405
400
395
390
385
380
375
370
365
360
61
60
59
58
57
56
8/25/25
9/1/25
9/8/25
9/15/25
9/22/25

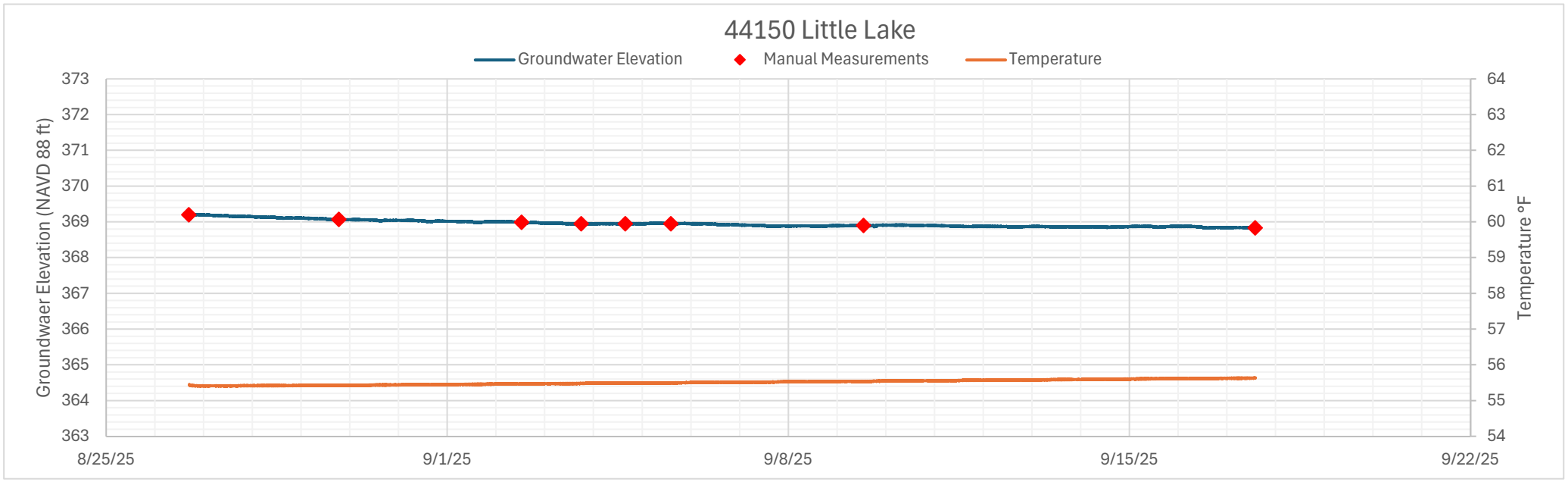

Test Well 8
Groundwater Elevation
Manual Measurements
Well Bottom
Temperature
Groundwaer Elevation (NAVD 88 ft)
Temperature °F
400
395
390
385
380
375
370
365
360
64
63
62
61
60
59
58
57
56
8/25/25
9/1/25
9/8/25
9/15/25
9/22/25

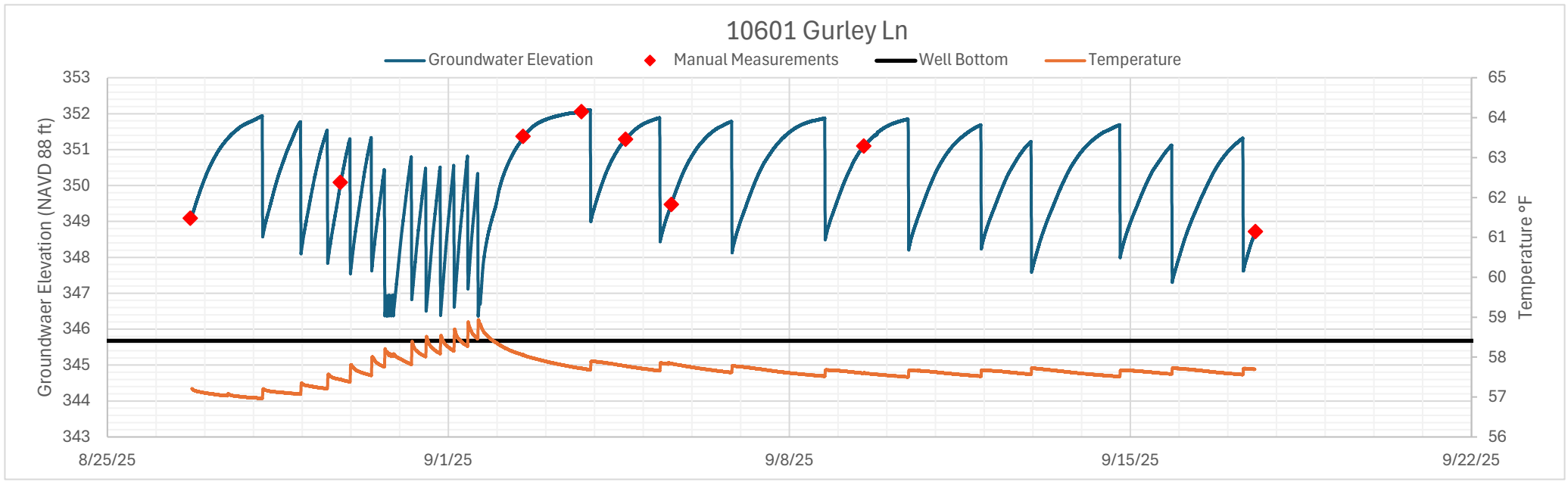

North Caisson
Groundwater Elevation
Manual Measurements
Temperature
Groundwaer Elevation (NAVD 88 ft)
Temperature °F
400
399
398
397
396
395
394
393
392
391
390
58
57
56
55
54
53
52
6/30/25
7/7/25
7/14/25
7/21/25
7/28/25
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9/8/25
9/15/25
9/22/25

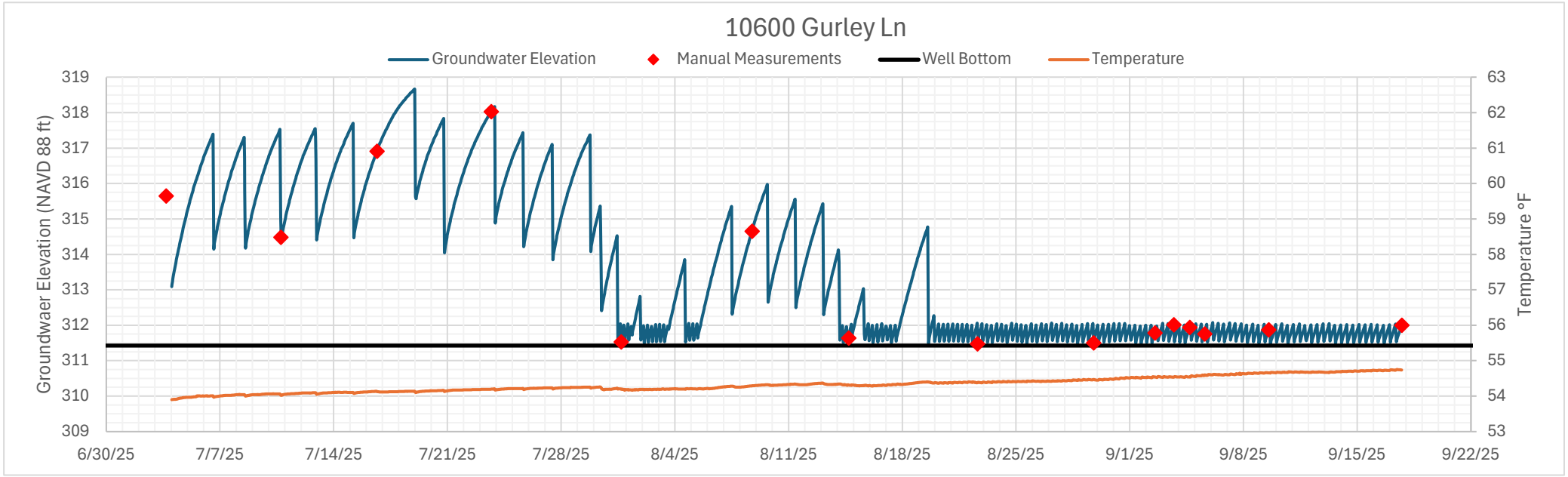

MUSD Creek
Creek Water Elevation
Manual Measurements
Temperature
Groundwaer Elevation (NAVD 88 ft)
Temperature °F
375.0
374.9
374.8
374.7
374.6
374.5
374.4
374.3
374.2
374.1
374.0
62
61
60
59
58
57
56
55
54
53
52
6/30/25
7/7/25
7/14/25
7/21/25
7/28/25
8/4/25
8/11/25
8/18/25
8/25/25
9/1/25
9/8/25
9/15/25
9/22/25

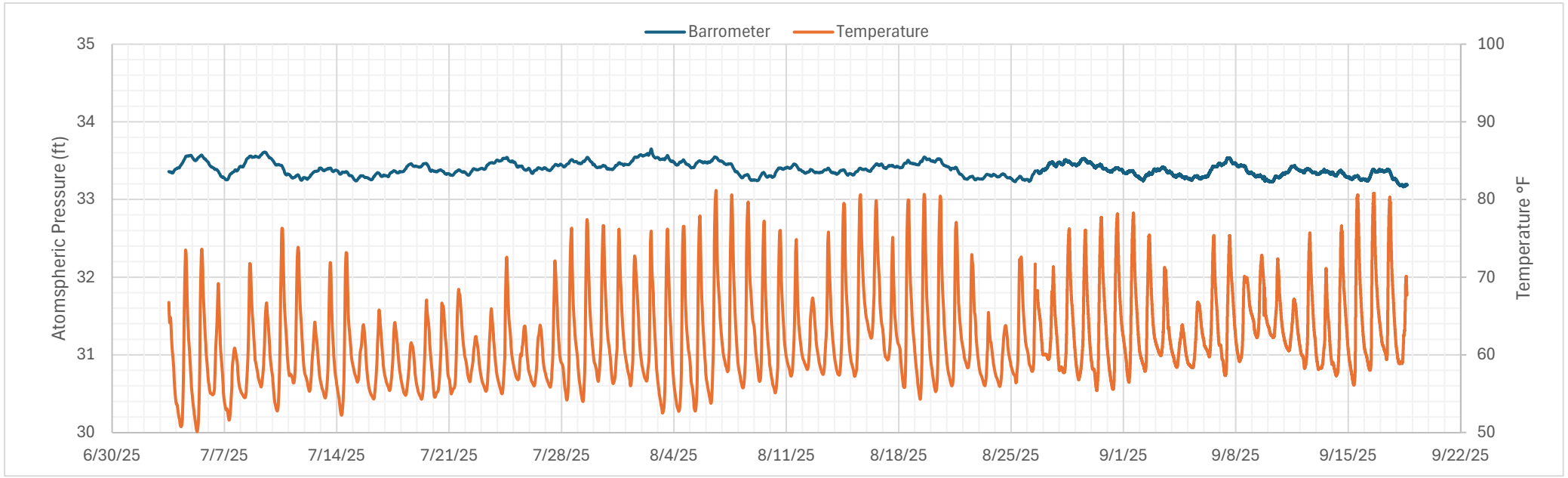

10800 Cummings Ln
Groundwater Elevation
Manual Measurements
Temperature
Groundwaer Elevation (NAVD 88 ft)
Temperature °F
457
456
455
454
453
452
451
450
449
448
447
63
62
61
60
59
58
57
56
55
54
53
6/30/25
7/7/25
7/14/25
7/21/25
7/28/25
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8/11/25
8/18/25
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9/1/25
9/8/25
9/15/25
9/22/25

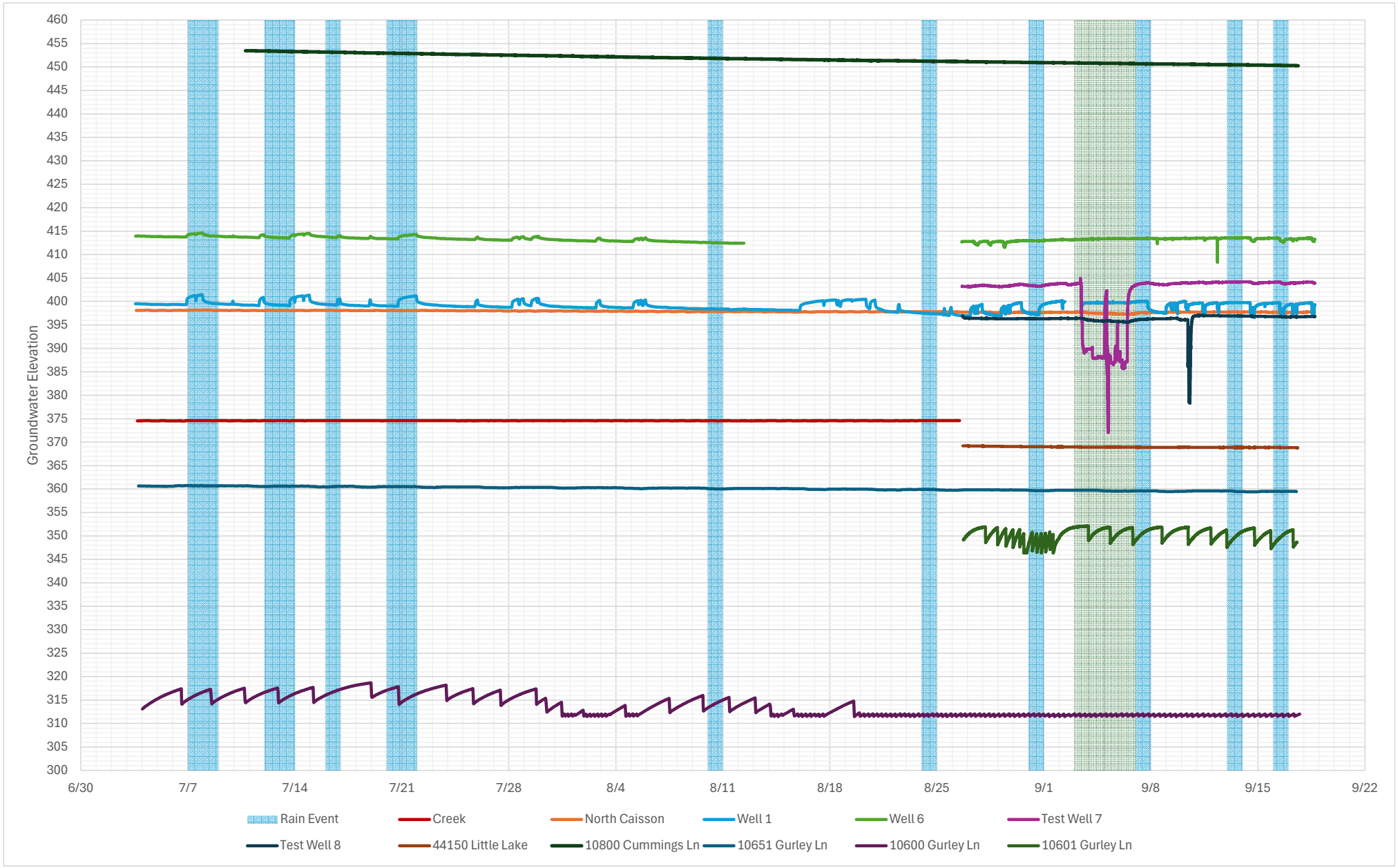

10651 Gurley Ln
Groundwater Elevation
Manual Measurements
Temperature
Groundwaer Elevation (NAVD 88 ft)
Temperature °F
365
364
363
362
361
360
359
358
357
356
355
63
62
61
60
59
58
57
56
55
54
53
6/30/25
7/7/25
7/14/25
7/21/25
7/28/25
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9/1/25
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9/15/25
9/22/25

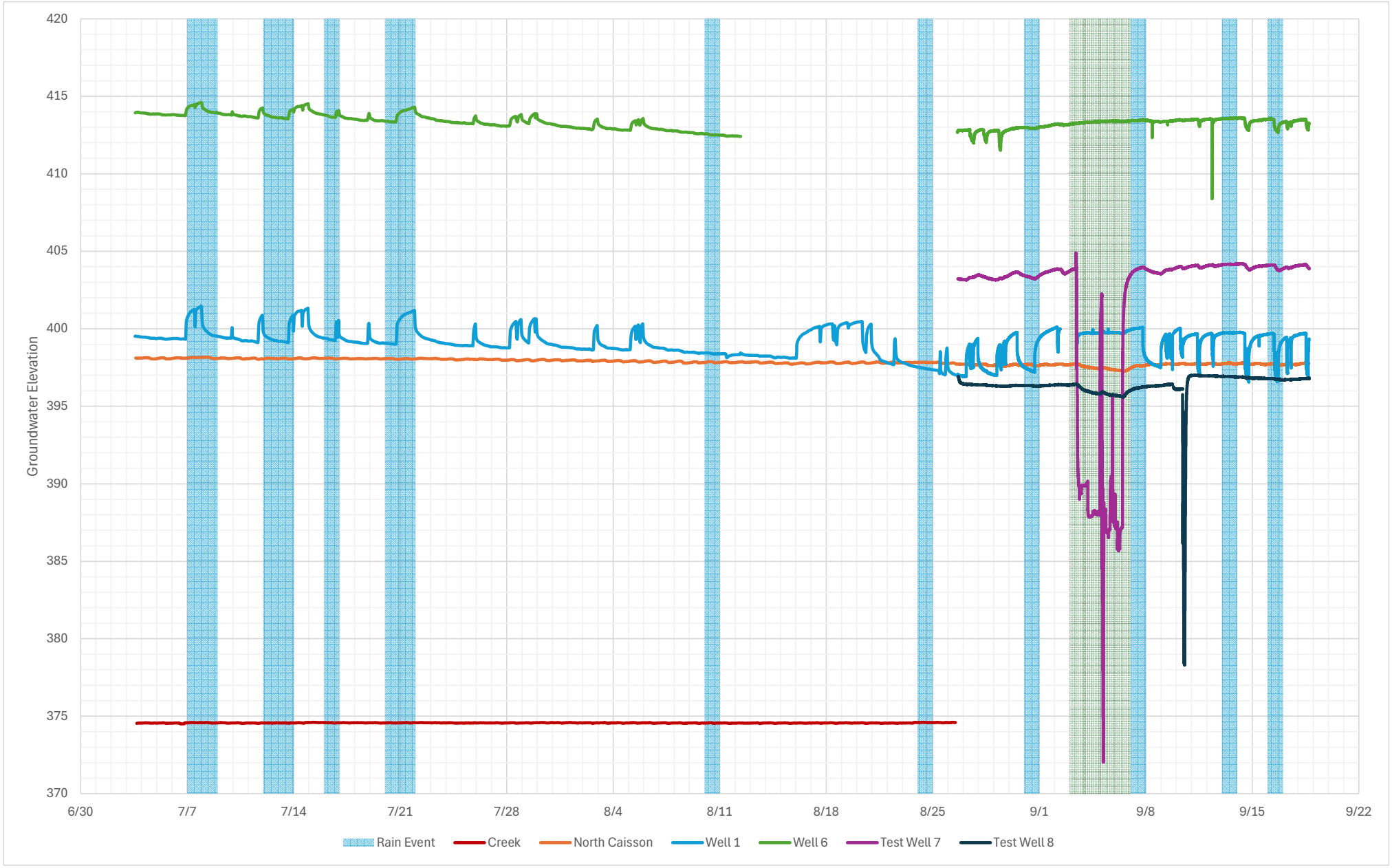

44150 Little Lake
Groundwater Elevation
Manual Measurements
Temperature
Groundwaer Elevation (NAVD 88 ft)
Temperature °F
373
372
371
370
369
368
367
366
365
364
363
64
63
62
61
60
59
58
57
56
55
54
8/25/25
9/1/25
9/8/25
9/15/25
9/22/25


10601 Gurley Ln
Groundwater Elevation
Manual Measurements
Well Bottom
Temperature
Groundwaer Elevation (NAVD 88 ft)
Temperature °F
353
352
351
350
349
348
347
346
345
344
343
65
64
63
62
61
60
59
58
57
56
8/25/25
9/1/25
9/8/25
9/15/25
9/22/25


10600 Gurley Ln
Groundwater Elevation
Manual Measurements
Well Bottom
Temperature
Groundwaer Elevation (NAVD 88 ft)
Temperature °F
319
318
317
316
315
314
313
312
311
310
309
63
62
61
60
59
58
57
56
55
54
53
6/30/25
7/7/25
7/14/25
7/21/25
7/28/25
8/4/25
8/11/25
8/18/25
8/25/25
9/1/25
9/8/25
9/15/25
9/22/25


Barrometer
Temperature
Atomspheric Pressure (ft)
Temperature °F
35
34
33
32
31
30
100
90
80
70
60
50
6/30/25
7/7/25
7/14/25
7/21/25
7/28/25
8/4/25
8/11/25
8/18/25
8/25/25
9/1/25
9/8/25
9/15/25
9/22/25


Groundwater Elevation
460
455
450
445
440
435
430
425
420
415
410
405
400
395
390
385
380
375
370
365
360
355
350
345
340
335
330
325
320
315
310
305
300
6/30
7/7
7/14
7/21
7/28
8/4
8/11
8/18
8/25
9/1
9/8
9/15
9/22
Rain Event
Creek
North Caisson
Well 1
Well 6
Test Well 7
Test Well 8
44150 Little Lake
10800 Cummings Ln
10651 Gurley Ln
10600 Gurley Ln
10601 Gurley Ln


Groundwater Elevation
420
415
410
405
400
395
390
385
380
375
370
6/30
7/7
7/14
7/21
7/28
8/4
8/11
8/18
8/25
9/1
9/8
9/15
9/22
Rain Event
Creek
North Caisson
Well 1
Well 6
Test Well 7
Test Well 8

Appendix E

Radius of Influence Calculations

Appendix F - Theis Equation Radius of Influence

T	415	ft^2/day
S	8.2.E-03	
Pumping Rate (Q)	6	gpm
	1,155	ft^3/day

Days Pumping	3	days

TW 07 (1,155 ft^3/day)	TW-8	Well 1	Well 2	Well 6	N. Caisson	44000 Little Lake	44150 Little Lake Rd	10601 Gurley Ln	10651 Gurley Ln	43906 Tibbens Ln	10750 Cummings Ln	43901 Little Lake Rd	10600 Gruely Ln
Distance (ft)	111	115	203	225	246	297	395	574	691	699	716	752	765
u	2.0.E-02	2.2.E-02	6.7.E-02	8.3.E-02	9.9.E-02	1.4.E-01	2.6.E-01	5.4.E-01	7.8.E-01	8.0.E-01	8.4.E-01	9.3.E-01	9.6.E-01
W(u)	3.35E+00	3.35E+00	2.15E+00	2.03E+00	1.82E+00	1.82E+00	9.10E-01	5.60E-01	3.10E-01	3.10E-01	3.10E-01	2.60E-01	2.19E-01
s (ft)	0.74	0.74	0.48	0.45	0.40	0.40	0.20	0.12	0.07	0.07	0.07	0.06	0.05

Days Pumping	90	days

TW 07 (1,155 ft^3/day)	TW-8	Well 1	Well 2	Well 6	N. Caisson	44000 Little Lake	44150 Little Lake Rd	10601 Gurley Ln	10651 Gurley Ln	43906 Tibbens Ln	10750 Cummings Ln	43901 Little Lake Rd	10600 Gruely Ln
Distance (ft)	111	115	203	225	246	297	395	574	691	699	716	752	765
u	6.7.E-04	7.2.E-04	2.2.E-03	2.8.E-03	3.3.E-03	4.8.E-03	8.5.E-03	1.8.E-02	2.6.E-02	2.7.E-02	2.8.E-02	3.1.E-02	3.2.E-02
W(u)	6.69E+00	6.69E+00	5.64E+00	5.23E+00	5.23E+00	4.73E+00	4.14E+00	3.35E+00	2.96E+00	2.96E+00	2.96E+00	2.96E+00	2.96E+00
s (ft)	1.48	1.48	1.25	1.16	1.16	1.05	0.92	0.74	0.66	0.66	0.66	0.66	0.66

Days Pumping	180	days

TW 07 (1,155 ft^3/day)	TW-8	Well 1	Well 2	Well 6	N. Caisson	44000 Little Lake	44150 Little Lake Rd	10601 Gurley Ln	10651 Gurley Ln	43906 Tibbens Ln	10750 Cummings Ln	43901 Little Lake Rd	10600 Gruely Ln
Distance (ft)	111	115	203	225	246	297	395	574	691	699	716	752	765
u	3.4.E-04	3.6.E-04	1.1.E-03	1.4.E-03	1.7.E-03	2.4.E-03	4.3.E-03	9.0.E-03	1.3.E-02	1.3.E-02	1.4.E-02	1.5.E-02	1.6.E-02
W(u)	7.53E+00	7.25E+00	6.33E+00	6.33E+00	5.64E+00	5.64E+00	4.95E+00	4.14E+00	4.04E+00	4.04E+00	4.04E+00	3.35E+00	3.35E+00
s (ft)	1.67	1.61	1.40	1.40	1.25	1.25	1.10	0.92	0.89	0.89	0.89	0.74	0.74

43970 Little Lake Rd	10800 Cummings Ln	10780 Cummings Ln	10781 Cummings Ln	10833 Cummings Ln	10511 Wheeler St	10851 Merrill Ln	44460 Little Lake Rd
776	863	907	1073	1337	1476	1870	1982
9.9.E-01	1.2.E+00	1.3.E+00	1.9.E+00	2.9.E+00	3.6.E+00	5.7.E+00	6.4.E+00
2.19E-01	2.19E-01	2.19E-01	4.90E-02	1.30E-02	3.80E-03	3.60E-04	3.60E-04
0.05	0.05	0.05	0.01	0.00	0.00	0.00	0.00

43970 Little Lake Rd	10800 Cummings Ln	10780 Cummings Ln	10781 Cummings Ln	10833 Cummings Ln	10511 Wheeler St	10851 Merrill Ln	44460 Little Lake Rd
776	863	907	1073	1337	1476	1870	1982
3.3.E-02	4.1.E-02	4.5.E-02	6.3.E-02	9.8.E-02	1.2.E-01	1.9.E-01	2.1.E-01
2.96E+00	2.68E+00	2.68E+00	2.30E+00	1.82E+00	1.82E+00	1.22E+00	1.22E+00
0.66	0.59	0.59	0.51	0.40	0.40	0.27	0.27

43970 Little Lake Rd	10800 Cummings Ln	10780 Cummings Ln	10781 Cummings Ln	10833 Cummings Ln	10511 Wheeler St	10851 Merrill Ln	44460 Little Lake Rd
776	863	907	1073	1337	1476	1870	1982
1.6.E-02	2.0.E-02	2.2.E-02	3.1.E-02	4.9.E-02	5.9.E-02	9.5.E-02	1.1.E-01
3.35E+00	3.35E+00	3.35E+00	2.96E+00	2.47E+00	2.30E+00	1.82E+00	1.82E+00
0.74	0.74	0.74	0.66	0.55	0.51	0.40	0.40

Appendix F - Theis Equation Radius of Influence

MDD	**17.7**	
T	415	ft^2/day
S	8.2.E-03	
Days Pumping	3	days

	TW 07	Well 1	Well 2	Well 6	Total
Max gpm	6	10	7	5	28
% of Total Capacity	21%	36%	25%	18%	100%
Weighted Avg gpm	3.8	6.3	4.4	3.2	17.7
Q (ft^3/day)	730	1217	852	608	3407

TW 07 (730 ft^3/day)	TW-7	TW-8	Well 1	Well 2	Well 6	N. Caisson	44000 Little Lake	44150 Little Lake Rd	10601 Gurley Ln	10651 Gurley Ln	43906 Tibbens Ln	10750 Cummings Ln
Distance (ft)		111	115	203	225	246	297	395	574	691	699	716
u	-	2.0.E-02	2.2.E-02	6.7.E-02	8.3.E-02	9.9.E-02	1.4.E-01	2.6.E-01	5.4.E-01	7.8.E-01	8.0.E-01	8.4.E-01
W(u)	-	3.35E+00	3.35E+00	2.15E+00	2.03E+00	1.82E+00	1.82E+00	9.10E-01	5.60E-01	3.10E-01	3.10E-01	3.10E-01
s (ft)	-	0.47	0.47	0.30	0.28	0.25	0.25	0.13	0.08	0.04	0.04	0.04

Well 01 (1,217 ft^3/day)	TW-7	TW-8	Well 1	Well 2	Well 6	N. Caisson	44000 Little Lake	44150 Little Lake Rd	10601 Gurley Ln	10651 Gurley Ln	43906 Tibbens Ln	10750 Cummings Ln
Distance (ft)	115	225		103.5	144.4	291.2	249	497	687	769	587	649
u	2.2.E-02	8.3.E-02	-	1.8.E-02	3.4.E-02	1.4.E-01	1.0.E-01	4.0.E-01	7.7.E-01	9.7.E-01	5.6.E-01	6.9.E-01
W(u)	3.35E+00	2.03E+00	-	3.35E+00	2.96E+00	1.82E+00	1.82E+00	7.00E-01	3.10E-01	2.19E-01	4.50E-01	3.70E-01
s (ft)	0.78	0.47	-	0.78	0.69	0.42	0.42	0.16	0.07	0.05	0.11	0.09

Well 02 (852 ft^3/day)	TW-7	TW-8	Well 1	Well 2	Well 6	N. Caisson	44000 Little Lake	44150 Little Lake Rd	10601 Gurley Ln	10651 Gurley Ln	43906 Tibbens Ln	10750 Cummings Ln
Distance (ft)	203	304	103.5		54.5	293	173	546	751	780	542	550
u	6.7.E-02	1.5.E-01	1.8.E-02	-	4.9.E-03	1.4.E-01	4.9.E-02	4.9.E-01	9.2.E-01	1.0.E+00	4.8.E-01	5.0.E-01
W(u)	2.15E+00	1.22E+00	3.35E+00	-	4.73E+00	1.82E+00	2.47E+00	5.60E-01	2.60E-01	2.19E-01	5.60E-01	5.60E-01
s (ft)	0.35	0.20	0.55	-	0.77	0.30	0.40	0.09	0.04	0.04	0.09	0.09

Well 06 (608 ft^3/day)	TW-7	TW-8	Well 1	Well 2	Well 6	N. Caisson	44000 Little Lake	44150 Little Lake Rd	10601 Gurley Ln	10651 Gurley Ln	43906 Tibbens Ln	10750 Cummings Ln
Distance (ft)	225	314	144	55		262	118	532	744	746	571	504
u	8.3.E-02	1.6.E-01	3.4.E-02	5.0.E-03	-	1.1.E-01	2.3.E-02	4.6.E-01	9.1.E-01	9.1.E-01	5.3.E-01	4.2.E-01
W(u)	2.03E+00	1.22E+00	2.96E+00	4.73E+00	-	1.82E+00	3.35E+00	5.60E-01	2.60E-01	2.60E-01	5.60E-01	7.00E-01
s (ft)	0.24	0.14	0.35	0.55	-	0.21	0.39	0.07	0.03	0.03	0.07	0.08

Cummulative Drawdown (ft)	**-**	**1.28**	**-**	**-**	**-**	**1.19**	**1.47**	**0.45**	**0.22**	**0.16**	**0.31**	**0.30**

43901 Little Lake Rd	10600 Gruely Ln	43970 Little Lake Rd	10800 Cummings Ln	10780 Cummings Ln	10781 Cummings Ln	10833 Cummings Ln	10511 Wheeler St	10851 Merrill Ln	44460 Little Lake Rd
752	765	776	863	907	1073	1337	1476	1870	1982
9.3.E-01	9.6.E-01	9.9.E-01	1.2.E+00	1.3.E+00	1.9.E+00	2.9.E+00	3.6.E+00	5.7.E+00	6.4.E+00
2.60E-01	2.19E-01	2.19E-01	2.19E-01	2.19E-01	4.90E-02	1.30E-02	3.80E-03	3.60E-04	3.60E-04
0.04	0.03	0.03	0.03	0.03	0.01	0.00	0.00	0.00	0.00

43901 Little Lake Rd	10600 Gruely Ln	43970 Little Lake Rd	10800 Cummings Ln	10780 Cummings Ln	10781 Cummings Ln	10833 Cummings Ln	10511 Wheeler St	10851 Merrill Ln	44460 Little Lake Rd
640	876	688	835	852	999	1249	1590	1959	2097
6.7.E-01	1.3.E+00	7.7.E-01	1.1.E+00	1.2.E+00	1.6.E+00	2.6.E+00	4.1.E+00	6.3.E+00	7.2.E+00
3.70E-01	2.19E-01	3.10E-01	2.19E-01	2.19E-01	4.90E-02	1.30E-02	3.80E-03	3.60E-04	1.20E-04
0.09	0.05	0.07	0.05	0.05	0.01	0.00	0.00	0.00	0.00

43901 Little Lake Rd	10600 Gruely Ln	43970 Little Lake Rd	10800 Cummings Ln	10780 Cummings Ln	10781 Cummings Ln	10833 Cummings Ln	10511 Wheeler St	10851 Merrill Ln	44460 Little Lake Rd
552	936	585	755	757	897	1146	1675	1975	2177
5.0.E-01	1.4.E+00	5.6.E-01	9.3.E-01	9.4.E-01	1.3.E+00	2.1.E+00	4.6.E+00	6.4.E+00	7.8.E+00
5.60E-01	2.19E-01	4.50E-01	2.60E-01	2.60E-01	2.19E-01	4.90E-02	1.10E-03	3.60E-04	3.80E-05
0.09	0.04	0.07	0.04	0.04	0.04	0.01	0.00	0.00	0.00

43901 Little Lake Rd	10600 Gruely Ln	43970 Little Lake Rd	10800 Cummings Ln	10780 Cummings Ln	10781 Cummings Ln	10833 Cummings Ln	10511 Wheeler St	10851 Merrill Ln	44460 Little Lake Rd
550	925	551	701	708	856	1113	1682	1941	2179
5.0.E-01	1.4.E+00	5.0.E-01	8.0.E-01	8.2.E-01	1.2.E+00	2.0.E+00	4.6.E+00	6.2.E+00	7.8.E+00
5.60E-01	2.19E-01	5.60E-01	3.10E-01	3.10E-01	2.19E-01	4.90E-02	1.10E-03	3.60E-04	3.80E-05
0.07	0.03	0.07	0.04	0.04	0.03	0.01	0.00	0.00	0.00

0.28	**0.14**	**0.24**	**0.16**	**0.16**	**0.08**	**0.02**	**0.00**	**0.00**	**0.00**



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→ The Power of Commitment